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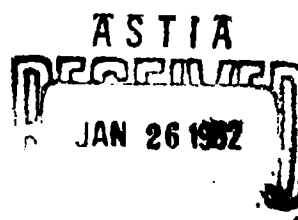
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WIND-TUNNEL TESTS OF A 1/20-SCALE AIRSHIP MODEL
WITH STERN PROPELLERS

By H. Clyde McLemore

Langley Research Center
Langley Air Force Base, Va.

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SUMMARY

An investigation has been conducted in the Langley full-scale tunnel on a 1/20-scale airship model to determine the characteristics of stern-mounted propellers (or wake propellers) and the effect of the propellers on the airship. The investigation included tests of two different propellers and included measurements of propeller thrust and power characteristics, airship force and moment characteristics, hull pressure distributions, and hull boundary-layer and wake characteristics. The tests were conducted for several propeller-blade angles and rotational speeds for test velocities of about 94 ft/sec and 139 ft/sec.

The test results showed that a stern-mounted propeller can give a much higher propulsive efficiency than that of a conventional-mounted- or a fin-mounted-propeller installation. This increased efficiency should result in increased range and endurance for the stern-propeller configuration. In general, stern-propeller operation was found to have only very small effects on the model aerodynamic characteristics.

INTRODUCTION

For many years the idea of a stern-mounted propeller or a wake propeller for airships has been suggested as a means of improving the propeller efficiency. A few sporadic wind-tunnel tests and theoretical analyses have been made and in most instances the conclusion reached was that a propeller designed to operate in the airship wake would operate more efficiently than a conventional-propeller installation. Recent developments have shown the need for longer endurance flights of airships used for aircraft early warning and submarine detection missions which would require configurations having a more efficient propulsive system. The stern-mounted propeller would have further advantages for

the longer endurance flights by providing some relief of aircrew fatigue and detection instrument inaccuracies resulting from the noise and vibration of a normal close-proximity propeller installation.

Because of these apparant advantages of the stern-propeller configuration, it was decided that this type of configuration should be investigated. It was decided, however, that a propeller should be designed specifically for the airflow conditions existing at the intended propeller plane. These airflow conditions had been obtained during previous unreported wind-tunnel tests conducted in the Langley full-scale tunnel by Marvin P. Fink on the same airship hull.

In order to check the theories involved in the design of a stern propeller, two different approaches to the problem were made. The results gave two dissimilar wake propellers for use on a 1/20-scale model airship designed for wind-tunnel tests in the Langley full-scale tunnel. One propeller was designed by using the best available theories as a 4-blade, 2-foot-diameter, twisted and tapered propeller having a propeller solidity of 0.129 and Clark Y airfoil sections. The other propeller, for reasons of simplicity, was designed as a 3-blade, 1.37-foot-diameter, untwisted and untapered propeller having a propeller solidity of 0.103 and NACA 63₂-015 airfoil sections.

Tests were conducted for each of these propellers for three blade angles over a range of advance ratios from about 0.5 to 1.3. The Reynolds numbers of the tests, based on hull length, were about 11.9×10^6 and 17.5×10^6 which corresponds to test airspeeds of about 94 ft/sec and 139 ft/sec, respectively. The tests included the determination of the propeller characteristics, complete-model aerodynamic forces and moments, aft section hull boundary-layer and propeller-wake characteristics, and surface-pressure distributions for one longitudinal station of the fuselage.

SYMBOLS

Force and moment coefficients are based on hull volume and are referred to the stability axes the origin of which is the center of buoyancy. This point is located on the model center line 109.30 inches aft of the model nose.

A_e total effective blade area factor, $(B)(F)(D^2)$, sq ft

F activity factor per blade, $\frac{100,000}{16} \int_{0.2}^{1.0} \left(\frac{c}{D}\right) x^3 dx$

B number of blades

L
1
6
1
8

c	local propeller chord, ft
c _e	propeller equivalent chord, $\frac{\int_0^{1.0} cx^2 dx}{\int_0^{1.0} x^2 dx}$, ft
D	propeller diameter, ft
D ₀	drag of basic model (propeller off), lb
h	total length of boundary-layer or wake rake, ft
l	total length of hull, ft
n	propeller rotational speed, rps
P	power, $2\pi nQ$, ft-lb/sec
p _l	local static pressure, lb/sq ft
p _∞	free-stream static pressure, lb/sq ft
Q	propeller torque, ft-lb
q _l	local dynamic pressure, lb/sq ft
q _∞	free-stream dynamic pressure, lb/sq ft
R	propeller radius, ft
r	propeller radius at any station, ft
T _p	propeller thrust, lb
T _e	effective thrust (Propeller thrust - Propeller-induced change in hull drag), lb
t	propeller blade width, ft
U _l	local velocity, ft/sec
U _∞	free-stream velocity, ft/sec

U_{∞}/nD	propeller advance ratio	
V	hull volume, 184 cu ft	
x	chordwise distance along fuselage, ft or fraction of propeller radius, (r/R)	
y	distance from and normal to hull longitudinal axis, ft	
z	distance from propeller axis along wake rake, ft	
α	model angle of attack, deg	1
β	propeller blade angle measured at $0.75R$, deg	6
δ_e	elevator deflection angle (positive deflection, trailing edge down), deg	1
η	propeller efficiency, $\frac{C_T}{C_P} \frac{U_{\infty}}{nD} = \frac{T_P U_{\infty}}{P}$	8
η_e	propeller propulsive efficiency, $\frac{C_{T_e}}{C_P} \frac{U_{\infty}}{nD}$	
ρ	mass density of air, slugs/cu ft	
C_L	lift coefficient, $\frac{\text{Lift}}{q_{\infty} V^{2/3}}$	
C_D	drag coefficient measured on scale system during propeller operating tests (equal to $C_{D,o}$ when propeller removed), $\frac{\text{Drag}}{q_{\infty} V^{2/3}}$	
$C_{D,e}$	effective drag coefficient $(C_{D,o} - C_D)$	
$C_{D,o}$	drag coefficient of basic hull, propeller off ($C_{D,o} = 0.0210$)	
$C_{D,e}/C_{D,o}$	ratio of effective drag to the drag of the basic hull	
C_l	rolling-moment coefficient, $\frac{\text{Rolling moment}}{q_{\infty} V}$	

C_m	pitching-moment coefficient, $\frac{\text{Pitching moment}}{q_\infty V}$
C_n	yawing-moment coefficient, $\frac{\text{Yawing moment}}{q_\infty V}$
C_p	power coefficient, $\frac{P}{\rho n^3 D^5}$
C_p	pressure coefficient, $\frac{p_l - p_\infty}{q_\infty}$
C_T	thrust coefficient, $\frac{T_p}{\rho n^2 D^4}$
C_{T_e}	propeller propulsive thrust coefficient, $\frac{v^{2/3}}{2D^2} C_{D,e} \left(\frac{U_\infty}{nD} \right)^2$
C_Y	side-force coefficient, $\frac{\text{Side force}}{q_\infty v^{2/3}}$

MODEL

A 1/20-scale model of an airship equipped for stern propulsion was used in the present investigation. The model had a length of about 20.5 feet and a volume of 184 cubic feet. Principal dimensions of the hull, gondola, and tail surfaces are shown in figure 1. Photographs of the model and some of its components are shown in figure 2.

The tail configuration of the model was an inverted Y arrangement with 120° radial spacing of the surfaces. The longitudinal-control surfaces were equipped with actuators for remote control through ±20° range elevator deflection. The elevators were equipped with a servo tab with linkage to provide equal but opposite deflections to those of the elevator.

The model was equipped to operate with either of the two different propellers shown in the photographs of figures 2(b) and 2(c). The blade-form curves of the two propellers are shown in figures 3(a) and 3(b). Propeller 1 had 4 blades which were twisted and tapered, a diameter of 2 feet, a solidity of 0.129 (based on an equivalent chord c_e of

0.104 foot), an activity factor per blade of 68.5, a total effective blade area A_e of 1,095 square feet, and Clark Y airfoil sections.

Propeller 2 had 3 blades which were untwisted and untapered, a diameter of 1.37 feet, a solidity of 0.103, an activity factor per blade of 84.3, a total effective blade area A_e of 475 square feet, and NACA

632-015 airfoil sections. Each propeller had provisions for manually varying the blade angle. Both propellers were driven by 20-horsepower electric-induction motors. One motor was used to drive propeller 2, whereas two motors were required and were mounted in tandem to drive propeller 1. In each case, the motors were attached to the model with a strain-gage mount to measure propeller thrust and torque. The tandem-motor arrangement and strain-gage balance are shown in figure 2(d) and the single-motor arrangement is shown mounted in the model in figure 2(e).

Boundary-layer characteristics of the aft section of the hull were obtained by two rakes mounted so that the total and static tubes were parallel to the airship surface. The location of the rakes was 30° up from the horizontal plane; the port rake was 1 foot forward of the plane of propeller 1 and the starboard rake was 2 feet forward of this plane. The rakes were 13.6 inches long with 14 total tubes and 4 static tubes. The rakes are shown mounted on the model in figures 2(b), (c), and (e). The wake-survey rake which was mounted perpendicular to the longitudinal axis and rotated 45° to the starboard of the vertical fin was 2 feet long with the inboard tube on the propeller-shaft axis 1 foot aft of the plane of propeller 1. The wake-survey rake had 21 total tubes and 6 static tubes. Location of the individual tubes in the various rakes is given, in terms of their distances from the hull surface or shaft axis, in percent of rake length in the pressure-distribution tables 1 to 7. Surface-pressure-distribution data were obtained with two longitudinal rows of static-pressure orifices along the hull. The stations were 60° down from the vertical center line of the model and included 20 orifices on the port side and 5 orifices on the aft section of the starboard side. Location of the orifices, for plotting purposes, can be considered to be in a single longitudinal row on one side of the hull because they were symmetrical about the vertical center line. The chordwise locations in percent of fuselage length from the nose of the model are given in tables 2 to 7.

The model was mounted on a single support strut which entered the model through the gondola as shown in figure 2(f). Angle-of-attack changes were accomplished by remotely controlling an actuator mounted inside of the model. The gondola used in this investigation was somewhat larger than the original gondola as shown in figure 1 because of the mounting system of the model. The tunnel six-component scale-balance system was used for all force and moment measurements except those obtained from the motor-mount strain-gage system.

TESTS

Tests were conducted in the Langley full-scale tunnel on a 1/20-scale model of an airship with each of the two propellers and with the propellers removed. At $\alpha = -0.5^\circ$ the propeller characteristics were determined for a large range of rotational speeds for tunnel speeds of about 94 ft/sec and 139 ft/sec to give a range of propeller advance ratio from about 0.5 to 1.3. The configuration with propeller 1 installed was tested with blade angles, measured at the 0.75R station, of 15° , 20° , and 25° . Propeller 2 was initially checked out at the design angles of 15° , 17° , and 20° ; but it was found that, at settings of 15° and 17° for the design model speed and maximum allowable rotational speed, the propeller would not produce the desired thrust ($T_e = \text{Drag}$) nor would it absorb the expected power. The blade angles tested in the systematic investigation were, therefore, arbitrarily increased to 20° , 25° , and 30° .

The effect of propeller operation on the airship aerodynamic characteristics and the effect of angle of attack on the propeller characteristics for three arbitrary power conditions ($n = 70.33$, 76.67 , and 83.33) were determined for an angle-of-attack range of -10.5° to 9.5° . Elevator-effectiveness data were obtained from elevator-deflection tests (δ_e range from -20° to 20°) for the same angle-of-attack range only for the case of propeller 1 operating at a blade angle of 20° . All of these angle-of-attack tests were made for a test velocity of 139 ft/sec.

The surface-pressure-distribution orifices and the boundary-layer and wake rakes were connected to kerosene manometers and the results photographically recorded during all of the $\alpha = -0.5^\circ$ tests. The pressure coefficients, velocity- and dynamic-pressure ratios were determined by IBM data-reduction processes.

CORRECTIONS

All of the force and moment data presented have been corrected for airstream misalignment, buoyancy, and support-strut tares.

A drag coefficient of 0.0120 and 0.0100 at the test velocities of 94 ft/sec and 139 ft/sec, respectively, at $\alpha = -0.5^\circ$ has been subtracted from the drag results to correct for support-strut tares. The drag data at angles of attack other than -0.5° have been corrected by similar but slightly different values of drag coefficient. In general, the six-component scale balance is considered to be accurate in the drag component to ± 0.3 pound which at the test velocities of 94 ft/sec

and 139 ft/sec would result in possible errors in drag coefficient of about ± 0.0009 and ± 0.0004 , respectively.

RESULTS AND DISCUSSION

Propeller and Model Characteristics at $\alpha = -0.5^\circ$

The variation of the propeller thrust and power coefficients, propeller efficiency, and model drag coefficient with advance ratio are shown in figures 4 and 5 for propellers 1 and 2, respectively. For comparison purposes, the efficiencies of more conventional-propeller installations are shown in figure 6. The stern-propeller coefficients are seen to vary in a normal manner but the maximum propeller efficiencies as shown in figures 4(c) and 5(c) are much greater than those expected for a conventional-mounted propeller (fig. 6). The large values of maximum efficiency (on the order of 140 percent) are apparently erroneous because the propellers are operating in the wake of the airship, a reduced velocity field, and because the standard definition of propeller efficiency η includes free-stream velocity. Because of the low velocity of the wake, the propeller can produce more thrust per horsepower than it could in the free-stream flow. When this greater ratio of thrust to power is multiplied by the higher free-stream velocity to obtain the propeller efficiency ($\eta = \frac{T_p U_\infty}{P}$), the resulting value of efficiency may be very large. Because of these two factors, η may be well above 1.00; whereas, the efficiency of the propeller based on the velocity of the flow in which it is actually operating is conventional, that is, well below 1.00.

Additional analysis is required in order to determine whether these large values of propeller efficiency can actually be achieved with these particular propellers when they are producing enough thrust to propel the airship. In order to make this additional analysis, the data will be examined for the following thrust conditions: $T_e = D_0$, $T_e = 0.75D_0$, $T_e = 0.50D_0$, and $T_e = 0.25D_0$. In order to determine the operating conditions for these thrust conditions for propeller 1 and for conventional-mounted and fin-mounted propellers the data have been reduced to the form of $C_{D,e}/C_{D,0}$ and plotted against advance ratio in figure 7. Propeller 2 was not included in this analysis since preliminary analysis had shown that it was much too small to produce the thrust required for propulsion when operating at the conditions for high efficiency. $C_{D,e}$ represents the resultant drag of the configuration and is obtained by subtracting the drag measured with the propeller operating from the drag of the basic hull with the propeller removed. $C_{D,0}$ then represents the total

L
1
6
1
8

effective thrust applied to the airship by the propeller. For a value

of $\frac{C_{D,e}}{C_{D,o}} = 1.0$, the resultant thrust of the configuration is equal to

the drag; so the configuration is considered to be in a steady-state cruise condition. For the aforementioned thrust conditions, the propeller efficiencies were determined and are shown as a function of advance ratio in figure 8. For the steady-state condition ($T_e = D_o$), the maximum propeller efficiency is seen to be about 122 percent for propeller 1 and about 73 percent for the conventional-mounted and fin-mounted propellers. Only one blade angle was tested for the conventional-propeller installation, but the efficiencies for the various power conditions at $\beta = 20^\circ$ are quite similar for both the fin-mounted and the conventional-mounted propellers; so it is assumed that the fin-mounted propeller will provide an adequate basis of comparison for the wake-propeller configuration.

The data of figure 8 show that for the case of $T_e = D_o$ the efficiency of the stern propeller is well below its maximum value and that the efficiency is higher for the lower values of thrust ($T_e = 0.75D_o$, $T_e = 0.50D_o$, and $T_e = 0.25D_o$). This fact indicates that the propeller was too small for most efficient propulsion of this airship. Since the attainment of the very high efficiencies of stern propellers is critically dependent upon keeping the propeller largely in the hull wake, it seems that the loading of this propeller should be reduced by increasing the solidity rather than by increasing the propeller diameter.

So far the discussion has dealt only with propeller efficiencies; however, in order to determine whether these very high efficiencies of the stern propeller are indicative of the effectiveness of the propeller in propelling the airship or whether they are obtained at the expense of some other factor, such as an increase in hull drag, the data have also been reduced to the form of propulsive efficiency η_e . The values of propulsive efficiency were determined for thrust conditions of $T_e = D_o$, $T_e = 0.75D_o$, and $T_e = 0.50D_o$ and are presented in figure 9. The maximum propulsive efficiency of the stern-propeller installation at $T_e = D_o$ is about 103 percent as compared to a value of about 59 percent for the fin-mounted configuration. The reduction in values of efficiency from about 122 percent for propeller efficiency to about 103 percent for propulsive efficiency is in part attributed to the increase in pressure drag of the model with the stern propeller operating. This increase in hull drag with the stern propeller operating will be demonstrated later with the pressure-distribution data.

In order to show in another manner the relative merit of conventional-mounted- and fin-mounted-propeller installations with stern-mounted-propeller installations, the horsepower required to fly for various thrust conditions is shown in figure 10. A composite of these data is shown in figure 11. The stern-mounted propeller is seen to require considerably less horsepower to fly in a steady-state cruise condition than does either of the other configurations. From the viewpoint of reduced horsepower required and therefore increased propulsive efficiency, a stern-mounted-propeller installation would provide a configuration having greatly increased range and endurance as compared with a conventional-propeller configuration.

Propeller and Model Characteristics at Angle of Attack

The variation of the thrust and power coefficients with angle of attack for propeller 1 operating at a blade angle of 20° and the effect of elevator deflection on the propeller characteristics are shown in figure 12. Only the zero-elevator-deflection data are faired for purposes of clarity. Thrust and power for a given operating condition are seen to decrease with either plus or minus angle of attack. The decrease in thrust caused by angle of attack is, in general, considerably greater than that caused by elevator deflection. Therefore, it is surmised that the change with angle of attack of the airflow field (or wake) in which the propeller is operating caused the decrease in thrust. The decrease in power is, of course, caused by the decreased thrust. Elevator deflection is seen to have only minor effects on thrust and power.

The variation of the model aerodynamic characteristics with angle of attack with and without propeller operation at $\beta = 20^\circ$ is shown in figure 13. Propeller operation is seen to have negligible effect on all the forces and moments except, of course, the drag which is a direct function of thrust input.

The effect of elevator deflection on the airship aerodynamic characteristics for the same operating conditions noted in figure 13 is given in figure 14. Elevator effectiveness, as indicated by the range of deflection angles required for longitudinal trim, is about the same for all operating conditions.

Chordwise-Pressure-Distribution, Boundary-Layer

and Wake Characteristics

The pressure coefficients of the hull surface, the velocity, and the dynamic-pressure ratios in the hull boundary layer and wake are given

L
1
6
1
8

for all test conditions in tables 1 to 7. Some of the pressure-coefficient data, particularly the propeller-off data, are missing because the camera which photographed the manometer board malfunctioned during some of the tests.

The pressure coefficients of the aft portion of the hull surface are shown in figure 15 for the model with propeller 1 operating at various values of advance ratio. Pressure drag was not determined from this series of tests because the forward-pressure data are questionable as a result of camera malfunction. Unpublished data have shown, however, that the stern-mounted-propeller operation should not affect the pressure coefficients near the nose of the model; therefore, it is believed that the aft-pressure coefficients would show the general effect of propeller operation on the pressure drag. In general, the increased propeller rotational speed (fig. 15) increases the pressure drag as indicated by the pressure coefficients being, in general, less positive with increased rotational speed. This increase in hull pressure drag with increased propeller rotational speed, which means increased propeller thrust, ties in the previously demonstrated fact that the propulsive efficiency η_e is lower than the propeller efficiency η .

To show the general effect of propeller operation on the hull boundary-layer and wake characteristics over the aft portion of the hull, the boundary-layer and wake rakes and the velocity ratios existing at these rakes are shown with and without propeller 1 operating in figure 16. Propeller operation begins to decrease the boundary-layer thickness over the hull just forward of the port rake with this boundary-layer thickness becoming progressively much less toward and aft of the propeller plane. The boundary-layer or wake thickness is considered to extend outward from the hull or propeller-shaft axis to a point at which the velocity ratio (U_l/U_∞) is 0.9.

CONCLUDING REMARKS

The results of tests in the Langley full-scale tunnel to determine the propeller characteristics of a stern-mounted propeller (or wake propeller) on an airship model indicate that a stern-mounted propeller can be designed to operate at higher values of propulsive efficiency than those experienced by a conventional-mounted- or a fin-mounted-propeller installation. Because of the resulting decreased horsepower required for a given operating condition, the stern-propeller-airship configuration should have much greater range and endurance than a configuration

with a conventional-propeller arrangement. In general, propeller operation had only small effects on the model aerodynamic characteristics.

Langley Research Center,
National Aeronautics and Space Administration,
Langley Field, Va., June 26, 1961.

11618

TABLE 1
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER OFF INSTALLED WITH $\beta = 00$
 $\alpha = -0.5$

Sta- tion	y/h	u_1/u_∞	q_1/q_∞
Port rake	.0177	.4430	.1953
	.0443	.5045	.2540
	.0797	.5420	.2938
	.1507	.7270	.5280
	.2920	.8750	.7630
	.4340	.9880	.9780
	.5050	1.0090	1.0150
	.5750	1.0000	.9960
	.6460	1.0000	.9960
	.7180	1.0090	1.0150
St'b'd rake	.7890	1.0090	1.0150
	.8590	1.0180	1.0380
	.9300	1.0180	1.0380
	1.0000	1.0000	.9960
	.0177	.5940	.3520
	.0443	.6550	.4300
	.0797	.7530	.5670
	.1507	.8570	.7330
	.2920	.8750	.7630
	.4340	.9880	.9780
St'b'd hull	.5050	1.0090	1.0150
	.5750	1.0090	1.0150
	.6460	1.0000	.9960
	.7180	1.0000	.9960
	.7890	1.0090	1.0150
	.8590	1.0090	1.0150
	.9300	1.0090	1.0150
	1.0000	1.0120	1.0260

Sta- tion	x/l	C_p
Port hull		
St'b'd hull		

Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Wake rake	.0000	.4890	.2390
	.0833	.4500	.2020
	.1667	.5740	.3290
	.2081	.6300	.3960
	.2500	.7090	.5020
	.2919	.7600	.5770
	.3338	.8110	.6570
	.3750	.8600	.7390
	.4170	.8950	.7990
	.4580	.9190	.8430
	.5000	.9240	.8520
	.5420	.9250	.8540
	.5830	.9310	.8660
	.6250	.9610	.9230
	.6670	.9610	.9220
	.7080	.9550	.9100
	.7500	.9560	.9130
	.7900	.9610	.9220
	.8333	.9800	.9600
	.9170	.9870	.9730
1.0000	.9830	.9660	

TABLE 2
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(a) $n = 69.70$ rps $\frac{U}{nD} = 1.010$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0146	.592	Port rake	.0177	.4386	.1902	Wake rake	.0000	.4065	.1648
	.0633	.004		.0443	.5537	.3020		.0833	.6119	.3736
	.1120	-.127		.0797	.6315	.3937		.1667	.6858	.4693
	.1610	-.154		.1507	.7504	.5570		.2081	.7304	.5323
	.2100	-.196		.2920	.9358	.8658		.2500	.7807	.6080
	.2583	-.199		.4340	.9963	.9799		.2919	.8094	.6538
	.3075	-.199		.5050	1.0319	1.0515		.3338	.8462	.7144
	.3560	-.192		.5750	1.0267	1.0403		.3750	.8916	.7935
	.4050	-.185		.6460	1.0267	1.0425		.4170	.9310	.8648
	.4530	-.190		.7180	1.0252	1.0380		.4580	.9578	.9153
	.5020	-.161		.7890	1.0252	1.0380		.5000	.9597	.9190
	.5510	-.152		.8590	1.0536	1.0962		.5420	.9590	.9176
	.6000	-.114		.9300	1.0547	1.0984		.5830	.9581	.9158
	.6485	-.109		1.0000	1.0469	1.0828		.6250	.9879	.9736
	.6970	-.083	St'bd rake	.0177	.6135	.3714		.6670	.9864	.9708
	.7460	-.055		.0443	.7355	.5347		.7080	.9883	.9746
	.7950	-.035		.0797	.8063	.6421		.7500	.9869	.9718
	.8430	-.053		.1507	.9252	.8456		.7900	.9892	.9764
	.8920	.020		.2920	1.0319	1.0515		.8333	1.0140	1.0260
	.9410	.138		.4340	1.0307	1.0492		.9170	1.0108	1.0194
St'bd hull	.7800	-.024	St'bd rake	.5050	1.0416	1.0716		1.0000	1.0146	1.0274
	.8195	-.064		.5750	1.0427	1.0738				
	.8680	-.015		.6460	1.0440	1.0761				
	.9160	.080		.7180	1.0427	1.0738				
	.9650	.223		.7890	1.0440	1.0761				

TABLE 2 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(b) $n = 47.36$ rps $\frac{U}{nD} = .999$ $\alpha = -5.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_{∞}	q_1/q_{∞}	Sta- tion	z/h	U_1/U_{∞}	q_1/q_{∞}
Port hull	.0146	.595	Port rake	.0177	.4305	.1850	Wake rake	.0000	.3820	.1456
	.0633	-.030		.0443	.5325	.2800		.0833	.6129	.3749
	.1120	-.160		.0797	.6179	.3800		.1667	.6892	.4740
	.1610	-.190		.1507	.7532	.5650		.2081	.7343	.5380
	.2100	-.220		.2920	.9230	.8500		.2500	.7734	.5968
	.2583	-.220		.4340	.9874	.9700		.2919	.8062	.6485
	.3075	-.220		.5050	1.0329	1.0650		.3338	.8451	.7125
	.3560	-.210		.5750	1.0240	1.0450		.3750	.8916	.7931
	.4050	-.200		.6460	1.0209	1.0400		.4170	.9391	.8798
	.4530	-.205		.7180	1.0179	1.0350		.4580	.9646	.9284
	.5020	-.180		.7890	1.0240	1.0450		.5000	.9577	.9149
	.5510	-.160		.8590	1.0627	1.1250		.5420	.9614	.9221
	.6000	-.130		.9300	1.0593	1.1200		.5830	.9577	.9149
	.6485	-.120		1.0000	1.0534	1.1100		.6250	.9758	.9501
	.6970	-.097	St'bd hull	.0177	.5984	.3550		.6670	.9662	.9315
St'bd hull	.7460	-.075		.0443	.7279	.5300		.7080	.9737	.9459
	.7950	-.060		.0797	.8010	.6400		.7500	.9726	.9439
	.8430	-.070		.1507	.9291	.8600		.7900	.9774	.9531
	.8920	.000		.2920	1.0390	1.0750		.8333	1.0055	1.0089
	.9410	.130		.4340	1.0415	1.0850		.9170	.9983	.9945
	.7800	-.050		.5050	1.0444	1.0900		1.0000	1.0055	1.0089
	.8195	-.090		.5750	1.0415	1.0800				
	.8680	-.040		.6460	1.0444	1.0900				
	.9160	.060		.7180	1.0510	1.1000				
	.9650	.205		.7890	1.0510	1.1000				
				.8590	1.0510	1.1000				
				.9300	1.0534	1.1100				
				1.0000	1.0534	1.1100				

TABLE 2 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(C) $n = 75.00$ rps $\frac{U}{nD} = .943$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.604	Port rake	.0177	.4454	.1978	Wake rake	.0000	.4250	.1802
	.0633	.002		.0443	.5568	.3079		.0833	.6494	.4208
	.1120	-.125		.0797	.6388	.4045		.1667	.7245	.5237
	.1610	-.157		.1507	.7587	.5708		.2081	.7700	.5916
	.2100	-.197		.2920	.9411	.8764		.2500	.8130	.6594
	.2583	-.197		.4340	.9904	.9708		.2919	.8391	.7025
	.3075	-.197		.5050	1.0319	1.0539		.3338	.8704	.7558
	.3560	-.193		.5750	1.0264	1.0427		.3750	.9068	.8204
	.4050	-.177		.6460	1.0237	1.0382		.4170	.9426	.8864
	.4530	-.188		.7180	1.0237	1.0382		.4580	.9569	.9135
	.5020	-.161		.7890	1.0223	1.0337		.5000	.9581	.9159
	.5510	-.152		.8590	1.0466	1.0854		.5420	.9581	.9159
	.6000	-.116		.9300	1.0452	1.0831		.5830	.9586	.9169
	.6485	-.103		1.0000	1.0414	1.0742		.6250	.9920	.9819
	.6970	-.082						.6670	.9892	.9762
	.7460	-.053						.7080	.9913	.9805
	.7950	-.036						.7500	.9920	.9819
St'bd hull	.8430	-.053	St'bd rake	.0177	.6122	.3708		.7900	.9235	.9847
	.8920	.011		.0443	.7364	.5371		.8333	1.0168	1.0315
	.9410	.137		.0797	.8073	.6449		.9170	1.0180	1.0338
				.1507	.9293	.8539		1.0000	1.0198	1.0376
				.2920	1.0359	1.0629				
				.4340	1.0359	1.0629				
				.5050	1.0439	1.0787				
				.5750	1.0439	1.0787				
				.6460	1.0439	1.0787				
				.7180	1.0452	1.0809				
				.7890	1.0414	1.0742				
				.8590	1.0452	1.0831				
				.9300	1.0452	1.0831				
				1.0000	1.0466	1.0854				

TABLE 2 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(d) $n = 53.40$ rps $\frac{U}{nD} = .883$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.592	Port rake	.0177	.4319	.1841	Wake rake	.0000	.4270	.1819
	.0633	-.005		.0443	.5459	.2935		.0833	.6592	.4335
	.1120	-.144		.0797	.6260	.3881		.1667	.7481	.5582
	.1610	-.179		.1507	.7605	.5672		.2081	.7973	.6341
	.2100	-.213		.2920	.9222	.8408		.2500	.8281	.6841
	.2583	-.209		.4340	.9935	.9751		.2919	.8547	.7287
	.3075	-.204		.5050	1.0396	1.0647		.3338	.8804	.7735
	.3560	-.194		.5750	1.0329	1.0547		.3750	.9216	.8473
	.4050	-.194		.6460	1.0244	1.0348		.4170	.9500	.9003
	.4530	-.189		.7180	1.0274	1.0398		.4580	.9737	.9461
	.5020	-.174		.7890	1.0244	1.0348		.5000	.9705	.9399
	.5510	-.169		.8590	1.0569	1.1045		.5420	.9737	.9461
	.6000	-.145		.9300	1.0569	1.1045		.5830	.9658	.9305
	.6485	-.124		1.0000	1.0451	1.0796		.6250	.9935	.9846
St'bd hull	.6970	-.100	St'bd rake	.0177	.6057	.3582		.6670	.9882	.9742
	.7460	-.084		.0443	.7304	.5274		.7080	.9903	.9784
	.7950	-.054		.0797	.8109	.6468		.7500	.9891	.9762
	.8430	-.079		.1507	.9355	.8607		.7900	.9918	.9815
	.8920	-.014		.2920	1.0451	1.0796		.8333	1.0157	1.0292
	.9410	.129		.4340	1.0451	1.0796		.9170	1.0126	1.0230
				.5050	1.0569	1.0995		1.0000	1.0178	1.0334
				.5750	1.0569	1.1045				
St'bd hull	.7800	-.054		.6460	1.0569	1.1045				
	.8195	-.089		.7180	1.0569	1.0995				
	.8680	-.044		.7890	1.0569	1.1045				
	.9160	.044		.8590	1.0515	1.0896				
	.9650	.194		.9300	1.0545	1.0945				
				1.0000	1.0545	1.0945				

TABLE 2 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15$

(e) $n = 81.60$ rps $\frac{U}{nD} = .860$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0146	.622	Port rake	.0177	.4486	.1991	Wake rake	.0000	.4622	.2132
	.0633	.016		.0443	.5634	.3158		.0833	.6816	.4634
	.1120	-.109		.0797	.6412	.4096		.1667	.7762	.6011
	.1610	-.157		.1507	.7642	.5812		.2081	.8258	.6805
	.2100	-.192		.2920	.9479	.8947		.2500	.8655	.7473
	.2583	-.190		.4340	.9935	.9794		.2919	.8854	.7821
	.3075	-.189		.5050	1.0286	1.0503		.3338	.9059	.8186
	.3560	-.187		.5750	1.0229	1.0389		.3750	.9352	.8727
	.4050	-.178		.6460	1.0229	1.0389		.4170	.9544	.9088
	.4530	-.180		.7180	1.0229	1.0389		.4580	.9562	.9121
	.5020	-.155		.7890	1.0216	1.0366		.5000	.9582	.9159
	.5510	-.144		.8590	1.0449	1.0847		.5420	.9575	.9145
	.6000	-.112		.9300	1.0435	1.0824		.5830	.9589	.9174
	.6485	-.100		1.0000	1.0395	1.0732		.6250	.9925	.9829
	.6970	-.079						.6670	.9925	.9829
St'bd hull	.7460	-.054	St'bd rake	.0177	.6167	.3776		.7080	.9907	.9791
	.7950	-.034		.0443	.7359	.5378		.7500	.9927	.9834
	.8430	-.048		.0797	.8075	.6476		.7900	.9896	.9772
	.8920	.011		.1507	.9253	.8513		.8333	1.0193	1.0365
	.9410	.121		.2920	1.0255	1.0458		.9170	1.0197	1.0375
				.4340	1.0311	1.0572		1.0000	1.0207	1.0394
				.5050	1.0395	1.0732				
				.5750	1.0395	1.0732				
				.6460	1.0395	1.0732				
				.7180	1.0380	1.0709				

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TABLE 2 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(f) $n = 88.22$ rps $\frac{U}{nD} = .795$ $\alpha = -5.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0146	.608	Port rake	.0177	.4646	.2143	Wake rake	.0000	.4968	.2463
	.0633	.004		.0443	.5813	.3364		.0833	.7107	.5040
	.1120	-.126		.0797	.6567	.4309		.1667	.8335	.6932
	.1610	-.159		.1507	.7795	.6083		.2081	.8838	.7793
	.2100	-.195		.2920	.9560	.9124		.2500	.9184	.8415
	.2583	-.196		.4340	.9982	.9954		.2919	.9399	.8815
	.3075	-.195		.5050	1.0248	1.0507		.3338	.9535	.9072
	.3560	-.191		.5750	1.0222	1.0438		.3750	.9728	.9443
	.4050	-.184		.6460	1.0237	1.0461		.4170	.9610	.9214
	.4530	-.188		.7180	1.0237	1.0484		.4580	.9521	.9043
	.5020	-.161		.7890	1.0222	1.0438		.5000	.9485	.8976
	.5510	-.154		.8590	1.0496	1.1014		.5420	.9483	.8972
	.6000	-.115		.9300	1.0521	1.1060		.5830	.9505	.9015
	.6485	-.108		1.0000	1.0481	1.0968		.6250	.9815	.9614
	.6970	-.083						.6670	.9666	.9666
	.7460	-.057						.7080	.9853	.9685
St'bd hull	.7950	-.039	St'bd rake	.0177	.6212	.3848		.7500	.9866	.9714
	.8430	-.055		.0443	.7477	.5599		.7900	.9880	.9737
	.8920	.004		.0797	.8150	.6636		.8333	1.0162	1.0303
	.9410	.106		.1507	.9336	.8710		.9170	1.0166	1.0312
				.2920	1.0374	1.0760		1.0000	1.0166	1.0312
				.4340	1.0359	1.0737				
				.5050	1.0441	1.0899				
				.5750	1.0428	1.0876				
				.6460	1.0428	1.0876				
				.7180	1.0441	1.0899				
				.7890	1.0456	1.0922				
				.8590	1.0496	1.1014				
				.9300	1.0496	1.1014				
				1.0000	1.0496	1.1014				

TABLE 2 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(B) $n = 60.01$ rps $\frac{U}{nD} = .762$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u/U_∞	q_1/q_∞	Sta- tion	z/h	u/U_∞	q_1/q_∞
Port hull	.0146	.614	Port rake	.0177	.4553	.2030	Wake rake	.0000	.4778	.2278
	.0633	.000		.0443	.5656	.3198		.0833	.6995	.4882
	.1120	-.126		.0797	.6479	.4213		.1667	.8206	.6719
	.1610	-.172		.1507	.7792	.6041		.2081	.8686	.7527
	.2100	-.208		.2920	.9634	.9239		.2500	.8960	.8010
	.2583	-.213		.4340	1.0227	1.0406		.2919	.9175	.8399
	.3075	-.218		.5050	1.0380	1.0761		.3338	.9307	.8640
	.3560	-.203		.5750	1.0355	1.0711		.3750	.9600	.9197
	.4050	-.182		.6460	1.0355	1.0660		.4170	.9580	.9155
	.4530	-.192		.7180	1.0355	1.0660		.4580	.9694	.9375
	.5020	-.157		.7890	1.0355	1.0711		.5000	.9612	.9217
	.5510	-.162		.8590	1.0597	1.1168		.5420	.9672	.9333
	.6000	-.145		.9300	1.0597	1.1168		.5830	.9672	.9333
	.6485	-.132		1.0000	1.0567	1.1117		.6250	.9961	.9900
St'bd hull	.6970	-.108	St'bd rake	.0177	.6290	.3909		.6670	.9887	.9752
	.7460	-.086		.0443	.7383	.5431		.7080	.9931	.9836
	.7950	-.091		.0797	.8077	.6497		.7500	.9914	.9805
	.8430	-.066		.1507	.9401	.8832		.7900	.9961	.9900
	.8920	-.010		.2920	1.0355	1.0660		.8333	1.0135	1.0246
	.9410	.106		.4340	1.0380	1.0761		.9170	1.0160	1.0299
	.7800	-.040		.5050	1.0532	1.1066		1.0000	1.0144	1.0267
	.8195	-.106		.5750	1.0501	1.0964				
	.8680	-.045		.6460	1.0567	1.1117				
	.9160	.040		.7180	1.0501	1.1015				
	.9650	.177		.7890	1.0532	1.1066				
				.8590	1.0501	1.1015				
				.9300	1.0501	1.0964				
				1.0000	1.0532	1.1066				

TABLE 2 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(h) $n = 95.20$ rps $\frac{U}{ND} = .737$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u/U_∞	q_1/q_∞	Sta- tion	z/h	u/U_∞	q_1/q_∞
Port hull	.0146	.628	Port rake	.0177	.4645	.2148	Wake rake	.0000	.5261	.2762
	.0633	.025		.0443	.5861	.3441		.0833	.7314	.5337
	.1120	-.103		.0797	.6612	.4388		.1667	.8812	.7746
	.1610	-.150		.1507	.7793	.6074		.2081	.9306	.8640
	.2100	-.177		.2920	.9590	.9215		.2500	.9588	.9172
	.2583	-.183		.4340	.9994	1.0000		.2919	.9809	.9600
	.3075	-.189		.5050	1.0301	1.0647		.3338	.9930	.9837
	.3560	-.177		.5750	1.0274	1.0577		.3750	1.0068	1.0114
	.4050	-.177		.6460	1.0246	1.0531		.4170	.9437	.8887
	.4530	-.182		.7180	1.0235	1.0508		.4580	.9427	.8868
	.5020	-.154		.7890	1.0235	1.0508		.5000	.9420	.8854
	.5510	-.145		.8590	1.0439	1.0924		.5420	.9432	.8877
	.6000	-.113		.9300	1.0439	1.0924		.5830	.9430	.8873
	.6485	-.101		1.0000	1.0399	1.0831		.6250	.9809	.9600
St'bd hull	.6970	-.076	St'bd rake	.0177	.6211	.3857		.6670	.9834	.9647
	.7460	-.048		.0443	.7378	.5473		.7080	.9831	.9643
	.7950	-.032		.0797	.8063	.6513		.7500	.9826	.9633
	.8430	-.050		.1507	.9198	.8476		.7900	.9867	.9714
	.8920	.011		.2920	1.0246	1.0531		.8333	1.0117	1.0213
	.9410	.108		.4340	1.0290	1.0600		.89170	1.0125	1.0228
	.7800	-.020		.5050	1.0357	1.0762		1.0000	1.0129	1.0237
	.8195	-.067		.5750	1.0384	1.0808				
	.8680	-.020		.6460	1.0357	1.0762				
	.9160	.057		.7180	1.0357	1.0762				
	.9650	.173		.7890	1.0357	1.0762				
				.8590	1.0384	1.0808				
				.9300	1.0371	1.0785				
				1.0000	1.0399	1.0831				

TABLE 2 Continued

CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(1) $n = 66.63$ rps $\frac{U_\infty}{nD} = .702$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.637	Port rake	.0177	.4568	.2041	Wake rake	.0000	.5328	.2833
	.0633	.005		.0443	.5939	.3520		.0833	.7458	.5549
	.1120	-.132		.0797	.6558	.4286		.1667	.8956	.8001
	.1610	-.183		.1507	.7906	.6224		.2081	.9445	.8900
	.2100	-.234		.2920	.9568	.9133		.2500	.9705	.9397
	.2583	-.234		.4340	1.0111	1.0153		.2919	.9835	.9650
	.3075	-.234		.5050	1.0329	1.0612		.3338	.9943	.9862
	.3560	-.209		.5750	1.0298	1.0561		.3750	1.0154	1.0285
	.4050	-.193		.6460	1.0206	1.0357		.4170	.9540	.9079
	.4530	-.214		.7180	1.0173	1.0306		.4580	.9644	.9280
	.5020	-.183		.7890	1.0206	1.0357		.5000	.9573	.9143
	.5510	-.173		.8590	1.0657	1.1276		.5420	.9655	.9302
St'bd hull	.6000	-.137	St'bd rake	.9300	1.0657	1.1327		.5830	.9562	.9122
	.6485	-.132		1.0000	1.0657	1.1276		.6250	.9974	.9925
	.6970	-.101		.0177	.5895	.3469		.6670	.9921	.9820
	.7460	-.071		.0443	.7242	.5204		.7080	.9953	.9884
	.7950	-.056		.0797	.7906	.6224		.7500	.9921	.9820
	.8430	-.091		.1507	.9056	.8163		.7900	.9947	.9873
	.8920	-.030		.2920	1.0390	1.0765		.8333	1.0221	1.0422
	.9410	.066		.4340	1.0329	1.0612		.9170	1.0221	1.0422
	.7800	-.051		.5050	1.0538	1.1071		1.0000	1.0252	1.0486
	.8195	-.107		.5750	1.0512	1.0969				
	.8680	-.030		.6460	1.0512	1.0969				
	.9160	.015		.7180	1.0512	1.0969				
	.9650	.122		.7890	1.0538	1.1020				
				.8590	1.0538	1.1020				
				.9300	1.0568	1.1122				
				1.0000	1.0538	1.1071				

TABLE 2 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15$

(j) $n = 101.90$ rps $\frac{U}{nD} = .685$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.605	Port rake	.0177	.4672	.2207	Wake rake	.0000	.5648	.3183
	.0633	-.002		.0443	.5870	.3474		.0833	.7705	.5923
	.1120	-.131		.0797	.6604	.4390		.1667	.9487	.8981
	.1610	-.159		.1507	.7783	.6103		.2081	.9988	.9952
	.2100	-.204		.2920	.9495	.9085		.2500	1.0171	1.0322
	.2583	-.208		.4340	1.0069	1.0211		.2919	1.0386	1.0764
	.3075	-.211		.5050	1.0350	1.0775		.3338	1.0478	1.0952
	.3560	-.194		.5750	1.0264	1.0610		.3750	1.0557	1.1120
	.4050	-.192		.6460	1.0264	1.0610		.4170	.9414	.8842
	.4530	-.197		.7180	1.0249	1.0587		.4580	.9464	.8938
	.5020	-.166		.7890	1.0264	1.0610		.5000	.9459	.8928
	.5510	-.154		.8590	1.0525	1.1150		.5420	.9452	.8914
	.6000	-.122		.9300	1.0486	1.1080		.5830	.9487	.8981
	.6485	-.112		1.0000	1.0459	1.1009		.6250	.9888	.9755
	.6970	-.900	St'bd rake	.0177	.6205	.3872		.6670	.9895	.9770
	.7460	-.065		.0443	.7405	.5516		.7080	.9873	.9726
	.7950	-.051		.0797	.8092	.6596		.7500	.9881	.9741
	.8430	-.065		.1507	.9251	.8615		.7900	.9883	.9745
	.8920	-.014		.2920	1.0361	1.0798		.8333	1.0153	1.0283
	.9410	.084		.4340	1.0350	1.0775		.9170	1.0171	1.0322
				.5050	1.0417	1.0915		1.0000	1.0162	1.0303
St'bd hull	.7800	-.039	St'bd rake	.5750	1.0431	1.0962				
	.8195	-.077		.6460	1.0431	1.0962				
	.8680	-.037		.7180	1.0444	1.0986				
	.9160	.035		.7890	1.0431	1.0962				
	.9650	.140		.8590	1.0470	1.1033				
				.9300	1.0470	1.1033				
				1.0000	1.0444	1.0986				

TABLE 2 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(K) $n = 73.33$ rps $\frac{U}{nD} = .641$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u/U_∞	q_1/q_∞	Sta- tion	z/h	u/U_∞	q_1/q_∞
Port hull	.0146	.581	Port rake	.0177	.4806	.2296	Wake rake	.0000	.5930	.3510
	.0633	-.020		.0443	.5815	.3418		.0833	.7904	.6234
	.1120	-.137		.0797	.6617	.4388		.1667	.9775	.9534
	.1610	-.183		.1507	.7983	.6378		.2081	1.0308	1.0604
	.2100	-.219		.2920	.9558	.9184		.2500	1.0505	1.1012
	.2583	-.223		.4340	1.0103	1.0255		.2919	1.0698	1.1421
	.3075	-.224		.5050	1.0404	1.0867		.3338	1.0738	1.1505
	.3560	-.209		.5750	1.0344	1.0765		.3750	1.0766	1.1567
	.4050	-.199		.6460	1.0404	1.0867		.4170	.9476	.8958
	.4530	-.199		.7180	1.0282	1.0612		.4580	.9590	.9178
	.5020	-.168		.7890	1.0344	1.0765		.5000	.9443	.8896
	.5510	-.168		.8590	1.0555	1.1173		.5420	.9558	.9116
	.6000	-.137		.9300	1.0555	1.1173		.5830	.9519	.9042
	.6485	-.127		1.0000	1.0520	1.1122		.6250	.9903	.9786
	.6970	-.122						.6670	.9812	.9608
St'bd hull	.7460	-.081	St'bd rake	.0177	.6122	.3776		.7080	.9887	.9755
	.7950	-.061		.0443	.7544	.5714		.7500	.9844	.9671
	.8430	-.086		.0797	.8140	.6684		.7900	.9882	.9744
	.8920	-.025		.1507	.9459	.8980		.8333	1.0150	1.0278
	.9410	.076		.2920	1.0465	1.0969		.9170	1.0170	1.0320
				.4340	1.0490	1.1020		1.0000	1.0195	1.0373
	.7800	-.071		.5050	1.0490	1.1071				
	.8195	-.096		.5750	1.0609	1.1327				
	.8680	-.051		.6460	1.0555	1.1173				
	.9160	.010		.7180	1.0490	1.1071				
	.9650	.112		.7890	1.0555	1.1173				
				.8590	1.0555	1.1173				
				1.0000	1.0555	1.1173				
					1.0609	1.1276				

8191-1

L-1618

TABLE 2 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15^\circ$

(1) $n = 80.02$ rps $\frac{U}{nD} = .583$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0146	.609	Port rake	.0177	.4840	.2335	Wake rake	.0000	.6550	.4281
	.0533	.000		.0443	.6069	.3604		.0833	.8725	.7595
	.1120	-.142		.0797	.6750	.4518		.1667	1.0822	1.1685
	.1510	-.152		.1507	.8164	.6548		.2081	1.1321	1.2789
	.2100	-.198		.2920	.9854	.9543		.2500	1.1453	1.3087
	.2583	-.195		.4340	1.0288	1.0457		.2919	1.1582	1.3385
	.3075	-.192		.5050	1.0564	1.1015		.3338	1.1508	1.3214
	.3560	-.192		.5750	1.0594	1.1066		.3750	1.1429	1.3034
	.4050	-.187		.6460	1.0564	1.1015		.4170	.9503	.9007
	.4530	-.192		.7180	1.0441	1.0761		.4580	.9651	.9294
	.5020	-.162		.7890	1.0415	1.0660		.5000	.9575	.9146
	.5510	-.137		.8590	1.0659	1.1168		.5420	.9597	.9188
	.6000	-.121		.9300	1.0594	1.1066		.5830	.9603	.9199
	.6485	-.121		1.0000	1.0594	1.1066		.6250	.9968	.9910
St'd hull	.6970	-.094	St'd rake	.0177	.6166	.3756		.6670	.9903	.9784
	.7460	-.071		.0443	.7596	.5685		.7080	.9924	.9826
	.7950	-.060		.0797	.8197	.6650		.7500	.9860	.9699
	.8430	-.071		.1507	.9558	.8985		.7900	.9913	.9805
	.8920	-.030		.2920	1.0538	1.0914		.8333	1.0194	1.0367
	.9410	.040		.4340	1.0594	1.1066		.9170	1.0194	1.0367
	.7800	-.060		.5050	1.0683	1.1269		1.0000	1.0220	1.0421
	.8195	-.101		.5750	1.0683	1.1269				
	.8580	-.071		.6460	1.0629	1.1117				
	.9160	.005		.7180	1.0659	1.1168				

TABLE 2 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS

OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15$

(III) $n = 86.65$ rps $\frac{U}{nD} = .543$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0146	.596	Port rake	.0177	.5056	.2551	Wake rake	.0000	.7026	.4926
	.0633	-.020		.0443	.6278	.3929		.0833	.9213	.8470
	.1120	-.158		.0797	.6981	.4898		.1667	1.1559	1.3333
	.1610	-.168		.1507	.8324	.6939		.2081	1.2062	1.4515
	.2100	-.215		.2920	.9739	.9541		.2500	1.2178	1.4797
	.2583	-.213		.4340	1.0182	1.0408		.2919	1.2246	1.4964
	.3075	-.209		.5050	1.0481	1.1020		.3338	1.2096	1.4599
	.3550	-.193		.5750	1.0510	1.1122		.3750	1.1816	1.3929
	.4050	-.188		.6460	1.0426	1.0918		.4170	.9293	.8617
	.4530	-.180		.7180	1.0359	1.0816		.4580	.9461	.8930
	.5020	-.173		.7890	1.0333	1.0765		.5000	.9421	.8857
	.5510	-.163		.8590	1.0575	1.1224		.5420	.9388	.8795
	.6000	-.132		.9300	1.0575	1.1224		.5830	.9382	.8784
	.6435	-.132		1.0000	1.0600	1.1276		.6250	.9808	.9600
	.6970	-.120						.6670	.9750	.9485
St'bd hull	.7460	-.086	St'bd rake	.0177	.6073	.3724		.7080	.9787	.9558
	.7950	-.076		.0443	.7418	.5510		.7500	.9728	.9443
	.8430	-.096		.0797	.8254	.6837		.7900	.9799	.9579
	.8920	-.051		.1507	.9550	.9184		.8333	1.0046	1.0071
	.9410	.020		.2920	1.0575	1.1224		.9170	1.0094	1.0164
				.4340	1.0600	1.1276		1.0000	1.0072	1.0122
				.5050	1.0600	1.1276				
				.5750	1.0600	1.1327				
				.6460	1.0600	1.1276				
				.7180	1.0600	1.1327				
				.7890	1.0629	1.1378				
				.8590	1.0510	1.1122				
				.9300	1.0545	1.1173				
				1.0000	1.0545	1.1173				

L-161B

TABLE 2 Concluded
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 15$

(n) $n = 93.41$ rps $\frac{U}{nD} = .502$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.593	Port rake	.0177	.5315	.2792	Wake rake	.0000	.7684	.5890
	.0633	-.020		.0443	.6388	.4061		.0833	1.0065	1.0108
	.1120	-.157		.0797	.7173	.5127		.1667	1.2546	1.5705
	.1610	-.167		.1507	.8461	.7107		.2081	1.3093	1.7103
	.2100	-.213		.2920	.9928	.9797		.2500	1.3138	1.7219
	.2583	-.218		.4340	1.0334	1.0609		.2919	1.3113	1.7156
	.3075	-.223		.5050	1.0607	1.1168		.3338	1.2890	1.6578
	.3560	-.208		.5750	1.0577	1.1117		.3750	1.2313	1.5125
	.4050	-.187		.6460	1.0486	1.0914		.4170	.9287	.8604
	.4530	-.177		.7180	1.0390	1.0761		.4580	.9389	.8794
	.5020	-.167		.7890	1.0512	1.0964		.5000	.9281	.8594
	.5510	-.162		.8590	1.0577	1.1117		.5420	.9338	.8699
	.6000	-.137		.9300	1.0577	1.1117		.5830	.9287	.8604
	.6485	-.137		1.0000	1.0607	1.1168		.6250	.9730	.9446
St'bd hull	.6970	-.116	St'bd rake	.0177	.6135	.3756		.6670	.9605	.9204
	.7460	-.066		.0443	.7517	.5635		.7080	.9751	.9488
	.7950	-.045		.0797	.8240	.6751		.7500	.9730	.9446
	.8430	-.081		.1507	.9544	.9086		.7900	.9757	.9499
	.8920	-.035		.2920	1.0577	1.1117		.8333	1.0034	1.0045
	.9410	.005		.4340	1.0512	1.1015		.9170	1.0081	1.0139
				.5050	1.0631	1.1269		1.0000	1.0050	1.0077
	.7800	-.045		.5750	1.0607	1.1168				
	.8195	-.106		.6460	1.0607	1.1168				
	.8680	-.066		.7180	1.0631	1.1218				
	.9160	-.015		.7890	1.0631	1.1218				
	.9650	.015		.8590	1.0661	1.1320				
				.9300	1.0691	1.1371				
				1.0000	1.0631	1.1218				

TABLE 3
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20^\circ$

(a) $n = 52.15$ rps $\frac{U_e}{nD} = 1.351$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0146	.592	Port rake	.0177	.4213	.1748	Wake rake	.0000	.4072	.1654
	.0633	.008		.0443	.5367	.2832		.0833	.4891	.2388
	.1120	-.115		.0797	.6157	.3717		.1667	.5992	.3583
	.1610	-.150		.1507	.7382	.5354		.2081	.6609	.4357
	.2100	-.192		.2920	.9263	.8429		.2500	.7262	.5261
	.2583	-.193		.4340	.9828	.9491		.2919	.7708	.5929
	.3075	-.194		.5050	1.0188	1.0199		.3338	.8160	.6642
	.3560	-.177		.5750	1.0146	1.0133		.3750	.8667	.7496
	.4050	-.168		.6460	1.0188	1.0199		.4170	.9140	.8334
	.4530	-.158		.7180	1.0188	1.0199		.4580	.9548	.9096
	.5020	-.148		.7890	1.0173	1.0177		.5000	.9627	.9248
	.5510	-.139		.8590	1.0469	1.0774		.5420	.9627	.9248
	.6000	-.104		.9300	1.0444	1.0730		.5830	.9633	.9257
	.6485	-.097		1.0000	1.0444	1.0708		.6250	.9967	.9910
St'bd hull	.6970	-.072	St'bd rake	.0177	.6112	.3673		.6670	.9969	.9916
	.7460	-.048		.0443	.7328	.5288		.7080	.9952	.9884
	.7950	-.028		.0797	.8033	.6350		.7500	.9978	.9934
	.8430	-.042		.1507	.9217	.8341		.7900	.9941	.9860
	.8920	.022		.2920	1.0255	1.0332		.8333	1.0213	1.0407
	.9410	.152		.4340	1.0255	1.0332		.9170	1.0201	1.0383
				.5050	1.0378	1.0575		1.0000	1.0219	1.0421
				.5750	1.0363	1.0553				
				.6460	1.0335	1.0509				
				.7180	1.0363	1.0553				

TABLE 3 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20^\circ$

(b) $n = 35.99$ rps $\frac{U}{nD} = 1.314$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_{∞}	q_1/q_{∞}	Sta- tion	z/h	u_1/U_{∞}	q_1/q_{∞}
Port hull	.0146	.585	Port rake	.0177	.4136	.1750	Wake rake	.0000	.3733	.1390
	.0633	-.010		.0443	.5060	.2600		.0833	.5288	.2790
	.1120	-.125		.0797	.5840	.3450		.1667	.6263	.3914
	.1610	-.170		.1507	.7409	.5500		.2081	.6796	.4609
	.2100	-.200		.2920	.9309	.8750		.2500	.7340	.5375
	.2583	-.207		.4340	.9910	.9900		.2919	.7793	.6060
	.3075	-.215		.5050	1.0276	1.0650		.3338	.8216	.6734
	.3560	-.290		.5750	1.0305	1.0700		.3750	.8746	.7634
	.4050	-.290		.6460	1.0276	1.0600		.4170	.9220	.8482
	.4530	-.185		.7180	1.0216	1.0500		.4580	.9600	.9197
	.5020	-.170		.7890	1.0216	1.0500		.5000	.9585	.9167
	.5510	-.150		.8590	1.0479	1.1050		.5420	.9633	.9258
	.6000	-.135		.9300	1.0454	1.1000		.5830	.9622	.9237
	.6485	-.120		1.0000	1.0454	1.1000		.6250	.9843	.9666
	.6970	-.095						.6670	.9781	.9544
	.7460	-.070						.7080	.9816	.9616
St'bd hull	.7800	-.040	St'bd rake	.0177	.6047	.3700	St'bd rake	.7500	.9828	.9636
	.8195	-.085		.0443	.7409	.5500		.7900	.9843	.9666
	.8680	-.030		.0797	.7969	.6400		.8333	1.0044	1.0065
	.9160	.070		.1507	.9309	.8750		.9170	1.0029	1.0035
	.9650	.220		.2920	1.0336	1.0750		1.0000	1.0034	1.0045
				.4340	1.0390	1.0900				
				.5050	1.0508	1.1100				
				.5750	1.0454	1.1000				
				.6460	1.0390	1.0900				
				.7180	1.0508	1.1150				
				.7890	1.0508	1.1100				
				.8590	1.0390	1.0900				
				.9300	1.0454	1.1000				
				1.0000	1.0424	1.0950				

TABLE 3 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20$

(c) $n = 58.37$ rps $\frac{U}{ND} = 1.202$ $\alpha = -5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_l/U_∞	q_l/q_∞	Sta- tion	z/h	u_l/U_∞	q_l/q_∞
Port hull	.0146	.607	Port rake	.0177	.4366	.1896	Wake rake	.0000	.4290	.1836
	.0633	.018		.0443	.5546	.3047		.0833	.5516	.3036
	.1120	-.108		.0797	.6346	.3995		.1667	.6536	.4262
	.1610	-.144		.1507	.7515	.5598		.2081	.7140	.5087
	.2100	-.185		.2920	.9340	.6668		.2500	.7701	.5916
	.2583	-.182		.4340	.9939	.9797		.2919	.8110	.6563
	.3075	-.180		.5050	1.0242	1.0406		.3338	.8503	.7213
	.3560	-.176		.5750	1.0186	1.0293		.3750	.8923	.7944
	.4050	-.171		.6460	1.0227	1.0384		.4170	.9320	.8666
	.4530	-.171		.7180	1.0161	1.0248		.4580	.9581	.9158
	.5020	-.151		.7890	1.0200	1.0316		.5000	.9649	.9289
	.5510	-.140		.8590	1.0470	1.0880		.5420	.9647	.9284
	.6000	-.103		.9300	1.0457	1.0858		.5830	.9661	.9312
	.6485	-.090		1.0000	1.0443	1.0813		.6250	.9979	.9935
	.6970	-.066	St'bd hull	.0177	.6102	.3702		.6670	.9991	.9959
	.7460	-.040		.0443	.7326	.5327		.7080	.9972	.9921
	.7950	-.018		.0797	.8037	.6411		.7500	.9989	.9953
	.8430	-.038		.1507	.9190	.8375		.7900	.9979	.9935
	.8920	.024		.2920	1.0242	1.0406		.8333	1.0221	1.0422
	.9410	.144		.4340	1.0255	1.0429		.9170	1.0221	1.0422
	.7800	-.013		.5050	1.0324	1.0587		1.0000	1.0221	1.0422
	.8195	-.051		.5750	1.0335	1.0609				
	.8680	-.011		.6460	1.0403	1.0745				
	.9160	.081		.7180	1.0351	1.0632				
	.9650	.223		.7890	1.0364	1.0655				
				.8590	1.0389	1.0722				
				.9300	1.0403	1.0745				
				1.0000	1.0403	1.0745				

TABLE 3 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20$

(d) $n = 41.61$ rps $\frac{U}{nD} = 1.137$ $\alpha = -5$						
Station	x/l	C_p	Station	y/h	u_1/U_∞	q_1/q_∞
Port hull	.0146	.606	Port rake	.0177	.4048	.1602
	.0633	-.009		.0443	.5298	.2718
	.1120	-.140		.0797	.6098	.3641
	.1610	-.150		.1507	.7539	.5774
	.2100	-.213		.2920	.9242	.8353
	.2583	-.204		.4340	.9910	.9612
	.3075	-.194		.5050	1.0424	1.0631
	.3560	-.184		.5750	1.0305	1.0388
	.4050	-.169		.6460	1.0336	1.0437
	.4530	-.165		.7180	1.0336	1.0437
	.5020	-.160		.7890	1.0305	1.0388
	.5510	-.135		.8590	1.0508	1.0825
	.6000	-.116		.9300	1.0508	1.0825
	.6485	-.097		1.0000	1.0479	1.0728
	.6970	-.078				
	.7460	-.063				
St'bd hull	.7950	-.038	St'bd rake	.0177	.6205	.3738
	.8430	-.048		.0443	.7450	.5437
	.8920	.029		.0797	.8160	.6505
	.9410	.135		.1507	.9407	.8641
				.2920	1.0537	1.0874
				.4340	1.0454	1.0680
				.5050	1.0454	1.0680
				.5750	1.0479	1.0728
				.6460	1.0454	1.0680
				.7180	1.0390	1.0583
				.7890	1.0508	1.0777
				.8590	1.0537	1.0874
				.9300	1.0537	1.0874
				1.0000	1.0508	1.0777

TABLE 3 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20$

(e) $n = 64.99$ rps $\frac{U}{nD} = 1.082$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0146	.616	Port rake	.0177	.4356	.1896	Wake rake	.0000	.4409	.1940
	.0633	.013		.0443	.5633	.3160		.0833	.6168	.3796
	.1120	-.103		.0797	.6266	.3928		.1667	.7421	.5494
	.1610	-.142		.1507	.7480	.5576		.2081	.8023	.6422
	.2100	-.182		.2920	.9292	.8600		.2500	.8460	.7140
	.2583	-.183		.4340	.9872	.9729		.2919	.8856	.7826
	.3075	-.182		.5050	1.0178	1.0339		.3338	.9165	.8381
	.3560	-.182		.5750	1.0151	1.0271		.3750	.9458	.8927
	.4050	-.164		.6460	1.0178	1.0316		.4170	.9766	.9514
	.4530	-.171		.7180	1.0205	1.0384		.4580	.9550	.9099
	.5020	-.146		.7890	1.0164	1.0293		.5000	.9557	.9113
	.5510	-.135		.8590	1.0420	1.0835		.5420	.9560	.9118
	.6000	-.103		.9300	1.0420	1.0835		.5830	.9577	.9150
	.6485	-.097		1.0000	1.0396	1.0767		.6250	.9950	.9878
	.6970	-.090						.6670	.9956	.9892
	.7460	-.047	St'bd hull	.0177	.6130	.3747		.7080	.9939	.9855
St'bd hull	.7950	-.018		.0443	.7331	.5350		.7500	.9956	.9892
	.8430	-.033		.0797	.8057	.6479		.7900	.9939	.9855
	.8920	.024		.1507	.9187	.8420		.8333	1.0182	1.0345
	.9410	.128		.2920	1.0205	1.0384		.89170	1.0205	1.0391
				.4340	1.0219	1.0406		1.0000	1.0192	1.0363
				.5050	1.0313	1.0609				
				.5750	1.0342	1.0655				
				.6460	1.0301	1.0564				
				.7180	1.0313	1.0609				
				.7890	1.0313	1.0609				
				.8590	1.0355	1.0677				
				.9300	1.0342	1.0655				
				1.0000	1.0396	1.0767				

TABLE 3 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20^\circ$

(f) $n = 48.38$ rps $\frac{U_\infty}{nD} = .978$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0146	-.607	Port rake	.0177	.4491	.2040	Wake rake	.0000	.3678	.1349
	.0633	-.005		.0443	.5689	.3234		.0833	.6147	.3771
	.1120	-.144		.0797	.6489	.4229		.1667	.7668	.5865
	.1610	-.169		.1507	.7687	.5920		.2081	.8315	.6897
	.2100	-.203		.2920	.9537	.9104		.2500	.8611	.7398
	.2583	-.204		.4340	1.3064	1.0149		.2919	.9120	.8298
	.3075	-.204		.5050	1.0336	1.0697		.3338	.9336	.8696
	.3560	-.204		.5750	1.0336	1.0697		.3750	.9612	.9217
	.4050	-.184		.6460	1.0360	1.0746		.4170	.9962	.9902
	.4530	-.179		.7180	1.0305	1.0647		.4580	.9660	.9310
	.5020	-.174		.7890	1.0336	1.0697		.5000	.9585	.9167
	.5510	-.154		.8590	1.0537	1.1144		.5420	.9622	.9237
	.6000	-.164		.9300	1.0537	1.1144		.5830	.9622	.9237
	.6485	-.114		1.0000	1.0424	1.0896		.6250	.9823	.9626
St'bd hull	.6970	-.104	St'bd rake	.0177	.6047	.3682	St'bd rake	.6670	.9766	.9514
	.7460	-.074		.0443	.7368	.5423		.7080	.9766	.9514
	.7950	-.034		.0797	.8122	.6617		.7500	.9802	.9585
	.8430	-.059		.1507	.9440	.8955		.7900	.9802	.9585
	.8920	-.014		.2920	1.0479	1.0995		.8333	1.0034	1.0045
	.9410	.109		.4340	1.0390	1.0846		.9170	1.0019	1.0015
				.5050	1.0508	1.1095		1.0000	1.0029	1.0035
				.5750	1.0479	1.0995				
				.6460	1.0454	1.0945				
				.7180	1.0454	1.0945				

TABLE 3 Continued
CHORDWISE PRESSURE--DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20$

(ξ) $n = 71.66$ rps $\frac{U}{ND} = .976$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_{∞}	q_1/q_{∞}	Sta- tion	z/h	u_1/u_{∞}	q_1/q_{∞}
Port hull	.0146	.623	Port rake	.0177	.4590	.2086	Wake rake	.0000	.4611	.2121
	.0633	.020		.0443	.5732	.3265		.0833	.6330	.3997
	.1120	-.113		.0797	.6509	.4218		.1667	.7920	.6259
	.1610	-.147		.1507	.7733	.5941		.2081	.8514	.7233
	.2100	-.197		.2920	.9641	.9229		.2500	.8853	.7821
	.2583	-.195		.4340	1.0041	1.0023		.2919	.9264	.8563
	.3075	-.192		.5050	1.0289	1.0522		.3338	.9567	.9132
	.3560	-.197		.5750	1.0289	1.0522		.3750	.9839	.9659
	.4050	-.183		.6460	1.0247	1.0431		.4170	1.0078	1.0134
	.4530	-.172		.7180	1.0289	1.0499		.4580	.9533	.9067
	.5020	-.161		.7890	1.0289	1.0499		.5000	.9548	.9095
	.5510	-.151		.8590	1.0506	1.0952		.5420	.9548	.9095
	.6000	-.120		.9300	1.0520	1.0975		.5850	.9557	.9114
	.6485	-.113		1.0000	1.0464	1.0862		.6250	.9930	.9837
St'bd hull	.6970	-.084	St'bd rake	.0177	.6086	.3673		.6670	.9927	.9833
	.7460	-.059		.0443	.7245	.5215		.7080	.9924	.9829
	.7950	-.043		.0797	.7894	.6190		.7500	.9913	.9805
	.8430	-.056		.1507	.9131	.8277		.7900	.9927	.9833
	.8920	.000		.2920	1.0289	1.0522		.8333	1.0206	1.0393
	.9410	.111		.4340	1.0344	1.0612		.9170	1.0201	1.0383
				.5050	1.0410	1.0771		1.0000	1.0215	1.0411
	.7800	-.024		.5750	1.0423	1.0794				
	.8195	-.074		.6460	1.0410	1.0771				
	.8680	-.027		.7180	1.0398	1.0748				
	.9160	.052		.7890	1.0398	1.0726				
	.9650	.174		.8590	1.0464	1.0862				
				.9300	1.0453	1.0839				
				1.0000	1.0464	1.0862				

TABLE 3 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20^\circ$

(h) $n = 78.37$ rps $\frac{U}{nD} = .891$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_{∞}	q_1/q_{∞}	Sta- tion	z/h	u_1/u_{∞}	q_1/q_{∞}
Port hull	.0146	.601	Port rake	.0177	.4502	.2028	Wake rake	.0000	.4490	.2012
	.0633	.000		.0443	.5719	.3295		.0833	.6639	.4398
	.1120	-.124		.0797	.6437	.4171		.1667	.8549	.7293
	.1610	-.156		.1507	.7621	.5829		.2081	.9139	.8331
	.2100	-.198		.2920	.9378	.8848		.2500	.9366	.8752
	.2583	-.198		.4340	.9949	.9954		.2919	.9761	.9507
	.3075	-.198		.5050	1.0243	1.0553		.3338	1.0023	1.0022
	.3560	-.191		.5750	1.0228	1.0507		.3750	1.0247	1.0476
	.4050	-.179		.6460	1.0243	1.0553		.4170	1.0449	1.0892
	.4530	-.167		.7180	1.0243	1.0530		.4580	.9497	.8998
	.5020	-.161		.7890	1.0259	1.0576		.5000	.9506	.9017
	.5510	-.147		.8590	1.0446	1.0968		.5420	.9513	.9031
	.6000	-.124		.9300	1.0446	1.0968		.5830	.9518	.9040
	.6485	-.103		1.0000	1.0407	1.0876		.6250	.9897	.9773
	.6970	-.080	St'bd hull	.0177	.6170	.3825		.6670	.9899	.9777
St'bd hull	.7460	-.055		.0443	.7418	.5530		.7080	.9901	.9781
	.7950	-.032		.0797	.8141	.6659		.7500	.9887	.9753
	.8430	-.055		.1507	.9305	.8710		.7900	.9897	.9773
	.8920	.004		.2920	1.0311	1.0668		.8333	1.0180	1.0339
	.9410	.106		.4340	1.0298	1.0645		.9170	1.0170	1.0320
				.5050	1.0367	1.0783		1.0000	1.0185	1.0349
				.5750	1.0353	1.0760				
				.6460	1.0367	1.0783				
				.7180	1.0353	1.0760				
				.7890	1.0378	1.0829				
				.8590	1.0433	1.0945				
				.9300	1.0433	1.0945				
				1.0000	1.0433	1.0945				

TABLE 3 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20^\circ$

(1) $n = 55.00$ rps $\frac{U}{nD} = .860$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_h/u_∞	q_1/q_∞	Sta- tion	z/h	u_y/u_∞	q_1/q_∞
Port hull	.0146	.613	Port rake	.0177	.4679	.2126	Wake rake	.0000	.2519	.0633
	.0633	.004		.0443	.5740	.3188		.0833	.6898	.4747
	.1120	-.120		.0797	.6485	.4106		.1667	.9065	.8198
	.1610	-.164		.1507	.7926	.6087		.2081	.9654	.9300
	.2100	-.198		.2920	.9660	.9082		.2500	.9864	.9708
	.2583	-.198		.4340	1.0119	1.0000		.2919	1.0195	1.0373
	.3075	-.198		.5050	1.0501	1.0725		.3338	1.0410	1.0811
	.3560	-.178		.5750	1.0501	1.0725		.3750	1.0541	1.1086
	.4050	-.165		.6460	1.0473	1.0676		.4170	1.0429	1.0852
	.4530	-.159		.7180	1.0384	1.0483		.4580	.9510	.9025
	.5020	-.149		.7890	1.0449	1.0628		.5000	.9527	.9056
	.5510	-.125		.8590	1.0566	1.0870		.5420	.9489	.8984
	.6000	-.101		.9300	1.0532	1.0821		.5830	.9434	.8882
	.6485	-.073		1.0000	1.0705	1.1159		.6250	.9817	.9617
	.6970	-.043	St'bd hull	.0177	.6390	.3961		.6670	.9776	.9535
	.7460	-.033		.0443	.7610	.5652		.7080	.9790	.9565
	.7950	-.053		.0797	.8224	.6618		.7500	.9764	.9515
	.8430	-.009		.1507	.9590	.8937		.7900	.9790	.9565
	.8920	.096		.2920	1.0449	1.0628		.8333	1.0110	1.0199
	.9410			.4340	1.0473	1.0676		.9170	1.0095	1.0168
				.5050	1.0648	1.1014		1.0000	1.0100	1.0178
				.5750	1.0648	1.1014				
				.6460	1.0648	1.1014				
				.7180	1.0566	1.0870				
				.7890	1.0566	1.0870				
				.8590	1.0501	1.0725				
				.9300	1.0501	1.0773				
				1.0000	1.0501	1.0773				

TABLE 3 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20^\circ$

(j) $n = 85.02$ rps $\frac{U}{ND} = .822$ $\alpha = -5.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.625	Port rake	.0177	.4808	.2333	Wake rake	.0000	.4255	.1806
	.0633	.011		.0443	.5985	.3603		.0833	.7050	.4959
	.1120	-.115		.0797	.6698	.4527		.1667	.9324	.8674
	.1610	-.152		.1507	.7897	.6282		.2081	.9896	.9772
	.2100	-.184		.2920	.9637	.9330		.2500	1.0068	1.0111
	.2583	-.175		.4340	1.0010	1.0092		.2919	1.0433	1.0859
	.3075	-.182		.5050	1.0289	1.0647		.3338	1.0644	1.1304
	.3560	-.180		.5750	1.0208	1.0485		.3750	1.0781	1.1596
	.4050	-.170		.6460	1.0264	1.0600		.4170	1.0787	1.1610
	.4530	-.175		.7180	1.0208	1.0485		.4580	.9463	.8934
	.5020	-.150		.7890	1.0247	1.0577		.5000	.9463	.8934
	.5510	-.150		.8590	1.0491	1.1062		.5420	.9446	.8902
	.6000	-.115		.9300	1.0505	1.1109		.5830	.9471	.8949
	.6485	-.101		1.0000	1.0451	1.0993		.6250	.9841	.9663
	.6970	-.076	St'bd hull	.0177	.6219	.3880		.6670	.9849	.9677
	.7460	-.053		.0443	.7401	.5497		.7080	.9849	.9677
	.7950	-.025		.0797	.8075	.6559		.7500	.9841	.9663
	.8430	-.046		.1507	.9263	.8637		.7900	.9839	.9658
	.8920	-.004		.2920	1.0302	1.0670		.8333	1.0133	1.0244
	.9410	.094		.4340	1.0371	1.0808		.9170	1.0138	1.0253
	.7800	-.023		.5050	1.0426	1.0924		1.0000	1.0140	1.0259
	.8195	-.069		.5750	1.0357	1.0785				
	.8680	-.018		.6460	1.0412	1.0901				
	.9160	.039		.7180	1.0399	1.0878				
	.9650	.150		.7890	1.0426	1.0924				
				.8590	1.0437	1.0970				
				.9300	1.0437	1.0970				
				1.0000	1.0451	1.0993				

TABLE 3 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20^\circ$

(K) $n = 61.63$ rps $\frac{U}{nD} = .767$ $\alpha = -0.5^\circ$

Station	x/l	C_p
Port hull	.0146	.617
	.0633	-.035
	.1120	-.153
	.1610	-.193
	.2100	-.205
	.2583	-.215
	.3075	-.229
	.3560	-.224
	.4050	-.224
	.4530	-.219
	.5020	-.188
	.5510	-.178
	.6000	-.142
	.6485	-.132
	.6970	-.106
	.7460	-.081
St'bd hull	.7950	-.066
	.8430	-.086
	.8920	-.030
	.9410	.061
	.9650	.132

Station	y/h	U/U_∞	q_1/q_∞
Port rake	.0177	.4883	.2449
	.0443	.5837	.3520
	.0797	.6618	.4541
	.1507	.8003	.6582
	.2920	.9718	.9745
	.4340	1.0151	1.0612
	.5050	1.0449	1.1224
	.5750	1.0449	1.1224
	.6460	1.0384	1.1071
	.7180	1.0384	1.1122
	.7890	1.0566	1.1480
	.8590	1.0590	1.1531
	.9300	1.0566	1.1480
	1.0000		
St'bd rake	.0177	.6292	.4082
	.0443	.7569	.5867
	.0797	.8261	.7041
	.1507	.9532	.9337
	.2920	1.0618	1.1582
	.4340	1.0590	1.1531
	.5050	1.0501	1.1327
	.5750	1.0590	1.1531
	.6460	1.0566	1.1480
	.7180	1.0648	1.1633
	.7890	1.0590	1.1531
	.8590	1.0648	1.1633
	.9300	1.0618	1.1582
	1.0000	1.0648	1.1633

Station	z/h	U/U_∞	q_1/q_∞
Wake rake	.0000	.1865	.0347
	.0833	.7364	.5410
	.1667	.9776	.9535
	.2081	1.0355	1.0699
	.2500	1.0501	1.1005
	.2919	1.0834	1.1710
	.3338	1.0997	1.2067
	.3750	1.1080	1.2251
	.4170	1.0570	1.1148
	.4580	.9553	.9106
	.5000	.9521	.9045
	.5420	.9510	.9025
	.5830	.9473	.8954
	.6250	.9811	.9606
	.6670	.9740	.9463
	.7080	.9776	.9535
	.7500	.9776	.9535
	.7900	.9790	.9565
	.8333	1.0100	1.0178
	.9170	1.0085	1.0148
	1.0000	1.0135	1.0250

TABLE 3 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20$

(1) $n = 68.34$ rps $\frac{U}{nD} = .694$ $\alpha = -5.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.603	Port rake	.0177	.4982	.2513	Wake rake	.0000	.2277	.0518
	.0633	-.020		.0443	.6077	.3769		.0833	.7859	.6162
	.1120	-.160		.0797	.6789	.4724		.1667	1.0622	1.1257
	.1610	-.180		.1507	.8050	.6633		.2081	1.1191	1.2496
	.2100	-.200		.2920	.9789	.9749		.2500	1.1281	1.2699
	.2583	-.215		.4340	1.0241	1.0704		.2919	1.1575	1.3369
	.3075	-.226		.5050	1.0501	1.1256		.3338	1.1680	1.3613
	.3560	-.211		.5750	1.0501	1.1256		.3750	1.1636	1.3511
	.4050	-.206		.6460	1.0472	1.1206		.4170	1.0501	1.1004
	.4530	-.190		.7180	1.0355	1.0955		.4580	.9429	.8872
	.5020	-.175		.7890	1.0472	1.1156		.5000	.9370	.8760
	.5510	-.175		.8590	1.0560	1.1357		.5420	.9391	.8801
	.6000	-.140		.9300	1.0560	1.1357		.5830	.9375	.8771
	.6485	-.130		1.0000	1.0472	1.1206		.6250	.9774	.9532
St'bd hull	.6970	-.120	St'bd rake	.0177	.6184	.3869		.6670	.9732	.9450
	.7460	-.080		.0443	.7466	.5678		.7080	.9712	.9411
	.7950	-.050		.0797	.8280	.6985		.7500	.9722	.9430
	.8430	-.095		.1507	.9595	.9397		.7900	.9700	.9390
	.8920	-.030		.2920	1.0472	1.1206		.8333	1.0085	1.0151
	.9410	.050		.4340	1.0536	1.1307		.9170	1.0097	1.0172
				.5050	1.0501	1.1256		1.0000	1.0101	1.0181
	.7800	-.040		.5750	1.0501	1.1256				
	.8195	-.095		.6460	1.0501	1.1256				
	.8680	-.050		.7180	1.0560	1.1357				
	.9160	.005		.7890	1.0560	1.1357				
	.9650	.090		.8590	1.0501	1.1256				
				.9300	1.0536	1.1307				
				1.0000	1.0588	1.1407				

TABLE 3 Concluded
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 20^\circ$

(M) $n = 75.00$ rps $\frac{U}{ND} = .631$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.589	Port rake	.0177	.4992	.2475	Wake rake	.0000	.4686	.2191
	.0633	.000		.0443	.6089	.3713		.0833	.8722	.7592
	.1120	-.143		.0797	.6935	.4802		.1667	1.1776	1.3837
	.1610	-.173		.1507	.8147	.6634		.2081	1.2380	1.5294
	.2100	-.193		.2920	.9708	.9406		.2500	1.2352	1.5223
	.2583	-.195		.4340	1.0261	1.0495		.2919	1.2621	1.5896
	.3075	-.198		.5050	1.0345	1.0693		.3338	1.2617	1.5885
	.3560	-.193		.5750	1.0375	1.0792		.3750	1.2405	1.5355
	.4050	-.183		.6460	1.0345	1.0693		.4170	1.0090	1.0159
	.4530	-.183		.7180	1.0321	1.0644		.4580	.9344	.8712
	.5020	-.158		.7890	1.0261	1.0545		.5000	.9240	.8518
	.5510	-.143		.8590	1.0492	1.1040		.5420	.9334	.8691
	.6000	-.113		.9300	1.0555	1.1139		.5830	.9344	.8712
	.6485	-.104		1.0000	1.0555	1.1139		.6250	.9688	.9364
	.6970	-.079						.6670	.9677	.9344
	.7460	-.054						.7080	.9661	.9314
St'bd hull	.7800	-.039	St'bd rake	.0177	.6138	.3762		.7500	.9661	.9314
	.8195	-.094		.0443	.7562	.5743		.7900	.9681	.9354
	.8680	-.039		.0797	.8110	.6584		.8333	1.0064	1.0108
	.9160	-.005		.1507	.9490	.9010		.9170	1.0050	1.0077
	.9650	.059		.2920	1.0492	1.0990		1.0000	1.0070	1.0118
				.4340	1.0492	1.0990				
				.5050	1.0463	1.0941				
				.5750	1.0463	1.0941				
				.6460	1.0463	1.0941				
				.7180	1.0463	1.0941				
				.7890	1.0463	1.0941				
				.8590	1.0492	1.1040				
				.9300	1.0492	1.1040				
				1.0000	1.0555	1.1139				

TABLE 4

(a) $n = 43.65$ rps $\frac{U_p}{D} = 1.609$ $\alpha = -0.5$

Sta- tion	y/h	U_y/U_{∞}	q_y/q_{∞}
Port rate	.0177	.4311	.1818
	.0443	.5399	.2860
	.0797	.6232	.3836
	.1507	.7412	.5410
	.2920	.9259	.8426
	.4340	.9898	.9645
	.5050	1.0268	1.0377
	.5750	1.0199	1.0244
	.6460	1.0226	1.0288
	.7180	1.0226	1.0333
	.7890	1.0240	1.0333
	.8590	1.0534	1.0931
St'bd rate	.9300	1.0534	1.0931
	1.0000	1.0510	1.0865
	.0177	.6191	.3769
	.0443	.7465	.5477
	.0797	.8160	.6563
	.1507	.9394	.8692
	.2920	1.0292	1.0443
	.4340	1.0360	1.0576
	.5050	1.0456	1.0754
	.5750	1.0428	1.0710
	.6460	1.0442	1.0732
	.7180	1.0442	1.0732
Wake rate	.7890	1.0456	1.0754
	.8590	1.0481	1.0820
	.9300	1.0481	1.0820
	1.0000	1.0467	1.0798
	.0000	.7080	.9979
	.0833	.7500	1.0001
	.1667	.7900	.9980
	.2500	.8333	.9977
	.3338	.8750	.9932
	.4170	.9129	1.0001
	.5000	.9565	.9937
	.5830	.9977	.9932
Wake rate	.6670	1.0001	.9932
	.7500	.9977	1.0011
	.8333	.9932	1.0011
	.9129	.9932	1.0011
	.9977	.9932	1.0011
	1.0001	.9932	1.0011
	.0000	.9932	1.0011
	.0833	.9932	1.0011
	.1667	.9932	1.0011
	.2500	.9932	1.0011
	.3338	.9932	1.0011
	.4170	.9932	1.0011

Sta- tion	x/l	C_p
Port hull	.0146	.605
	.0633	.011
	.1120	-.115
	.1610	-.150
	.2100	-.181
	.2583	-.182
	.3075	-.181
	.3560	-.177
	.4050	-.168
	.4530	-.158
	.5020	-.148
	.5510	-.141
St'bd hull	.6000	-.108
	.6485	-.106
	.6970	-.071
	.7460	-.046
	.7950	-.026
	.8430	-.042
	.8920	.026
	.9410	.155
	.7800	-.011
	.8195	-.055
	.8680	-.011
	.9160	.086
.9650	.248	

TABLE 4 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS

OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25$

(b) $n = 46.63$ rps $\frac{U}{nD} = 1.505$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.605	Port wake	.0177	.4281	.1804	Wake wake	.0000	.4074	.1656
	.0633	-.002		.0443	.5450	.2940		.0833	.5433	.2944
	.1120	-.113		.0797	.6213	.3808		.1667	.6413	.4103
	.1610	-.144		.1507	.7530	.5590		.2081	.7027	.4926
	.2100	-.184		.2920	.9382	.8708		.2500	.7625	.5801
	.2583	-.186		.4340	.9888	.9666		.2919	.8065	.6489
	.3075	-.187		.5050	1.0219	1.0312		.3338	.8525	.7252
	.3560	-.178		.5750	1.0192	1.0245		.3750	.8965	.8020
	.4050	-.167		.6460	1.0247	1.0356		.4170	.9349	.8721
	.4530	-.162		.7180	1.0206	1.0290		.4580	.9560	.9117
	.5020	-.155		.7890	1.0233	1.0334		.5000	.9616	.9225
	.5510	-.142		.8590	1.0473	1.0846		.5420	.9606	.9205
	.6000	-.124		.9300	1.0463	1.0802		.5830	.9622	.9239
	.6485	-.104		1.0000	1.0396	1.0668		.6250	.9975	.9927
St'bd hull	.6970	-.077	St'bd wake	.0177	.6236	.3831		.6670	.9975	.9927
	.7460	-.046		.0443	.7418	.5434		.7080	.9959	.9894
	.7950	-.022		.0797	.8079	.6459		.7500	.9963	.9903
	.8430	-.037		.1507	.9367	.8664		.7900	.9933	.9843
	.8920	.024		.2920	1.0288	1.0445		.8333	1.0194	1.0368
	.9410	.140		.4340	1.0288	1.0445		.9170	1.0201	1.0382
				.5050	1.0353	1.0579		1.0000	1.0199	1.0378
				.5750	1.0367	1.0624				
				.6460	1.0396	1.0668				
				.7180	1.0382	1.0646				

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(c) $n = 32.01$ rps $\frac{U}{nD} = 1.467$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_{∞}	q_1/q_{∞}	Sta- tion	z/h	u_1/U_{∞}	q_1/q_{∞}
Port hull	.0146	.604	Port rake	.0177	.4004	.1584	Wake rake	.0000	.4192	.1753
	.0633	.000		.0443	.5205	.2673		.0833	.5726	.3270
	.1120	-.138		.0797	.6033	.3614		.1667	.6783	.4591
	.1610	-.183		.1507	.7528	.5594		.2081	.7283	.5292
	.2100	-.198		.2920	.9387	.8713		.2500	.7890	.6210
	.2583	-.203		.4340	1.0025	.9950		.2919	.8268	.6820
	.3075	-.207		.5050	1.0410	1.0743		.3338	.8707	.7563
	.3560	-.198		.5750	1.0385	1.0644		.3750	.9123	.8305
	.4050	-.193		.6460	1.0325	1.0545		.4170	.9496	.8997
	.4530	-.188		.7180	1.0291	1.0495		.4580	.9663	.9316
	.5020	-.158		.7890	1.0291	1.0495		.5000	.9593	.9182
	.5510	-.148		.8590	1.0621	1.1139		.5420	.9679	.9347
	.6000	-.118		.9300	1.0646	1.1238		.5830	.9874	.9729
	.6485	-.104		1.0000	1.0588	1.1089		.6250	1.0185	1.0348
St'bd hull	.6970	-.076	St'bd rake	.0177	.6177	.3762		.6670	1.0334	1.0658
	.7460	-.049		.0443	.7486	.5545		.7080	1.0163	1.0306
	.7950	-.039		.0797	.8198	.6634		.7500	1.0138	1.0254
	.8430	-.044		.1507	.9452	.8861		.7900	1.0092	1.0162
	.8920	.000		.2920	1.0385	1.0693		.8333	1.0295	1.0575
	.9410	.158		.4340	1.0385	1.0644		.9170	1.0396	1.0781
				.5050	1.0646	1.1188		1.0000	1.0265	1.0512
	.7800	-.024		.5750	1.0621	1.1139				
	.8195	-.079		.6460	1.0646	1.1238				
	.8680	-.039		.7180	1.0646	1.1188				
	.9160	.064		.7890	1.0646	1.1188				
	.9650	.222		.8590	1.0528	1.0990				
				.9300	1.0557	1.1040				
				1.0000	1.0557	1.1040				

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25$

(d) $n = 50.00$ rps $\frac{U}{nD} = 1.400$ $\alpha = -0.5$

Station	x/l	C_p	Station	y/h	u_1/U_∞	q_1/q_∞	Station	z/h	u_1/U_∞	q_1/q_∞
Port hull	.6146	.612	Port rake	.0177	.4364	.1892	Wake rake	.0000	.4177	.1742
	.6633	.006		.0443	.5568	.3086		.0833	.5698	.3239
	.1120	-.119		.0797	.6366	.4009		.1667	.6745	.4540
	.1610	-.157		.1507	.7552	.5653		.2081	.7335	.5367
	.2100	-.193		.2920	.9395	.8761		.2500	.7890	.6210
	.2593	-.194		.4340	.9935	.9797		.2919	.8365	.6982
	.3075	-.193		.5050	1.0250	1.0428		.3338	.8760	.7656
	.3560	-.180		.5750	1.0195	1.0315		.3750	.9176	.8401
	.4050	-.168		.6460	1.0264	1.0450		.4170	.9543	.9089
	.4530	-.162		.7180	1.0223	1.0360		.4580	.9588	.9173
	.5020	-.157		.7890	1.0223	1.0383		.5000	.9624	.9243
	.5510	-.141		.8590	1.0452	1.0856		.5420	.9620	.9233
	.6000	-.105		.9300	1.0494	1.0923		.5830	.9639	.9271
	.6485	-.101		1.0000	1.0427	1.0788		.6250	.9945	.9945
	.6970	-.080	St'bd hull	.0177	.6099	.3694		.6670	.9971	.9921
St'bd	.7460	-.049		.0443	.7382	.5405		.7080	.9950	.9879
	.7950	-.027		.0797	.8103	.6509		.7500	.9955	.9889
	.8430	-.040		.1507	.9308	.8604		.7900	.9963	.9903
	.8920	.020		.2920	1.0329	1.0608		1.0225	1.0225	1.0432
	.9410	.137		.4340	1.0329	1.0608		1.0215	1.0215	1.0414
	.7800	-.015		.5050	1.0398	1.0743		1.0000	1.0229	1.0441
	.8195	-.060		.5750	1.0398	1.0721				
	.8580	-.013		.6460	1.0438	1.0811				
	.9160	.076		.7180	1.0413	1.0766				
	.9550	.214		.7890	1.0398	1.0743				
				.8590	1.0427	1.0788				
				.9300	1.0427	1.0788				
				1.0000	1.0413	1.0766				

TABLE 4 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25$

(e) $n = 34.19$ rps $\frac{U}{nD} = 1.370$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0146	.586	Port rake	.0177	.4165	.1786	Wake rake	.0000	.3800	.1441
	.0633	-.051		.0443	.5217	.2755		.0833	.5820	.3380
	.1120	-.158		.0797	.6141	.3827		.1667	.7121	.5059
	.1610	-.188		.1507	.7421	.5561		.2081	.7696	.5909
	.2100	-.219		.2920	.9275	.8724		.2500	.8129	.6593
	.2583	-.219		.4340	.9981	1.0102		.2919	.8619	.7412
	.3075	-.219		.5050	1.0289	1.0714		.3338	.9002	.8086
	.3560	-.193		.5750	1.0315	1.0816		.3750	.9359	.8739
	.4050	-.193		.6460	1.0289	1.0714		.4170	.9734	.9455
	.4530	-.193		.7180	1.0162	1.0510		.4580	.9675	.9341
	.5020	-.168		.7890	1.0260	1.0663		.5000	.9664	.9319
	.5510	-.148		.8590	1.0582	1.1378		.5420	.9679	.9350
	.6000	-.122		.9300	1.0553	1.1327		.5830	.9686	.9361
	.6485	-.106		1.0000	1.0528	1.1224		.6250	.9950	.9879
	.6970	-.086						.6670	.9966	.9910
	.7460	-.066						.7080	.9924	.9828
St'bd hull	.7950	-.045	St'bd rake	.0177	.6250	.3980		.7500	.9950	.9879
	.8430	-.071		.0443	.7504	.5714		.7900	.9919	.9817
	.8920	-.010		.0797	.8136	.6735		.8333	1.0162	1.0304
	.9410	.122		.1507	.9408	.8980		.9170	1.0209	1.0397
				.2920	1.0410	1.0969		1.0000	1.0187	1.0357
				.4340	1.0434	1.1071				
				.5050	1.0528	1.1224				
				.5750	1.0528	1.1224				
				.6460	1.0528	1.1224				
				.7180	1.0498	1.1173				
				.7890	1.0528	1.1224				
				.8590	1.0498	1.1173				
				.9300	1.0528	1.1224				
				1.0000	1.0464	1.1122				

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(f) $n = 53.31$ rps $\frac{U}{nD} = 1.311$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0146	.598	Port rake	.0177	.4335	.1839	Wake rake	.0000	.4236	.1790
	.0633	-.004		.0443	.5452	.2915		.0833	.5935	.3514
	.1120	-.132		.0797	.6289	.3901		.1667	.7155	.5107
	.1610	-.154		.1507	.7508	.5561		.2081	.7764	.6014
	.2100	-.188		.2920	.9326	.8565		.2500	.8215	.6733
	.2583	-.188		.4340	.9954	.9753		.2919	.8683	.7522
	.3075	-.188		.5050	1.0298	1.0448		.3338	.9078	.8223
	.3560	-.181		.5750	1.0216	1.0269		.3750	.9417	.8847
	.4050	-.170		.6460	1.0256	1.0359		.4170	.9731	.9448
	.4530	-.160		.7180	1.0243	1.0336		.4580	.9570	.9139
	.5020	-.152		.7890	1.0232	1.0291		.5000	.9588	.9171
	.5510	-.136		.8590	1.0501	1.0852		.5420	.9592	.9181
	.6000	-.109		.9300	1.0501	1.0852		.5830	.9594	.9186
	.6485	-.096		1.0000	1.0418	1.0695		.6250	.9973	.9923
St'bd hull	.6970	-.070	St'bd rake	.0177	.6357	.3969		.6670	.9966	.9909
	.7460	-.042		.0443	.7567	.5628		.7080	.9961	.9900
	.7950	-.031		.0797	.8257	.6704		.7500	.9973	.9923
	.8430	-.051		.1507	.9563	.8991		.7900	.9975	.9928
	.8920	.020		.2920	1.0350	1.0561		.8333	1.0224	1.0431
	.9410	.134		.4340	1.0380	1.0605		.9170	1.0211	1.0403
				.5050	1.0472	1.0807		1.0000	1.0229	1.0440
	.7800	-.017		.5750	1.0472	1.0807				
	.8195	-.056		.6460	1.0460	1.0762				
	.8680	-.015		.7180	1.0460	1.0762				
	.9160	.078		.7890	1.0434	1.0717				
	.9650	.219		.8590	1.0472	1.0785				
				.9300	1.0472	1.0807				
				1.0000	1.0501	1.0852				

8191-1

TABLE 4 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS

OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(g) $n = 36.65$ rps $\frac{U}{nD} = 1.278$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u/U_∞	q_1/q_∞	Sta- tion	z/h	u/U_∞	q_1/q_∞
Port hull	.0146	.618	Port rake	.0177	.4165	.1804	Wake rake	.0000	.3760	.1409
	.0633	-.020		.0443	.5508	.3093		.0833	.5900	.3472
	.1120	-.154		.0797	.6340	.4124		.1667	.7308	.5329
	.1610	-.190		.1507	.7628	.5979		.2081	.7895	.6220
	.2100	-.211		.2920	.9572	.9381		.2500	.8368	.6988
	.2583	-.201		.4340	1.0162	1.0619		.2919	.8816	.7754
	.3075	-.211		.5050	1.0349	1.0979		.3338	.9196	.8439
	.3560	-.211		.5750	1.0289	1.0825		.3750	.9551	.9102
	.4050	-.190		.6460	1.0289	1.0876		.4170	.9830	.9641
	.4530	-.185		.7180	1.0349	1.0979		.4580	.9626	.9247
	.5020	-.180		.7890	1.0349	1.0979		.5000	.9633	.9257
	.5510	-.164		.8590	1.0613	1.1546		.5420	.9647	.9288
	.6000	-.139		.9300	1.0613	1.1546		.5830	.9664	.9319
	.6485	-.118		1.0000	1.0553	1.1443		.6250	.9924	.9828
	.6970	-.087						.6670	.9955	.9890
	.7460	-.061	St'bd rake	.0177	.6250	.4021		.7080	.9908	.9796
	.7950	-.036		.0443	.7594	.5876		.7500	.9919	.9817
	.8430	-.077		.0797	.8249	.7010		.7900	.9883	.9745
	.8920	.010		.1507	.9408	.9072		.8333	1.0183	1.0346
	.9410	.108		.2920	1.0410	1.1082		.8917	1.0187	1.0357
				.4340	1.0410	1.1134		1.0000	1.0218	1.0418
				.5050	1.0434	1.1186				
St'bd hull	.7800	-.030	St'bd rake	.5750	1.0464	1.1237	St'bd rake			
	.8195	-.077		.6460	1.0498	1.1289				
	.8680	-.036		.7180	1.0434	1.1186				
	.9160	.077		.7890	1.0434	1.1186				
	.9650	.226		.8590	1.0528	1.1392				
				.9300	1.0528	1.1340				
				1.0000	1.0553	1.1443				

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(h) $n = 56.61$ rps $\frac{U}{nD} = 1.234$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0146	.603	Port rake	.0177	.4489	.2027	Wake rake	.0000	.4291	.1837
	.0633	-.002		.0443	.5633	.3166		.0833	.6108	.3722
	.1120	-.123		.0797	.6379	.4077		.1667	.7551	.5690
	.1610	-.154		.1507	.7642	.5831		.2081	.8117	.6574
	.2100	-.189		.2920	.9461	.8952		.2500	.8477	.7170
	.2583	-.189		.4340	.9995	1.0000		.2919	.8937	.7969
	.3075	-.189		.5050	1.0285	1.0569		.3338	.9302	.8631
	.3560	-.182		.5750	1.0243	1.0478		.3750	.9626	.9246
	.4050	-.173		.6460	1.0285	1.0569		.4170	.9905	.9787
	.4530	-.182		.7180	1.0256	1.0524		.4580	.9513	.9030
	.5020	-.152		.7890	1.0256	1.0524		.5000	.9529	.9059
	.5510	-.145		.8590	1.0501	1.1025		.5420	.9529	.9059
	.6000	-.123		.9300	1.0486	1.1002		.5830	.9558	.9115
	.6485	-.102		1.0000	1.0418	1.0843		.6250	.9787	.9787
St'bd hull	.6970	-.071	St'bd rake	.0177	.6289	.3964		.6670	.9899	.9777
	.7460	-.041		.0443	.7492	.5604		.7080	.9890	.9759
	.7950	-.027		.0797	.8223	.6765		.7500	.9885	.9749
	.8430	-.054		.1507	.9504	.9043		.7900	.9905	.9787
	.8920	.013		.2920	1.0311	1.0638		.8333	1.0162	1.0304
	.9410	.125		.4340	1.0271	1.0547		.9170	1.0156	1.0290
	.7800	-.018		.5050	1.0350	1.0729		1.0000	1.0162	1.0304
	.8195	-.066		.5750	1.0350	1.0706				
	.8680	-.018		.6460	1.0380	1.0774				
	.9150	.068		.7180	1.0350	1.0706				
	.9650	.211		.7890	1.0350	1.0706				
				.8590	1.0416	1.0843				
				.9300	1.0418	1.0866				
				1.0000	1.0447	1.0911				

819T-7

TABLE 4 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25$

(1) $n = 40.00$ rps $\frac{U}{ND} = 1.164$ $\alpha = -5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.601	Port rake	.0177	.4338	.1917	Wake rake	.0000	.3538	.1248
	.0633	-.010		.0443	.5597	.3212		.0833	.6246	.3892
	.1120	-.139		.0797	.6427	.4197		.1667	.7981	.6355
	.1610	-.160		.1507	.7754	.6114		.2081	.8573	.7332
	.2100	-.217		.2920	.9530	.9223		.2500	.8868	.7845
	.2583	-.225		.4340	1.0041	1.0259		.2919	.9290	.8611
	.3075	-.233		.5050	1.0320	1.0829		.3338	.9607	.9208
	.3560	-.202		.5750	1.0376	1.0829		.3750	.9855	.9691
	.4050	-.196		.6460	1.0376	1.0984		.4170	1.0124	1.0225
	.4530	-.186		.7180	1.0258	1.0725		.4580	.9596	.9187
	.5020	-.176		.7890	1.0258	1.0725		.5000	.9651	.9292
	.5510	-.155		.8590	1.0526	1.1295		.5420	.9628	.9250
	.6000	-.134		.9300	1.0471	1.1192		.5830	.9635	.9261
	.6485	-.139		1.0000	1.0471	1.1192		.6250	.9909	.9795
St'd hull	.6970	-.102	St'd rake	.0177	.5971	.3627		.6670	.9909	.9795
	.7460	-.072		.0443	.7293	.5440		.7080	.9924	.9827
	.7950	-.046		.0797	.8034	.6580		.7500	.9924	.9827
	.8430	-.057		.1507	.9262	.8756		.7900	1.0207	1.0393
	.8920	-.005		.2920	1.0410	1.1036		.8333	1.0207	1.0393
	.9410	.103		.4340	1.0350	1.0933		.9170	1.0201	1.0383
				.5050	1.0410	1.1036		1.0000		
				.5750	1.0376	1.0984				
				.6460	1.0441	1.1088				
				.7180	1.0441	1.1088				
				.7890	1.0376	1.0984				
				.8590	1.0471	1.1192				
				.9300	1.0496	1.1244				
				1.0000	1.0526	1.1295				

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(J) $n = 60.01$ rps $\frac{U}{nD} = 1.159$ $\alpha = -5.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u/U_∞	q_1/q_∞	Sta- tion	z/h	u/U_∞	q_1/q_∞
Port hull	.0146	.586	Port rake	.0177	.4418	.1941	Wake rake	.0000	.4042	.1630
	.0633	-.004		.0443	.5602	.3128		.0833	.6327	.3994
	.1120	-.125		.0797	.6405	.4087		.1667	.8124	.6585
	.1610	-.159		.1507	.7652	.5822		.2081	.8687	.7528
	.2100	-.191		.2920	.9380	.8744		.2500	.8939	.7973
	.2583	-.193		.4340	.9950	.9840		.2919	.9355	.8732
	.3075	-.194		.5050	1.0286	1.0525		.3338	.9676	.9343
	.3560	-.182		.5750	1.0219	1.0365		.3750	.9958	.9892
	.4050	-.180		.6460	1.0219	1.0388		.4170	1.0161	1.0300
	.4530	-.178		.7180	1.0244	1.0434		.4580	.9498	.9002
	.5020	-.148		.7890	1.0219	1.0388		.5000	.9529	.9059
	.5510	-.148		.8590	1.0462	1.0868		.5420	.9529	.9059
	.6000	-.127		.9300	1.0437	1.0822		.5830	.9540	.9083
	.6485	-.107		1.0000	1.0393	1.0753		.6250	.9886	.9750
St'bd hull	.6970	-.083	St'bd rake	.0177	.6405	.4064		.6670	.9895	.9770
	.7460	-.059		.0443	.7463	.5548		.7080	.9873	.9727
	.7950	-.036		.0797	.8309	.6849		.7500	.9895	.9770
	.8430	-.050		.1507	.9529	.9018		.7900	.9891	.9760
	.8920	.006		.2920	1.0274	1.0479		.8333	1.0186	1.0352
	.9410	.116		.4340	1.0286	1.0502		.9170	1.0174	1.0329
				.5050	1.0382	1.0708		1.0000	1.0188	1.0357
				.5750	1.0393	1.0731				
				.6460	1.0410	1.0776				
				.7180	1.0424	1.0799				

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(k) $n = 63.36$ rps $\frac{U_\infty}{nD} = 1.093$ $\alpha = -5.5^\circ$

Station	x/l	C_p	Station	y/h	u_1/U_∞	q_1/q_∞	Station	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0146	.600	Port rake	.0177	.4528	.2055	Wake rake	.0000	.3940	.1549
	.0633	.004		.0443	.5704	.3256		.0833	.6448	.4148
	.1120	-.115		.0797	.6389	.4065		.1667	.8397	.7036
	.1610	-.147		.1507	.7591	.5751		.2081	.8926	.7949
	.2100	-.189		.2920	.9406	.8822		.2500	.9138	.8331
	.2583	-.194		.4340	.9937	.9838		.2919	.9560	.9120
	.3075	-.194		.5050	1.0234	1.0439		.3338	.9871	.9722
	.3560	-.180		.5750	1.0208	1.0393		.3750	1.0126	1.0229
	.4050	-.180		.6460	1.0234	1.0439		.4170	1.0268	1.0521
	.4530	-.177		.7180	1.0208	1.0393		.4580	.9501	.9005
	.5020	-.152		.7890	1.0249	1.0462		.5000	.9517	.9039
	.5510	-.143		.8590	1.0456	1.0901		.5420	.9510	.9025
	.6000	-.115		.9300	1.0469	1.0924		.5830	.9517	.9039
	.6485	-.092		1.0000	1.0386	1.0762		.6250	.9895	.9770
	.6970	-.073	St'bd rake	.0177	.6136	.3741		.6670	.9910	.9799
St'bd hull	.7460	-.053		.0443	.7325	.5358		.7080	.9891	.9761
	.7950	-.027		.0797	.8118	.6559		.7500	.9895	.9770
	.8430	-.048		.1507	.9361	.8730		.7900	.9883	.9746
	.8920	.011		.2920	1.0290	1.0554		.8333	1.0172	1.0324
	.9410	.110		.4340	1.0264	1.0508		.9170	1.0182	1.0344
				.5050	1.0414	1.0808		1.0000	1.0187	1.0353
				.5750	1.0400	1.0785				
				.6460	1.0414	1.0808				
				.7180	1.0386	1.0762				
				.7890	1.0373	1.0716				
				.8590	1.0386	1.0739				
				.9300	1.0386	1.0739				
				1.0000	1.0386	1.0762				

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(1) $n = 43.40$ rps $\frac{U_\infty}{nD} = 1.074$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_y/U_∞	q_1/q_∞	Sta- tion	z/h	u_z/U_∞	q_1/q_∞
Port hull	.0146	.610	Port rake	.0177	.4738	.2167	Wake rake	.0000	.3072	.0942
	.0633	.024		.0443	.5612	.3251		.0833	.6381	.4061
	.1120	-.123		.0797	.6527	.4138		.1667	.8557	.7306
	.1610	-.157		.1507	.7868	.6010		.2081	.9080	.8227
	.2100	-.187		.2920	.9782	.9261		.2500	.9382	.8782
	.2583	-.195		.4340	1.0186	1.0049		.2919	.9723	.9431
	.3075	-.197		.5050	1.0580	1.0837		.3338	1.0073	1.0122
	.3560	-.167		.5750	1.0516	1.0739		.3750	1.0263	1.0509
	.4050	-.177		.6460	1.0461	1.0591		.4170	1.0289	1.0562
	.4530	-.162		.7180	1.0461	1.0640		.4580	.9554	.9106
	.5020	-.147		.7890	1.0516	1.0739		.5000	.9570	.9138
	.5510	-.128		.8590	1.0580	1.0887		.5420	.9549	.9097
	.6000	-.108		.9300	1.0580	1.0837		.5830	.9597	.9190
	.6485	-.108		1.0000	1.0516	1.0739		.6250	.9893	.9766
	.6970	-.070						.6670	.9825	.9829
	.7460	-.044	St'bd hull	.0177	.6566	.4187		.7080	.9893	.9766
St'bd hull	.7950	-.039		.0443	.7541	.5517		.7500	.9915	.9808
	.8430	-.039		.0797	.8220	.6552		.7900	.9899	.9776
	.8920	.024		.1507	.9521	.8818		.8333	1.0166	1.0310
	.9410	.118		.2920	1.0431	1.0542		.9170	1.0182	1.0342
				.4340	1.0400	1.0493		1.0000	1.0212	1.0405
				.5050	1.0580	1.0887				
				.5750	1.0580	1.0837				
				.6460	1.0486	1.0690				
				.7180	1.0550	1.0788				
				.7890	1.0486	1.0690				
				.8590	1.0486	1.0690				
				.9300	1.0516	1.0739				
				1.0000	1.0516	1.0739				

8761-7

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(21) $n = 66.67$ rps $\frac{U}{ND} = 1.043$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0146	.600	Port rake	.0177	.4610	.2091	Wake rake	.0000	.3936	.1546
	.0633	-.015		.0443	.5731	.3250		.0833	.6583	.4325
	.1120	-.122		.0797	.6496	.4182		.1667	.8759	.7654
	.1610	-.159		.1507	.7693	.5841		.2081	.9255	.8545
	.2100	-.197		.2920	.9353	.8636		.2500	.9435	.8882
	.2583	-.196		.4340	.9969	.9818		.2919	.9844	.9669
	.3075	-.195		.5050	1.0263	1.0409		.3338	1.0121	1.0219
	.3560	-.186		.5750	1.0209	1.0295		.3750	1.0329	1.0646
	.4050	-.181		.6460	1.0248	1.0386		.4170	1.0382	1.0754
	.4530	-.184		.7180	1.0235	1.0364		.4580	.9468	.8943
	.5020	-.156		.7890	1.0263	1.0409		.5000	.9487	.8982
	.5510	-.140		.8590	1.0466	1.0841		.5420	.9485	.8976
	.6000	-.111		.9300	1.0466	1.0841		.5830	.9521	.9043
	.6485	-.106		1.0000	1.0398	1.0705		.6250	.9905	.9788
St'd hull	.7800	-.020	St'd rake	.0177	.6204	.3818	St'd rake	.6670	.9938	.9853
	.8195	-.065		.0443	.7431	.5455		.7080	.9895	.9769
	.8680	-.018		.0797	.8157	.6591		.7500	.9897	.9773
	.9160	.047		.1507	.9339	.8614		.7900	.9895	.9769
	.9650	.172		.2920	1.0304	1.0500		.8333	1.0149	1.0276
				.4340	1.0291	1.0477		.9170	1.0165	1.0309
				.5050	1.0441	1.0773		1.0000	1.0165	1.0309
				.5750	1.0414	1.0727				
				.5460	1.0428	1.0750				
				.7180	1.0441	1.0773				

TABLE 4 Continued

CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS

OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$ (n) $n = 46.63$ rps $\frac{U}{nD} = .997$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u/U_∞	q_1/q_∞	Sta- tion	z/h	u/U_∞	q_1/q_∞
Port hull	.0146	.583	Port rake	.0177	.4475	.2030	Wake rake	.0000	.2922	.0852
	.0633	-.020		.0443	.5660	.3198		.0833	.6787	.4597
	.1120	-.142		.0797	.6345	.4010		.1667	.9126	.8310
	.1610	-.172		.1507	.7798	.6041		.2081	.9620	.9235
	.2583	-.218		.2920	.9675	.9340		.2500	.9788	.9561
	.3075	-.213		.4340	1.0211	1.0406		.2919	1.0112	1.0203
	.3560	-.223		.5050	1.0486	1.0914		.3338	1.0425	1.0845
	.4050	-.218		.5750	1.0390	1.0761		.3750	1.0561	1.1128
	.4530	-.208		.6460	1.0334	1.0609		.4170	1.0354	1.0697
	.5020	-.187		.7180	1.0236	1.0457		.4580	.9533	.9067
	.5510	-.152		.7890	1.0236	1.0457		.5000	.9543	.9088
	.6000	-.116		.8590	1.0575	1.1117		.5420	.9528	.9057
	.6485	-.089		.9300	1.0541	1.1066		.5830	.9549	.9099
	.6970	-.102		1.0000	1.0541	1.1066		.6250	.9842	.9666
	.7460	-.076						.6670	.9854	.9688
	.7950	-.071	St'd hull	.0177	.6091	.3706		.7080	.9832	.9646
St'd hull	.8430	-.076		.0443	.7439	.5482		.7500	.9848	.9677
	.8920	-.030		.0797	.8084	.6497		.7900	.9864	.9708
	.9410	.076		.1507	.9411	.8832		.8333	1.0123	1.0224
				.2920	1.0425	1.0812		.9170	1.0112	1.0203
				.4340	1.0456	1.0863		1.0000	1.0138	1.0256
				.5050	1.0575	1.1117				
				.5750	1.0605	1.1218				
				.6460	1.0541	1.1066				
				.7180	1.0541	1.1066				
				.7890	1.0541	1.1066				
				.8590	1.0486	1.0964				
				.9300	1.0511	1.1015				
				1.0000	1.0541	1.1066				

TABLE 4 Continued
 CHOIRWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25$

(O) $n = 70.02$ rps $\frac{U}{nD} = .989$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.C146	.595	Port rake	.0177	.4720	.2197	Wake rake	.0000	.3854	.1481
	.C633	-.009		.0443	.5852	.3387		.0833	.6796	.4607
	.1120	-.128		.0797	.6610	.4325		.1667	.9106	.8274
	.1610	-.153		.1507	.7867	.6110		.2081	.9620	.9234
	.2100	-.194		.2920	.9556	.9016		.2500	.9778	.9541
	.2583	-.193		.4340	1.0023	.9908		.2919	1.0177	1.0334
	.3075	-.192		.5050	1.0345	1.0572		.3338	1.0446	1.0889
	.3560	-.187		.5750	1.0320	1.0503		.3750	1.0621	1.1256
	.4050	-.178		.6460	1.0320	1.0503		.4170	1.0578	1.1166
	.4530	-.172		.7180	1.0331	1.0526		.4580	.9477	.8962
	.5020	-.160		.7890	1.0303	1.0481		.5000	.9505	.9015
	.5510	-.146		.8590	1.0508	1.0892		.5420	.9487	.8982
	.6000	-.114		.9300	1.0494	1.0870		.5830	.9515	.9034
	.6435	-.112		1.0000	1.0414	1.0709		.6250	.9900	.9779
	.6970	-.080						.6670	.9937	.9851
	.7460	-.052	St'bd hull	.0177	.6321	.3959		.7080	.9900	.9779
St'bd hull	.7950	-.032		.0443	.7477	.5515		.7500	.9910	.9799
	.8430	-.052		.0797	.8224	.6682		.7900	.9905	.9789
	.8920	.000		.1507	.9452	.8810		.8333	1.0187	1.0353
	.9410	.091		.2920	1.0428	1.0732		.9170	1.0212	1.0406
				.4340	1.0386	1.0641		1.0000	1.0187	1.0353
	.7800	-.025		.5050	1.0508	1.0892				
	.8195	-.073		.5750	1.0494	1.0870				
	.9160	.045		.6460	1.0494	1.0870				
	.9650	.160		.7180	1.0469	1.0824				
				.7890	1.0456	1.0801				
				.8590	1.0469	1.0824				
				.9300	1.0483	1.0847				
				1.0000	1.0494	1.0870				

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(p) $n = 71.66$ rps $\frac{U}{nD} = .968$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.614	Port rake	.0177	.4678	.2209	Wake rake	.0000	.3585	.1282
	.0633	.007		.0443	.5869	.3465		.0833	.6970	.4848
	.1120	-.116		.0797	.6554	.4326		.1667	.9373	.8767
	.1610	-.153		.1507	.7805	.6140		.2081	.9872	.9726
	.2100	-.188		.2920	.9558	.9186		.2500	1.0003	.9982
	.2583	-.189		.4340	1.0009	1.0070		.2919	1.0374	1.0736
	.3075	-.190		.5050	1.0276	1.0628		.3338	1.0601	1.1212
	.3560	-.190		.5750	1.0250	1.0581		.3750	1.0744	1.1518
	.4050	-.176		.6460	1.0290	1.0651		.4170	1.0596	1.1203
	.4530	-.179		.7180	1.0262	1.0605		.4580	.9445	.8900
	.5020	-.158		.7890	1.0290	1.0651		.5000	.9455	.8919
	.5510	-.146		.8590	1.0456	1.1000		.5420	.9453	.8915
	.6000	-.130		.9300	1.0456	1.1000		.5830	.9480	.8967
	.6485	-.109		1.0000	1.0442	1.0977		.6250	.9856	.9692
	.6970	-.077						.6670	.9883	.9744
	.7460	-.051	St'bd hull	.0177	.6289	.3977		.7080	.9856	.9692
St'bd hull	.7950	-.032		.0443	.7486	.5628		.7500	.9863	.9706
	.8430	-.058		.0797	.8196	.6767		.7900	.9853	.9687
	.8920	-.002		.1507	.9378	.8860		.8333	1.0190	1.0359
	.9410	.093		.2920	1.0346	1.0767		.9170	1.0196	1.0374
				.4340	1.0346	1.0767		1.0000	1.0187	1.0354
				.5050	1.0456	1.1000				
				.5750	1.0442	1.0977				
				.6460	1.0442	1.0977				
				.7180	1.0456	1.1000				
				.7890	1.0442	1.0977				
				.8590	1.0494	1.1070				
				.9300	1.0469	1.1023				
				1.0000	1.0469	1.1023				

8191-T

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25$

(r) $n = 55.00$ rps $\frac{U}{nD} = .846$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0146	.625	Port rake	.0177	.4813	.2300	Wake rake	.0000	.2921	.0851
	.0633	.020		.0443	.5823	.3350		.0833	.7576	.5727
	.1120	-.110		.0797	.6434	.4050		.1667	1.0263	1.0508
	.1510	-.150		.1507	.8120	.6450		.2081	1.0773	1.1580
	.2100	-.200		.2920	.9731	.9300		.2500	1.0846	1.1738
	.2583	-.197		.4340	1.0206	1.0250		.2500	1.1210	1.2537
	.3075	-.195		.5050	1.0420	1.0650		.3338	1.1331	1.2810
	.3560	-.185		.5750	1.0601	1.1000		.3750	1.1340	1.2830
	.4050	-.180		.6460	1.0452	1.0700		.4170	1.0232	1.0446
	.4530	-.175		.7180	1.0385	1.0600		.4580	.9489	.8985
	.5020	-.160		.7890	1.0360	1.0550		.5000	.9496	.8996
	.5510	-.140		.8590	1.0571	1.0950		.5420	.9473	.8953
	.6000	-.125		.9300	1.0601	1.1050		.5830	.9489	.8985
	.6485	-.110		1.0000	1.0571	1.0950		.6250	.9860	.9699
	.6970	-.085						.6670	.9864	.9709
St'bd hull	.7460	-.060	St'bd rake	.0177	.6037	.3550		.7080	.9843	.9667
	.7950	-.030		.0443	.7264	.5200		.7500	.9860	.9699
	.8430	-.060		.0797	.7996	.6250		.8333	.9864	.9709
	.8920	-.015		.1507	.9236	.8400		.9170	1.0143	1.0266
	.9410	.075		.2920	1.0482	1.0750		1.0000	1.0170	1.0319
				.4340	1.0482	1.0750				
				.5050	1.0482	1.0800				
				.5750	1.0482	1.0750				
				.6460	1.0482	1.0800				
				.7180	1.0506	1.0850				

8191-71

TABLE 4 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(S) $n = 60.01$ rps $\frac{U}{nD} = .778$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0146	.599	Port rake	.0177	.4731	.2292	Wake rake	.0000	.3219	.1033
	.0633	-.026		.0443	.5857	.3542		.0833	.8297	.6867
	.1120	-.156		.0797	.6605	.4479		.1667	1.1067	1.2222
	.1610	-.177		.1507	.7895	.6406		.2081	1.1684	1.3620
	.2100	-.213		.2920	.9606	.9479		.2500	1.1652	1.3547
	.2583	-.215		.4340	1.0233	1.0781		.2919	1.1941	1.4225
	.3075	-.218		.5050	1.0415	1.1146		.3338	1.2011	1.4392
	.3560	-.203		.5750	1.0415	1.1146		.3750	1.1782	1.3849
	.4050	-.197		.6460	1.0324	1.0938		.4170	.9884	.9748
	.4530	-.192		.7180	1.0415	1.1146		.4580	.9402	.8819
	.5020	-.187		.7890	1.0415	1.1146		.5000	.9402	.8819
	.5510	-.187		.8590	1.0565	1.1458		.5420	.9385	.8788
	.6000	-.165		.9300	1.0565	1.1510		.5830	.9413	.8840
	.6485	-.140		1.0000	1.0565	1.1458		.6250	.9795	.9571
	.6970	-.102						.6670	.9783	.9549
	.7460	-.078						.7080	.9783	.9549
St'bd hull	.7800	-.052	St'bd rake	.0177	.6111	.3854	St'bd rake	.7500	.9788	.9560
	.8195	-.099		.0443	.7447	.5677		.7900	1.0125	1.0229
	.8680	-.062		.0797	.8124	.6823		.8333	1.0109	1.0196
	.9160	-.010		.1507	.9341	.8958		.9170	1.0135	1.0249
	.9650	.062		.2920	1.0470	1.1302		1.0000		
				.4340	1.0565	1.1458				

TABLE 4 Concluded
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 1 INSTALLED WITH $\beta = 25^\circ$

(t) $n = 64.99$ rps $\frac{U_\infty}{nD} = .718$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0146	.599	Port rake	.0177	.5054	.2656	Wake rake	.0000	.3732	.1390
	.0633	-.026		.0443	.6217	.3958		.0833	.9049	.8170
	.1120	-.145		.0797	.6887	.4844		.1667	1.2061	1.4511
	.1610	-.177		.1507	.8129	.6823		.2081	1.2731	1.6172
	.2100	-.234		.2920	.9773	.9844		.2500	1.2629	1.5911
	.2583	-.229		.4340	1.0330	1.0990		.2919	1.2908	1.6622
	.3075	-.224		.5050	1.0452	1.1198		.3338	1.2782	1.6297
	.3560	-.218		.5750	1.0452	1.1198		.3750	1.2104	1.4616
	.4050	-.218		.6460	1.0452	1.1198		.4170	.9572	.9141
	.4530	-.197		.7180	1.0452	1.1250		.4580	.9351	.8724
	.5020	-.182		.7890	1.0390	1.1094		.5000	.9368	.8755
	.5510	-.161		.8590	1.0655	1.1667		.5420	.9345	.8713
	.6000	-.130		.9300	1.0625	1.1615		.5830	.9368	.8755
	.6485	-.125		1.0000	1.0595	1.1563		.6250	.9756	.9497
	.6970	-.100						.6670	.9794	.9570
	.7460	-.078	St'bd rake	.0177	.6325	.4115		.7080	.9746	.9475
St'bd hull	.7950	-.046		.0443	.7624	.5938		.7500	.9761	.9507
	.8430	-.083		.0797	.8250	.6979		.7900	.9761	.9507
	.8920	-.026		.1507	.9446	.9167		.8333	1.0088	1.0154
	.9410	.020		.2920	1.0422	1.1146		.9170	1.0084	1.0144
				.4340	1.0452	1.1250		1.0000	1.0100	1.0176
				.5050	1.0570	1.1458				
				.5750	1.0506	1.1354				
				.6460	1.0506	1.1354				
				.7180	1.0475	1.1302				
				.7890	1.0570	1.1510				
				.8590	1.0595	1.1563				
				.9300	1.0570	1.1510				
				1.0000	1.0595	1.1563				

TABLE 5

CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(a)

n = 67.13 rps

$\frac{U}{nD} = 1.517$

$\alpha = -0.5$

Station	x/l	C_p	Station	y/h	u/U_∞	q_1/q_∞
Port hull	.0144	.595	Port rate	.0177	.4260	.1761
	.0625	.015		.0443	.5454	.2891
	.1107	.110		.0797	.6206	.3761
	.1587	.139		.1507	.7420	.5348
	.2068	.180		.2920	.9263	.8348
	.2545	.179		.4340	.9841	.9435
	.3025	.178		.5050	1.0250	1.0239
	.3510	.173		.5750	1.0132	1.0000
	.3985	.160		.6460	1.0212	1.0152
	.4470	.176		.7180	1.0184	1.0109
	.4950	.143		.7890	1.0198	1.0130
	.5430	.137		.8590	1.0478	1.0674
	.5910	.097		.9300	1.0466	1.0652
	.6390	.087		1.0000	1.0413	1.0565
	.6870	.064				
St'bd hull	.7350	.039	St'bd rate	.0177	.6052	.3565
	.7845	.013		.0443	.7306	.5196
	.8310	.030		.0797	.7972	.6174
	.8795	.032		.1507	.9190	.8217
	.9275	.160		.2920	1.0239	1.0196
				.4340	1.0250	1.0239
	.7600	-.013		.5050	1.0371	1.0478
	.8075	-.045		.5750	1.0400	1.0522
	.8550	.002		.6460	1.0358	1.0457
	.9045	.097		.7180	1.0358	1.0457
	.9520	.243		.7890	1.0358	1.0457
				.8590	1.0522	1.0522
				.9300	1.0413	1.0565
				1.0000	1.0413	1.0565

Station	z/h	u_1/U_∞	q_1/q_∞
Wake rate	.0000		
	.0833	.4356	.1894
	.1667	.4569	.2082
	.2081	.6044	.3644
	.2500	.6782	.4589
	.2919	.7546	.5681
	.3338	.8102	.6548
	.3750	.8574	.7336
	.4170	.9064	.8197
	.4580	.9412	.8638
	.5000	.9644	.9280
	.5420	.9723	.9432
	.5830	.9716	.9418
	.6250	.9718	.9423
	.6670	1.0013	1.0013
	.7080	1.0003	1.0004
	.7500	1.0010	.9985
	.7900	1.0006	.9999
	.8333	1.0212	.9990
	.9170	1.0196	1.0405
	1.0000	1.0216	1.0373
			1.0414

TABLE 5 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS

OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(b) $n = 46.52$ rps $\frac{U}{nD} = 1.464$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0144	.631	Port rake	.0177	.4152	.1717	Wake rake	.0000	.3922	.1534
	.0625	.000		.0443	.5260	.2828		.0833	.4599	.2111
	.1107	-.146		.0797	.6172	.3838		.1667	.6010	.3603
	.1587	-.156		.1507	.7437	.5606		.2081	.6800	.4613
	.2068	-.207		.2920	.9311	.8788		.2500	.7535	.5663
	.2545	-.209		.4340	.9861	.9848		.2919	.8057	.6477
	.3025	-.212		.5050	1.0103	1.0354		.3338	.8572	.7332
	.3510	-.191		.5750	1.0103	1.0354		.3750	.9013	.8103
	.3985	-.176		.6460	1.0164	1.0455		.4170	.9464	.8938
	.4470	-.191		.7180	1.0042	1.0202		.4580	.9665	.9319
	.4950	-.171		.7890	1.0129	1.0404		.5000	.9638	.9268
	.5430	-.166		.8590	1.0548	1.1263		.5420	.9728	.9443
	.5910	-.126		.9300	1.0577	1.1313		.5830	.9697	.9380
	.6390	-.116		1.0000	1.0493	1.1111		.6250	.9928	.9834
	.6870	-.095	St'bd hull	.0177	.6172	.3838		.6670	.9839	.9659
	.7350	-.075		.0443	.7227	.5303		.7080	.9882	.9741
	.7845	-.050		.0797	.8000	.6465		.7500	.9877	.9731
	.8310	-.060		.1507	.9244	.8636		.7900	.9901	.9783
	.8795	.030		.2920	1.0225	1.0556		.8333	1.0154	1.0287
	.9275	.151		.4340	1.0280	1.0707		.9170	1.0123	1.0224
	.7600	-.030		.5050	1.0400	1.0960		1.0000	1.0113	1.0204
	.8075	-.070		.5750	1.0400	1.0960				
	.8550	-.020		.6460	1.0400	1.0960				
	.9045	.090		.7180	1.0400	1.0960				
	.9520	.232		.7890	1.0400	1.0960				
				.8590	1.0430	1.1010				
				.9300	1.0464	1.1061				
				1.0000	1.0430	1.1010				

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TABLE 5 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(C) $n = 76.11$ rps $\frac{U}{nD} = 1.340$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_{∞}	q_1/q_{∞}	Sta- tion	z/h	U/U_{∞}	q_1/q_{∞}
Port hull	.0144	.607	Port rake	.0177	.4178	.1707	Wake rake	.0000	.4211	.1769
	.0625	.008		.0443	.5308	.2794		.0833	.4841	.2339
	.1107	-.110		.0797	.6040	.3614		.1667	.6275	.3928
	.1587	-.148		.1507	.7268	.5211		.2081	.7065	.4979
	.2068	-.172		.2920	.9139	.8248		.2500	.7783	.6045
	.2545	-.174		.4340	.9853	.9579		.2919	.8221	.6743
	.3025	-.175		.5050	1.0251	1.0377		.3338	.8621	.7415
	.3510	-.166		.5750	1.0183	1.0244		.3750	.9128	.8314
	.3985	-.159		.6460	1.0224	1.0333		.4170	.9462	.8934
	.4470	-.166		.7180	1.0224	1.0333		.4580	.9652	.9296
	.4950	-.141		.7890	1.0211	1.0310		.5000	.9743	.9472
	.5430	-.133		.8590	1.0493	1.0865		.5420	.9709	.9407
	.5910	-.111		.9300	1.0465	1.0820		.5830	.9638	.9268
St'b'd hull	.6390	-.086	St'b'd rake	1.0000	1.0411	1.0710		.6250	.9901	.9783
	.6870	-.059		.0177	.6090	.3659		.6670	.9868	.9717
	.7350	-.028		.0443	.7306	.5277		.7080	.9885	.9749
	.7845	-.008		.0797	.8010	.6341		.7500	.9922	.9823
	.8310	-.026		.1507	.9244	.8448		.7900	.9950	.9879
	.8795	.039		.2920	1.5468	2.4061		.8333	1.0163	1.0305
	.9275	.166		.4340	1.5485	2.4112		.9170	1.0055	1.0088
	.7600	-.011		.5050	1.5606	2.4518		1.0000	1.0199	1.0379
	.8075	-.046		.5750	1.5606	2.4518				
	.8550	.006		.6460	1.5566	2.4365				
	.9045	.102		.7180	1.5629	2.4569				
	.9520	.250		.7890	1.5606	2.4518				
				.8590	1.5667	2.4721				
				.9300	1.5650	2.4619				
				1.0000	1.5705	2.4822				

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(d) $n = 86.21$ rps $\frac{U_\infty}{nD} = 1.180$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0144	.624	Port rake	.0177	.4278	.1812	Wake rake	.0000	.4343	.1881
	.0625	.033		.0443	.5399	.2886		.0833	.5219	.2718
	.1107	-.098		.0797	.6232	.3870		.1667	.6650	.4413
	.1587	-.140		.1507	.7465	.5548		.2081	.7437	.5519
	.2068	-.172		.2920	.9318	.8635		.2500	.8145	.6620
	.2545	-.154		.4340	.9839	.9620		.2919	.8349	.6954
	.3025	-.172		.5050	1.0173	1.0268		.3338	.8677	.7512
	.3510	-.163		.5750	1.0130	1.0201		.3750	.9155	.8362
	.3985	-.158		.6460	1.0158	1.0246		.4170	.9475	.8957
	.4470	-.167		.7180	1.0158	1.0246		.4580	.9650	.9291
	.4950	-.140		.7890	1.0144	1.0224		.5000	.9710	.9407
	.5430	-.132		.8590	1.0456	1.0850		.5420	.9718	.9421
	.5910	-.110		.9300	1.0442	1.0828		.5830	.9678	.9347
	.6390	-.094		1.0000	1.0376	1.0694		.6250	.9985	.9946
	.6870	-.060	St'bd hull	.0177	.6076	.3669		.6670	.9975	.9928
St'bd hull	.7350	-.031		.0443	.7337	.5347		.7080	.9973	.9923
	.7845	-.006		.0797	.8004	.6353		.7500	.9992	.9960
	.8310	-.026		.1507	.9182	.8367		.7900	.9985	.9946
	.8795	.033		.2920	1.0253	1.0447		.8333	1.0223	1.0430
	.9275	.163		.4340	1.0226	1.0380		.9170	1.0185	1.0350
	.7600	-.011		.5050	1.0307	1.0559		1.0000	1.0223	1.0430
	.8075	-.047		.5750	1.0321	1.0582				
	.8550	.006		.6460	1.0307	1.0559				
	.9045	.100		.7180	1.0321	1.0582				
	.9520	.241		.7890	1.0267	1.0470				
				.8590	1.0360	1.0671				
				.9300	1.0346	1.0649				
				1.0000	1.0346	1.0626				

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20$

(e) $n = 58.78$ rps $\frac{U}{nD} = 1.156$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_{∞}	q_1/q_{∞}	Sta- tion	z/h	U_1/U_{∞}	q_1/q_{∞}
Port hull	.0144	.606	Port rake	.0177	.4159	.1717	Wake rake	.0000	.4147	.1716
	.0625	.010		.0443	.5270	.2828		.0833	.5170	.2667
	.1107	-.136		.0797	.6083	.3737		.1667	.6510	.4228
	.1587	-.166		.1507	.7536	.5707		.2081	.7291	.5303
	.2068	-.205		.2920	.9329	.8788		.2500	.8034	.6439
	.2545	-.210		.4340	.9880	.9848		.2919	.8256	.6802
	.3025	-.202		.5050	1.0245	1.0606		.3338	.8667	.7494
	.3510	-.181		.5750	1.0214	1.0505		.3750	.9189	.8425
	.3985	-.181		.6460	1.0245	1.0556		.4170	.9640	.9272
	.4470	-.176		.7180	1.0245	1.0556		.4580	.9747	.9478
	.4950	-.171		.7890	1.0245	1.0556		.5000	.9684	.9355
	.5430	-.156		.8590	1.0514	1.1162		.5420	.9769	.9520
	.5910	-.131		.9300	1.0485	1.1061		.5830	.9710	.9406
	.6390	-.106		1.0000	1.0451	1.1010		.6250	.9900	.9778
	.6870	-.080						.6670	.9853	.9686
	.7350	-.055	St'bd rake	.0177	.6039	.3687		.7080	.9868	.9716
St'bd hull	.7845	-.030		.0443	.7240	.5303		.7500	.9827	.9634
	.8310	-.055		.0797	.8085	.6566		.7900	.9874	.9727
	.8795	.010		.1507	.9396	.8889		.8333	1.0077	1.0130
	.9275	.141		.2920	1.0365	1.0808		.9170	1.0103	1.0181
				.4340	1.0365	1.0808		1.0000	1.0107	1.0192
				.5050	1.0396	1.0859				
				.5750	1.0420	1.0960				
				.6460	1.0335	1.0758				
				.7180	1.0420	1.0960				
				.7890	1.0396	1.0909				
				.8590	1.0514	1.1111				
				.9300	1.0514	1.1111				
				1.0000	1.0485	1.1061				

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(f) $n = 95.71$ rps $\frac{U}{ND} = 1.060$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0144	.599	Port rake	.0177	.4232	.1779	Wake rake	.0000	.4495	.2016
	.0625	.002		.0443	.5364	.2860		.0833	.5633	.3166
	.1107	-.117		.0797	.6096	.3694		.1667	.7046	.4951
	.1587	-.150		.1507	.7341	.5360		.2081	.7874	.6187
	.2068	-.189		.2920	.9200	.8401		.2500	.8592	.7365
	.2545	-.189		.4340	.9787	.9505		.2919	.8515	.7234
	.3025	-.189		.5050	1.0178	1.0293		.3338	.8730	.7603
	.3510	-.175		.5750	1.0123	1.0180		.3750	.9200	.8445
	.3985	-.168		.6460	1.0178	1.0293		.4170	.9531	.9062
	.4470	-.175		.7180	1.0208	1.0360		.4580	.9692	.9371
	.4950	-.146		.7890	1.0153	1.0225		.5000	.9750	.9483
	.5430	-.137		.8590	1.0410	1.0766		.5420	.9737	.9459
	.5910	-.115		.9300	1.0424	1.0788		.5830	.9747	.9478
	.6390	-.096		1.0000	1.0380	1.0698		.6250	1.0017	1.0011
	.6870	-.068						.6670	1.0035	1.0049
	.7350	-.042						.7080	1.0035	1.0049
St'bd hull	.7845	-.018	St'bd rake	.0177	.5953	.3536		.7500	1.0022	1.0020
	.8310	-.036		.0443	.7245	.5225		.7900	1.0035	1.0049
	.8795	.029		.0797	.7892	.6194		.8333	1.0272	1.0525
	.9275	.144		.1507	.9077	.8198		.9170	1.0262	1.0507
				.2920	1.0219	1.0383		1.0000	1.0260	1.0502
				.4340	1.0219	1.0383				
				.5050	1.0301	1.0541				
				.5750	1.0301	1.0541				
				.6460	1.0288	1.0518				
				.7180	1.0315	1.0553				
				.7890	1.0315	1.0563				
				.8590	1.0369	1.0676				
				.9300	1.0380	1.0698				
				1.0000	1.0380	1.0698				

9191-1

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(g) $n = 105.21$ rps $\frac{U_\infty}{ND} = .965$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.624	Port rake	.0177	.4322	.1878	Wake rake	.0000	.4606	.2117
	.0625	.029		.0443	.5538	.3054		.0833	.5934	.3513
	.1107	-.106		.0797	.6338	.4027		.1667	.7351	.5391
	.1587	-.138		.1507	.7579	.5747		.2081	.8186	.6685
	.2068	-.181		.2920	.9388	.8801		.2500	.8949	.7989
	.2545	-.179		.4340	.9855	.9706		.2919	.8659	.7480
	.3025	-.178		.5050	1.0173	1.0339		.3338	.8806	.7737
	.3510	-.169		.5750	1.0118	1.0226		.3750	.9265	.8563
	.3985	-.167		.6460	1.0204	1.0385		.4170	.9514	.9031
	.4470	-.169		.7180	1.0159	1.0317		.4580	.9673	.9334
	.4950	-.144		.7890	1.0159	1.0317		.5000	.9688	.9362
	.5430	-.140		.8590	1.0418	1.0837		.5420	.9677	.9344
	.5910	-.099		.9300	1.0389	1.0792		.5830	.9697	.9382
	.6390	-.090		1.0000	1.0351	1.0701		.6250	.9975	.9928
St'bd hull	.6870	-.068	St'bd rake	.0177	.6117	.3733		.6670	.9982	.9942
	.7350	-.038		.0443	.7338	.5385		.7080	.9975	.9928
	.7845	-.009		.0797	.8065	.6493		.7500	.9975	.9928
	.8310	-.038		.1507	.9270	.8575		.7900	.9975	.9928
	.8795	.029		.2920	1.0227	1.0452		.8333	1.0219	1.0418
	.9275	.156		.4340	1.0255	1.0498		.9170	1.0231	1.0441
	.7600	-.009		.5050	1.0376	1.0747		1.0000	1.0219	1.0418
	.8075	-.047		.5750	1.0364	1.0724				
	.8550	.002		.6460	1.0337	1.0679				
	.9045	.092		.7180	1.0337	1.0679				

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(h) $n = 71.16$ rps $\frac{U}{nD} = .956$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_{∞}	q_1/q_{∞}	Sta- tion	z/h	u_1/U_{∞}	q_1/q_{∞}
Port hull	.0144	.593	Port rake	.0177	.4155	.1777	Wake rake	.0000	.3991	.1589
	.0625	-.015		.0443	.5265	.2843		.0833	.5708	.3250
	.1107	-.137		.0797	.6126	.3807		.1667	.7104	.5034
	.1587	-.177		.1507	.7445	.5635		.2081	.7955	.6313
	.2068	-.218		.2920	.9287	.8731		.2500	.8593	.7366
	.2545	-.210		.4340	.9958	1.0051		.2919	.8249	.6789
	.3025	-.203		.5050	1.0205	1.0558		.3338	.8629	.7428
	.3510	-.187		.5750	1.0174	1.0508		.3750	.9113	.8284
	.3985	-.177		.6460	1.0138	1.0457		.4170	.9474	.8955
	.4470	-.170		.7180	1.0174	1.0508		.4580	.9594	.9182
	.4950	-.162		.7890	1.0205	1.0558		.5000	.9551	.9099
	.5430	-.147		.8590	1.0504	1.1168		.5420	.9588	.9172
	.5910	-.111		.9300	1.0474	1.1117		.5830	.9610	.9213
	.6390	-.101		1.0000	1.0385	1.0964		.6250	.9764	.9512
	.6870	-.069	St'bd hull	.0177	.5823	.3452		.6670	.9701	.9388
	.7350	-.045		.0443	.7104	.5127		.7080	.9701	.9388
	.7845	-.025		.0797	.7884	.6345		.7500	.9631	.9254
	.8310	-.050		.1507	.9186	.8579		.7900	.9690	.9368
	.8795	.015		.2920	1.0290	1.0761		.8333	.9953	.9884
	.9275	.142		.4340	1.0355	1.0863		.9170	.9922	.9821
				.5050	1.0410	1.1015		1.0000	.9917	.9812
				.5750	1.0355	1.0863				
				.6460	1.0440	1.1066				
				.7180	1.0385	1.0964				
				.7890	1.0385	1.0964				
				.8590	1.0440	1.1066				
				.9300	1.0410	1.1015				
				1.0000	1.0385	1.0964				

TABLE 5 Continued

CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(1) $n = 114.74$ rps $\frac{U}{nD} = .884$ $\alpha = -5^\circ$

Station	x/l	C_p	Station	y/h	U_1/U_∞	q_1/q_∞	Station	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.621	Port rake	.0177	.4389	.1893	Wake rake	.0000	.4728	.2231
	.0625	.031		.0443	.5566	.3051		.0633	.6348	.4022
	.1107	-.102		.0797	.6364	.3987		.1667	.7839	.6130
	.1587	-.140		.1507	.7602	.5679		.2081	.8692	.7538
	.2068	-.180		.2920	.9467	.8820		.2500	.9452	.8913
	.2545	-.181		.4340	.9942	.9710		.2919	.8828	.7777
	.3025	-.182		.5050	1.0326	1.0490		.3338	.8886	.7879
	.3510	-.175		.5750	1.0288	1.0401		.3750	.9311	.8651
	.3985	-.167		.6460	1.0326	1.0490		.4170	.9526	.9053
	.4470	-.171		.7180	1.0315	1.0445		.4580	.9672	.9333
	.4950	-.147		.7890	1.0326	1.0490		.5000	.9708	.9403
	.5430	-.138		.8590	1.0581	1.1002		.5420	.9689	.9365
	.5910	-.093		.9300	1.0554	1.0958		.5830	.9697	.9380
	.6390	-.091		1.0000	1.0527	1.0891		.6250	1.0022	1.0020
St'bd hull	.6870	-.068	St'bd rake	.0177	.6096	.3653		.6670	.9982	.9941
	.7350	-.044		.0443	.7284	.5212		.7080	.9973	.9922
	.7845	-.006		.0797	.8031	.6347		.7500	1.0013	1.0002
	.8310	-.031		.1507	.9243	.8396		.7900	1.0003	.9984
	.8795	.031		.2920	1.0288	1.0401		.8333	1.0223	1.0428
	.9275	.147		.4340	1.0315	1.0445		.9170	1.0227	1.0437
	.7600	-.008		.5050	1.0447	1.0735		1.0000	1.0229	1.0441
	.8075	-.044		.5750	1.0435	1.0690				
	.8550	.000		.6460	1.0424	1.0568				
	.9045	.091		.7180	1.0435	1.0690				
	.9520	.222		.7890	1.0435	1.0690				
				.8590	1.0447	1.0735				
				.9300	1.0478	1.0780				
				1.0000	1.0478	1.0780				

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(J) $n = 83.51$ rps $\frac{U}{ND} = .815$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.618	Port rake	.0177	.4152	.1733	Wake rake	.0000	.4393	.1925
	.0625	.000		.0443	.5433	.2921		.0833	.6823	.4644
	.1107	-.118		.0797	.6230	.3812		.1667	.8253	.6796
	.1587	-.153		.1507	.7569	.5644		.2081	.9121	.8299
	.2068	-.198		.2320	.9409	.8812		.2500	.9697	.9380
	.2545	-.193		.4340	.9979	.9901		.2519	.8500	.7208
	.3025	-.188		.5050	1.0376	1.0693		.3338	.8840	.7795
	.3510	-.178		.5750	1.0346	1.0594		.3750	.9233	.8505
	.3985	-.158		.6460	1.0346	1.0594		.4170	.9606	.9205
	.4470	-.160		.7180	1.0346	1.0594		.4580	.9728	.9443
	.4950	-.153		.7890	1.0316	1.0545		.5000	.9562	.9124
	.5430	-.133		.8590	1.0519	1.0990		.5420	.9707	.9401
	.5910	-.119		.9300	1.0519	1.0990		.5830	.9653	.9298
	.6390	-.104		1.0000	1.0464	1.0842		.6250	.9913	.9803
	.6870	-.080	St'bd rake	.0177	.5976	.3564		.6670	.9861	.9700
	.7350	-.049		.0443	.7270	.5248		.7080	.9834	.9648
	.7845	-.019		.0797	.8038	.6386		.7500	.9839	.9659
	.8310	-.044		.1507	.9311	.8614		.7900	.9870	.9720
	.8795	.029		.2920	1.0400	1.0743		.8333	1.0103	1.0183
	.9275	.143		.4340	1.0400	1.0743		.9170	1.0113	1.0204
	.7600	-.014		.5050	1.0376	1.0693		1.0000	1.0103	1.0183
	.8075	-.049		.5750	1.0430	1.0792				
	.8550	-.009		.6460	1.0400	1.0743				
	.9045	.089		.7180	1.0376	1.0693				
St'bd hull	.9520	.212		.7890	1.0400	1.0743				
				.8590	1.0464	1.0842				
				.9300	1.0493	1.0891				
				1.0000	1.0493	1.0891				

8191-1

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(K) $n = 124.19$ rps $\frac{U_\infty}{ND} = .814$ $\alpha = -.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.593	Port rake	.0177	.4339	.1864	Wake rake	.0000	.4920	.2416
	.0625	.002		.0443	.5513	.3023		.0833	.6786	.4596
	.1107	-.122		.0797	.6274	.3909		.1667	.8306	.6884
	.1587	-.150		.1507	.7462	.5545		.2081	.9214	.8471
	.2068	-.186		.2920	.9183	.8409		.2500	1.0021	1.0020
	.2545	-.185		.4340	.9805	.9568		.2919	.8947	.7986
	.3025	-.184		.5050	1.0213	1.0386		.3338	.8978	.8042
	.3510	-.172		.5750	1.0143	1.0250		.3750	.9385	.8786
	.3985	-.172		.6460	1.0173	1.0295		.4170	.9511	.9027
	.4470	-.177		.7180	1.0187	1.0318		.4580	.9611	.9215
	.4950	-.150		.7890	1.0187	1.0341		.5000	.9630	.9253
	.5430	-.138		.8590	1.0430	1.0841		.5420	.9638	.9267
	.5910	-.106		.9300	1.0470	1.0909		.5830	.9640	.9272
	.6390	-.097		1.0000	1.0405	1.0773		.6250	.9955	.9888
	.6870	-.068						.6670	.9961	.9891
St'd hull	.7350	-.043	St'd rake	.0177	.6141	.3750		.7080	.9943	.9865
	.7845	-.025		.0443	.7367	.5409		.7500	.9961	.9898
	.8310	-.036		.0797	.8026	.6409		.7900	.9969	.9917
	.8795	.022		.1507	.9276	.8568		.8333	1.0200	1.0382
	.9275	.136		.2920	1.0243	1.0432		.9170	1.0206	1.0392
				.4340	1.0243	1.0455		1.0000	1.0217	1.0416
				.5050	1.0362	1.0705				
				.5750	1.0362	1.0705				
				.6460	1.0362	1.0705				
				.7180	1.0350	1.0682				
				.7890	1.0362	1.0705				
				.8590	1.0378	1.0727				
				.9300	1.0416	1.0795				
				1.0000	1.0416	1.0818				

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20$

(1) $n = 133.33$ rps $\frac{U}{nD} = .757$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0144	.610	Port rake	.0177	.4502	.2027	Wake rake	.0000	.5113	.2608
	.0625	.018		.0443	.5522	.3030		.0833	.7279	.5288
	.1107	-.109		.0797	.6397	.4077		.1667	.8863	.7839
	.1587	-.143		.1507	.7547	.5672		.2081	.9761	.9507
	.2068	-.170		.2920	.9337	.8679		.2500	1.0605	1.1223
	.2545	-.174		.4340	.9853	.9658		.2919	.9101	.8265
	.3025	-.175		.5050	1.0205	1.0364		.3338	.9039	.8151
	.3510	-.173		.5750	1.0191	1.0319		.3750	.9423	.8860
	.3985	-.168		.6460	1.0244	1.0433		.4170	.9511	.9026
	.4470	-.177		.7180	1.0231	1.0410		.4580	.9627	.9247
	.4950	-.143		.7890	1.0216	1.0387		.5000	.9615	.9224
	.5430	-.143		.8590	1.0478	1.0911		.5420	.9637	.9267
	.5910	-.120		.9300	1.0464	1.0888		.5830	.9673	.9337
	.6390	-.095		1.0000	1.0434	1.0820		.6250	1.0005	.9989
	.6870	-.072						.6670	1.0022	1.0022
	.7350	-.047	St'bd rake	.0177	.6035	.3622		.7080	.9994	.9965
	.7845	-.022		.0443	.7243	.5216		.7500	1.0010	.9999
	.8310	-.045		.0797	.7933	.6264		.7900	.9985	.9947
	.8795	.020		.1507	.9124	.8269		.8333	1.0233	1.0448
	.9275	.136		.2920	1.0261	1.0478		.9170	1.0265	1.0514
				.4340	1.0314	1.0569		1.0000	1.0240	1.0462
				.5050	1.0380	1.0729				
St'bd hull	.7600	-.027		.5750	1.0380	1.0729				
	.8075	-.070		.6460	1.0354	1.0661				
	.8550	-.004		.7180	1.0368	1.0706				
	.9045	.075		.7890	1.0368	1.0706				
	.9520	.214		.8590	1.0434	1.0843				
				.9300	1.0464	1.0888				
				1.0000	1.0434	1.0843				

8191-1

L-1618

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(M) $n = 95.82$ rps $\frac{U_\infty}{nD} = .713$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Ste- tion	y/h	u_1/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0144	.630	Port rake	.0177	.4496	.2050	Wake rake	.0000	.4675	.2181
	.0625	.005		.0443	.5631	.3200		.0833	.7423	.5498
	.1107	-.120		.0797	.6399	.4100		.1667	.8975	.8037
	.1587	-.170		.1507	.7695	.6000		.2081	.9915	.9808
	.2068	-.215		.2920	.9448	.9000		.2500	1.0518	1.1037
	.2545	-.212		.4340	.9950	1.0000		.2919	.8596	.7371
	.3025	-.210		.5050	1.0346	1.0750		.3338	.8860	.7832
	.3510	-.190		.5750	1.0316	1.0700		.3750	.9262	.8559
	.3985	-.175		.6460	1.0225	1.0550		.4170	.9540	.9082
	.4470	-.165		.7180	1.0250	1.0600		.4580	.9625	.9245
	.4950	-.155		.7890	1.0546	1.1200		.5000	.9610	.9214
	.5430	-.145		.8590	1.0580	1.1250		.5420	.9637	.9265
	.5910	-.110		.9300	1.0463	1.1050		.5830	.9578	.9153
	.6390	-.100		1.0000				.6250	.9827	.9634
	.6870	-.080						.6670	.9780	.9542
	.7350	-.055						.7080	.9832	.9644
St 'bd hull	.7845	-.020	St 'bd rake	.0177	.5959	.3550		.7500	.9842	.9664
	.8310	-.050		.0443	.7169	.5200		.7900	.9827	.9634
	.8795	.025		.0797	.7695	.6000		.8333	1.0023	1.0023
	.9275	.130		.1507	.9189	.8500		.9170	1.0018	1.0013
				.2920	1.0346	1.0750		1.0000	1.0028	1.0033
				.4340	1.0400	1.0900				
				.5050	1.0463	1.1050				
				.5750	1.0463	1.1000				
				.6460	1.0434	1.0950				
				.7180	1.0434	1.0950				
				.7890	1.0434	1.0950				
				.8590	1.0463	1.1000				
				.9300	1.0434	1.0950				
				1.0000	1.0463	1.1050				

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(n) $n = 108.11$ rps $\frac{U_\infty}{nD} = .628$ $\alpha = -0.5^\circ$

Sta- tion	y/h	U_1/U_∞	q_1/q_∞
Port rake	.0177	.4522	.2071
	.0443	.5664	.3232
	.0797	.6437	.4192
	.1507	.7739	.6061
	.2920	.9437	.8990
	.4340	1.0008	1.0051
	.5050	1.0376	1.0808
	.5750	1.0255	1.0556
	.6460	1.0346	1.0758
	.7180	1.0286	1.0657
	.7890	1.0346	1.0758
	.8590	1.0578	1.1263
.9300	1.0524	1.1162	
1.0000	1.0524	1.1111	
St'bd rake	.0177	.5932	.3535
	.0443	.7247	.5303
	.0797	.7899	.6313
	.1507	.9271	.8636
	.2920	1.0406	1.0909
	.4340	1.0376	1.0808
	.5050	1.0460	1.1010
	.5750	1.0430	1.0960
	.6460	1.0406	1.0909
	.7180	1.0406	1.0909
	.7890	1.0406	1.0909
	.8590	1.0406	1.0909
.9300	1.0430	1.0960	
1.0000	1.0460	1.1010	

Sta- tion	x/l	C_p
Port hull	.0144	.626
	.0625	.010
	.1107	-.116
	.1587	-.166
	.2068	-.191
	.2545	-.192
	.3025	-.191
	.3510	-.176
	.3985	-.171
	.4470	-.167
	.4950	-.161
	.5430	-.131
	.5910	-.111
	.6390	-.101
	.6870	-.076
.7350	-.050	
.7845	-.035	
.8310	-.040	
.8795	.010	
.9275	.131	
St'bd hull	.7600	-.025
	.8075	-.070
	.8550	-.020
	.9045	.070
.9520	.191	

Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Wake rake	.0000	.5054	.2548
	.0833	.8277	.6835
	.1667	1.0168	1.0315
	.2081	1.1198	1.2511
	.2500	1.1821	1.3940
	.2919	.8688	.7529
	.3338	.9062	.8192
	.3750	.7361	.8741
	.4170	.9541	.9083
	.4580	.9607	.9207
	.5000	.9558	.9114
	.5420	.9628	.9248
	.5830	.9585	.9165
	.6250	.9853	.9684
	.6670	.9778	.9538
	.7080	.9853	.9684
	.7500	.9795	.9570
	.7900	.9841	.9662
	.8333	1.0050	1.0077
	.9170	1.0081	1.0139
	1.0000	1.0065	1.0108

8191-1

TABLE 5 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(0) $n = 120.51$ rps $\frac{U_\infty}{nD} = .564$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0144	.604	Port rake	.0177	.4437	.1931	Wake rake	.0000	.5500	.3019
	.0625	-.009		.0443	.5611	.3119		.0833	.8903	.7908
	.1107	-.138		.0797	.6381	.4010		.1667	1.1178	1.2466
	.1587	-.158		.1507	.7732	.5891		.2081	1.2299	1.5091
	.2068	-.203		.2920	.9494	.8911		.2500	1.2718	1.6136
	.2545	-.200		.4340	1.0035	.9950		.2919	.8909	.7917
	.3025	-.198		.5050	1.0420	1.0743		.3338	.9052	.8176
	.3510	-.198		.5750	1.0275	1.0446		.3750	.9323	.8672
	.3985	-.178		.6460	1.0365	1.0594		.4170	.9549	.9097
	.4470	-.188		.7180	1.0275	1.0446		.4580	.9640	.9272
	.4950	-.163		.7890	1.0335	1.0545		.5000	.9516	.9034
	.5430	-.138		.8590	1.0514	1.0941		.5420	.9608	.9210
	.5910	-.104		.9300	1.0540	1.0990		.5830	.9604	.9200
	.6390	-.098		1.0000	1.0485	1.0842		.6250	.9890	.9758
St'bd hull	.6870	-.081	St'bd rake	.0177	.6241	.3812	St'bd rake	.6670	.9801	.9581
	.7350	-.054		.0443	.7452	.5495		.7080	.9853	.9686
	.7845	-.039		.0797	.8169	.6584		.7500	.9868	.9716
	.8310	-.054		.1507	.9461	.8861		.7900	.9858	.9695
	.8795	.019		.2920	1.0451	1.0792		.8333	1.0103	1.0181
	.9275	.118		.4340	1.0396	1.0693		.9170	1.0092	1.0161
	.7600	-.029		.5050	1.0514	1.0891		1.0000	1.0107	1.0192
	.8075	-.084		.5750	1.0514	1.0941				
	.8550	-.019		.6460	1.0485	1.0842				
	.9045	.064		.7180	1.0514	1.0891				
	.9520	.183		.7890	1.0514	1.0941				
				.8590	1.0540	1.0990				
				.9300	1.0540	1.0990				
				1.0000	1.0540	1.0990				

TABLE 5 Concluded
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 20^\circ$

(P) $n = 133.33$ rps $\frac{U}{ND} = .508$ $\alpha = -.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_{∞}	q_1/q_{∞}	Sta- tion	z/h	u_1/u_{∞}	q_1/q_{∞}
Port hull	.0144	.629	Port rake	.0177	.4725	.2234	Wake rake	.0000	.5803	.3362
	.0625	.020		.0443	.5795	.3401		.0833	.9586	.9169
	.1107	-.111		.0797	.6642	.4467		.1667	1.2260	1.4996
	.1587	.152		.1507	.7956	.6396		.2081	1.3552	1.8326
	.2068	.169		.2920	.9716	.9492		.2500	1.3591	1.8430
	.2545	.186		.4340	1.0157	1.0406		.2919	.9232	.8502
	.3025	.208		.5050	1.0279	1.0609		.3338	.9147	.8346
	.3510	.177		.5750	1.0309	1.0711		.3750	.9466	.8940
	.3985	.180		.6460	1.0430	1.0914		.4170	.9581	.9158
	.4470	.170		.7180	1.0309	1.0711		.4580	.9569	.9138
	.4950	.162		.7890	1.0370	1.0812		.5000	.9466	.8940
	.5430	.152		.8590	1.0603	1.1320		.5420	.9608	.9210
	.5910	.116		.9300	1.0603	1.1320		.5830	.9591	.9178
	.6390	.101		1.0000	1.0455	1.1015		.6250	.9934	.9845
	.6870	.080						.6670	.9860	.9699
	.7350	.055	St'bd rake	.0177	.6008	.3604		.7080	.9876	.9730
St'bd hull	.7845	.040		.0443	.7229	.5228		.7500	.9855	.9689
	.8310	.050		.0797	.7918	.6345		.7900	.9891	.9761
	.8795	.005		.1507	.9191	.8477		.8333	1.0085	1.0147
	.9275	.106		.2920	1.0400	1.0863		.9170	1.0172	1.0323
				.4340	1.0430	1.0964		1.0000	1.0100	1.0178
	.7600	-.030		.5050	1.0549	1.1218				
	.8075	-.081		.5750	1.0549	1.1168				
	.8550	-.020		.6460	1.0549	1.1218				
	.9045	.066		.7180	1.0549	1.1218				
	.9520	.167		.7890	1.0549	1.1168				

81618-1

TABLE 6
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(a) $n = 71.17$ rps $\frac{U}{nD} = 1.436$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.581	Port rake	.0177	.4139	.1693	Wake rake	.0000	.4721	.2223
	.0625	-.015		.0443	.5364	.2851		.0833	.5979	.3567
	.1107	-.133		.0797	.6131	.3742		.1667	.7256	.5252
	.1587	-.167		.1507	.7360	.5367		.2081	.7922	.6262
	.2068	-.193		.2920	.9108	.8241		.2500	.8431	.7091
	.2545	-.192		.4340	.9853	.9621		.2919	.8466	.7151
	.3025	-.191		.5050	1.0266	1.0468		.3338	.8862	.7837
	.3510	-.182		.5750	1.0211	1.0334		.3750	.9239	.8517
	.3985	-.175		.6460	1.0211	1.0356		.4170	.9489	.8985
	.4470	-.162		.7180	1.0211	1.0334		.4580	.9684	.9356
	.4950	-.151		.7890	1.0184	1.0290		.5000	.9751	.9486
	.5430	-.147		.8590	1.0518	1.0980		.5420	.9741	.9468
	.5910	-.109		.9300	1.0518	1.0980		.5830	.9749	.9480
	.6390	-.100		1.0000	1.0440	1.0824		.6250	1.0046	1.0070
	.6870	-.074	St'bd rake	.0177	.6067	.3653		.6670	1.0029	1.0036
	.7350	-.044		.0443	.7344	.5345		.7080	1.0023	1.0023
	.7845	-.033		.0797	.7975	.6303		.7500	1.0036	1.0050
	.8310	-.044		.1507	.9200	.8396		.7900	1.0019	1.0014
	.8795	.029		.2920	1.0360	1.0646		.8333	1.0245	1.0472
	.9275	.149		.4340	1.0360	1.0646		.89170	1.0232	1.0445
				.5050	1.0427	1.0780		1.0000	1.0254	1.0491
				.5750	1.0440	1.0802				
				.6460	1.0427	1.0780				
				.7180	1.0440	1.0824				
St'bd hull	.7600	-.024		.7890	1.0427	1.0780				
	.8075	-.060		.8590	1.0493	1.0913				
	.8550	-.015		.9300	1.0493	1.0913				
	.9045	.086		1.0000	1.0493	1.0913				
	.9520	.236								

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(b) $n = 80.01$ rps $\frac{U}{nD} = 1.275$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_{∞}	q_1/q_{∞}	Sta- tion	z/h	u_1/U_{∞}	q_1/q_{∞}
Port hull	.0144	.614	Port rake	.0177	.4219	.1779	Wake rake	.0000	.4695	.2199
	.0625	.018		.0443	.5402	.2905		.0833	.6041	.3641
	.1107	.121		.0797	.6211	.3851		.1667	.7434	.5515
	.1587	.144		.1507	.7453	.5563		.2081	.8115	.6570
	.2068	.189		.2920	.9322	.8671		.2500	.8622	.7416
	.2545	.194		.4340	.9871	.9752		.2919	.8424	.7081
	.3025	.195		.5050	1.0178	1.0360		.3338	.8788	.7705
	.3510	.184		.5750	1.0123	1.0225		.3750	.9167	.8383
	.3985	.175		.6460	1.0162	1.0315		.4170	.9422	.8858
	.4470	.177		.7180	1.0123	1.0248		.4580	.9618	.9230
	.4950	.153		.7890	1.0135	1.0270		.5000	.9700	.9388
	.5430	.144		.8590	1.0393	1.0788		.5420	.9693	.9374
	.5910	.122		.9300	1.0405	1.0833		.5830	.9717	.9420
	.6390	.105		1.0000	1.0380	1.0766		.6250	.9993	.9954
	.6870	.079						.6670	.9985	.9946
	.7350	.054						.7080	.9987	.9950
St'bd hull	.7845	.031	St'bd rake	.0177	.6006	.3604		.7500	.9991	.9960
	.8310	.054		.0443	.7147	.5113		.7900	1.0001	.9978
	.8795	.022		.0797	.7920	.6261		.8333	1.0251	1.0434
	.9275	.146		.1507	.9126	.8311		.9170	1.0240	1.0462
				.2920	1.0231	1.0473		1.0000	1.0255	1.0494
				.4340	1.0272	1.0541				

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(c) $n = 88.94$ rps $\frac{U_\infty}{nD} = 1.147$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.608	Port rake	.0177	.4348	.1892	Wake rake	.0000	.4762	.2263
	.0625	.004		.0443	.5548	.3086		.0833	.6434	.4130
	.1107	-.132		.0797	.6320	.4009		.1667	.7772	.6025
	.1587	-.162		.1507	.7484	.5608		.2081	.8503	.7214
	.2068	-.200		.2920	.9334	.8716		.2500	.9009	.8097
	.2545	-.201		.4340	.9827	.9662		.2919	.8506	.7220
	.3025	-.200		.5050	1.0213	1.0428		.3338	.8850	.7814
	.3510	-.184		.5750	1.0131	1.0270		.3750	.9231	.8501
	.3985	-.182		.6460	1.0173	1.0360		.4170	.9441	.8891
	.4470	-.170		.7180	1.0158	1.0315		.4580	.9638	.9268
	.4950	-.159		.7890	1.0186	1.0383		.5000	.9689	.9365
	.5430	-.146		.8590	1.0509	1.1036		.5420	.9713	.9412
	.5910	-.112		.9300	1.0481	1.0991		.5830	.9698	.9384
	.6390	-.105		1.0000	1.0413	1.0856		.6250	1.0001	.9979
St'd hull	.6870	-.079	St'd rake	.0177	.6076	.3694		.6670	1.0009	.9998
	.7350	-.049		.0443	.7279	.5293		.7080	1.0001	.9979
	.7845	-.024		.0797	.7972	.6351		.7500	1.0017	1.0011
	.8310	-.051		.1507	.9122	.8311		.7900	1.0022	1.0021
	.8795	.015		.2920	1.0226	1.0473		.8333	1.0247	1.0476
	.9275	.139		.4340	1.0268	1.0541		.9170	1.0194	1.0369
				.5050	1.0389	1.0788		1.0000	1.0251	1.0486
				.5750	1.0347	1.0698				
				.6460	1.0347	1.0721				
				.7180	1.0347	1.0721				

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(d) $n = 97.77$ rps $\frac{U_\infty}{nD} = 1.040$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.615	Port rake	.0177	.4392	.1945	Wake rake	.0000	.4848	.2346
	.0625	.006		.0443	.5522	.3066		.0833	.6517	.4238
	.1107	-.125		.0797	.6345	.4050		.1667	.7947	.6302
	.1587	-.155		.1507	.7569	.5767		.2081	.8751	.7641
	.2068	-.201		.2920	.9370	.8856		.2500	.9554	.9106
	.2545	-.198		.4340	.9865	.9817		.2919	.8974	.8035
	.3025	-.194		.5050	1.0252	1.0595		.3338	.8921	.7941
	.3510	-.189		.5750	1.0197	1.0481		.3750	.9275	.8582
	.3985	-.180		.6460	1.0213	1.0503		.4170	.9418	.8849
	.4470	-.170		.7180	1.0197	1.0481		.4580	.9610	.9214
	.4950	-.162		.7890	1.0225	1.0549		.5000	.9675	.9341
	.5430	-.160		.8590	1.0440	1.1007		.5420	.9688	.9364
	.5910	-.121		.9300	1.0440	1.1007		.5830	.9702	.9392
	.6390	-.112		1.0000	1.0416	1.0938		.6250	.9995	.9968
St'bd hull	.6870	-.090	St'bd rake	.0177	.6123	.3776		.6670	.9991	.9959
	.7350	-.070		.0443	.7269	.5332		.7080	1.0006	.9991
	.7845	-.034		.0797	.8003	.6453		.7500	.9988	.9955
	.8310	-.061		.1507	.9233	.8604		.7900	1.0232	1.0446
	.8795	.004		.2920	1.0266	1.0618		.8333	1.0199	1.0380
	.9275	.130		.4340	1.0293	1.0686		.9170	1.0232	1.0446
	.7600	-.032		.5050	1.0386	1.0870		1.0000		
	.8075	-.066		.5750	1.0386	1.0892				
	.8550	-.011		.6460	1.0376	1.0847				
	.9045	.082		.7180	1.0386	1.0870				
	.9520	.217		.7890	1.0386	1.0870				
				.8590	1.0430	1.0961				
				.9300	1.0440	1.1007				
				1.0000	1.0440	1.0984				

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25$

(e) $n = 67.00$ rps $\frac{U_\infty}{nD} = 1.022$ $\alpha = -5.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0144	.591	Port rake	.0177	.4158	.1786	Wake rake	.0000	.5208	.2706
	.0625	-.030		.0443	.5267	.2857		.0833	.7434	.5515
	.1107	-.163		.0797	.6180	.3878		.1667	.8620	.7414
	.1587	-.188		.1507	.7448	.5663		.2081	.9291	.8613
	.2068	-.224		.2920	.9229	.8673		.2500	.9341	.8705
	.2545	-.204		.4340	.9836	.9847		.2919	.8662	.7486
	.3025	-.204		.5050	1.0240	1.0714		.3338	.9002	.8086
	.3510	-.204		.5750	1.0240	1.0663		.3750	.9302	.8633
	.3985	-.185		.6460	1.0116	1.0459		.4170	.9581	.9160
	.4470	-.185		.7180	1.0179	1.0561		.4580	.9716	.9418
	.4950	-.180		.7890	1.0143	1.0510		.5000	.9763	.9511
	.5430	-.178		.8590	1.0509	1.1276		.5420	.9763	.9511
	.5910	-.150		.9300	1.0479	1.1173		.5830	.9768	.9521
	.6390	-.132		1.0000	1.0414	1.1071		.6250	.9988	.9955
St'bd hull	.6870	-.101	St'bd rake	.0177	.5826	.3469		.6670	.9994	.9965
	.7350	-.076		.0443	.7158	.5204		.7080	.9963	.9903
	.7845	-.040		.0797	.8010	.6531		.7500	.9983	.9945
	.8310	-.081		.1507	.9291	.8827		.7900	.9994	.9965
	.8795	-.015		.2920	1.0360	1.0918		.8333	1.0290	1.0564
	.9275	.102		.4340	1.0295	1.0816		.9170	1.0290	1.0564
				.5050	1.0390	1.1020		1.0000	1.0285	1.0553
	.7600	-.051		.5750	1.0390	1.0969				
	.8075	-.086		.6460	1.0414	1.1071				
	.8550	-.030		.7180	1.0390	1.0969				
	.9045	.051		.7890	1.0390	1.1020				
	.9520	.209		.8590	1.0533	1.1327				
				.9300	1.0533	1.1327				
				1.0000	1.0533	1.1327				

TABLE 6 Continued
 CHORDWISE PRESSURE--DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(f) $n = 106.38$ rps $\frac{U}{ND} = .956$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0144	.605	Port rake	.0177	.4392	.1919	Wake rake	.0000	.5262	.2763
	.0625	.004		.0443	.5570	.3093		.0833	.6517	.4238
	.1107	-.121		.0797	.6345	.3995		.1667	.8074	.6504
	.1587	-.153		.1507	.7535	.5643		.2081	.8947	.7987
	.2068	-.189		.2920	.9310	.8623		.2500	1.0017	1.0010
	.2545	-.190		.4340	.9865	.9684		.2919	.9896	.9772
	.3025	-.189		.5050	1.0225	1.0406		.3338	.9162	.8376
	.3510	-.180		.5750	1.0197	1.0339		.3750	.9511	.9027
	.3985	-.173		.6460	1.0213	1.0384		.4170	.9367	.8756
	.4470	-.180		.7180	1.0184	1.0316		.4580	.9561	.9120
	.4950	-.155		.7890	1.0213	1.0384		.5000	.9644	.9279
	.5430	-.144		.8590	1.0496	1.0971		.5420	.9646	.9285
	.5910	-.122		.9300	1.0483	1.0926		.5830	.9675	.9341
	.6390	-.101		1.0000	1.0416	1.0790		.6250	.9976	.9931
	.6870	-.075	St'bd rake	.0177	.6049	.3657		.6670	.9983	.9945
	.7350	-.045		.0443	.7249	.5237		.7080	.9978	.9935
	.7845	-.027		.0797	.7965	.6321		.7500	.9988	.9955
	.8310	-.040		.1507	.9033	.8126		.7900	.9986	.9949
	.8795	.018		.2920	1.0158	1.0248		.8333	1.0227	1.0436
	.9275	.137		.4340	1.0293	1.0542		.9170	1.0215	1.0412
				.5050	1.0321	1.0609		1.0000	1.0218	1.0418
St'bd hull	.7600	-.020	St'bd rake	.5750	1.0348	1.0655				
	.8075	-.054		.6460	1.0321	1.0587				
	.8550	-.006		.7180	1.0321	1.0609				
	.9045	.081		.7890	1.0348	1.0655				
	.9520	.214		.8590	1.0430	1.0813				

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(g) $n = 74.18$ rps $\frac{U}{ND} = .922$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0144	.592	Port rake	.0177	.4436	.1990	Wake rake	.0000	.5089	.2584
	.0625	.000		.0443	.5556	.3035		.0833	.7732	.5964
	.1107	-.129		.0797	.6381	.4030		.1667	.9059	.8186
	.1587	-.159		.1507	.7699	.5871		.2081	.9742	.9469
	.2068	-.194		.2920	.9591	.9154		.2500	.9603	.9200
	.2545	-.201		.4340	.9999	.9950		.2919	.8702	.7556
	.3025	-.209		.5050	1.0275	1.0498		.3338	.9030	.8135
	.3510	-.194		.5750	1.0335	1.0597		.3750	.9335	.8694
	.3985	-.184		.6460	1.0245	1.0398		.4170	.9640	.9272
	.4470	-.194		.7180	1.0149	1.0249		.4580	.9731	.9447
	.4950	-.164		.7890	1.0184	1.0299		.5000	.9769	.9520
	.5430	-.159		.8590	1.0514	1.0995		.5420	.9769	.9520
	.5910	-.114		.9300	1.0450	1.0846		.5830	.9773	.9530
	.6390	-.109		1.0000	1.0484	1.0896		.6250	.9972	.9923
	.6870	-.070	St'bd rake	.0177	.5829	.3383		.6670	1.0035	1.0047
St'bd hull	.7350	-.054		.0443	.7067	.4975		.7080	.9999	.9975
	.7845	-.034		.0797	.7779	.6020		.7500	1.0009	.9995
	.8310	-.054		.1507	.8990	.8060		.7900	1.0015	1.0006
	.8795	.010		.2920	1.0245	1.0448		.8333	1.0254	1.0492
	.9275	.134		.4340	1.0396	1.0746		.9170	1.0245	1.0471
				.5050	1.0484	1.0896		1.0000	1.0245	1.0471
				.5750	1.0450	1.0846				
				.6460	1.0419	1.0796				
				.7180	1.0419	1.0796				
				.7890	1.0396	1.0697				
				.8590	1.0419	1.0796				
				.9300	1.0484	1.0896				
				1.0000	1.0450	1.0846				

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(h) $n = 115.27$ rps $\frac{U}{ND} = .880$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0144	.617	Port rake	.0177	.4373	.1913	Wake rake	.0000	.5651	.3185
	.0625	.013		.0443	.5604	.3144		.0833	.6893	.4741
	.1107	.111		.0797	.6380	.4077		.1667	.8469	.7155
	.1587	.145		.1507	.7602	.5786		.2081	.9367	.8753
	.2068	.186		.2920	.9447	.8929		.2500	1.0536	1.1075
	.2545	.185		.4340	.9923	.9863		.2919	1.0389	1.0768
	.3025	.184		.5050	1.0216	1.0433		.3338	.9288	.8608
	.3510	.175		.5750	1.0177	1.0364		.3750	.9617	.9228
	.3985	.170		.6460	1.0188	1.0387		.4170	.9329	.8683
	.4470	.164		.7180	1.0163	1.0319		.4580	.9524	.9049
	.4950	.157		.7890	1.0177	1.0342		.5000	.9595	.9186
	.5430	.145		.8590	1.0460	1.0934		.5420	.9624	.9242
	.5910	.122		.9300	1.0435	1.0868		.5830	.9669	.9327
	.6390	.102		1.0000	1.0367	1.0752		.6250	.9996	.9970
	.6870	.077						.6670	1.0008	.9993
St'bd hull	.7350	.047	St'bd rake	.0177	.6061	.3690		.7080	.9996	.9970
	.7845	.018		.0443	.7263	.5262		.7500	1.0001	.9979
	.8310	.047		.0797	.7961	.6333		.7900	.9994	.9965
	.8795	.011		.1507	.9145	.8360		.8333	1.0229	1.0440
	.9275	.132		.2920	1.0216	1.0433		.9170	1.0266	1.0515
				.4340	1.0271	1.0547		1.0000	1.0229	1.0440
	.7600	-.015		.5050	1.0326	1.0661				
	.8075	-.056		.5750	1.0311	1.0638				
	.8550	-.015		.6460	1.0340	1.0683				
	.9045	.075		.7180	1.0326	1.0661				
	.9520	.207		.7890	1.0326	1.0661				
				.8590	1.0406	1.0820				
				.9300	1.0406	1.0820				
				1.0000	1.0395	1.0797				

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(1) $n = 81.32$ rps $\frac{U}{nD} = .837$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0144	.616	Port rake	.0177	.4542	.2124	Wake rake	.0000	.5454	.2967
	.0625	-.031		.0443	.5753	.3368		.0833	.8193	.6696
	.1107	-.155		.0797	.6561	.4404		.1667	.9660	.9308
	.1587	-.196		.1507	.7820	.6269		.2081	1.0309	1.0604
	.2068	-.214		.2920	.9643	.9482		.2500	.9848	.9674
	.2545	-.225		.4340	1.0177	1.0570		.2919	.8725	.7595
	.3025	-.228		.5050	1.0452	1.1140		.3338	.9073	.8211
	.3510	-.228		.5750	1.0452	1.1140		.3750	.9345	.8713
	.3985	-.217		.6460	1.0422	1.1088		.4170	.9654	.9298
	.4470	-.222		.7180	1.0330	1.0933		.4580	.9735	.9455
	.4950	-.196		.7890	1.0300	1.0829		.5000	.9795	.9570
	.5430	-.186		.8590	1.0595	1.1503		.5420	.9751	.9486
	.5910	-.155		.9300	1.0654	1.1606		.5830	.9783	.9548
	.6390	-.139		1.0000	1.0570	1.1451		.6250	.9973	.9924
St'd hull	.6870	-.108	St'd rake	.0177	.5958	.3627		.6670	1.0000	.9977
	.7350	-.082		.0443	.7200	.5285		.7080	.9948	.9873
	.7845	-.072		.0797	.7933	.6477		.7500	1.0000	.9977
	.8310	-.093		.1507	.9175	.8601		.7900	1.0000	.9977
	.8795	-.020		.2920	1.0330	1.0933		.8333	1.0243	1.0468
	.9275	.098		.4340	1.0452	1.1192		.9170	1.0248	1.0478
				.5050	1.0540	1.1347		1.0000	1.0264	1.0509
	.7600	-.051		.5750	1.0570	1.1399				
	.8075	-.114		.6460	1.0540	1.1347				
	.8550	-.062		.7180	1.0540	1.1347				
	.9045	.041		.7890	1.0506	1.1295				
	.9520	.176		.8590	1.0506	1.1295				
				.9300	1.0540	1.1347				
				1.0000	1.0570	1.1451				

(1) $\alpha = 126.19$ rds $\frac{d\alpha}{dt} = .815$ $\alpha = -0.5$

Station	y/h	U_1/U_{∞}	q_1/q_{∞}
Port rake	.0177	.4444	.1991
	.0443	.5619	.3194
	.0797	.6373	.4120
	.1507	.7587	.5810
	.2920	.9320	.8796
	.4340	.9909	.9931
	.5050	1.0215	1.0556
	.5750	1.0189	1.0486
	.6460	1.0215	1.0556
	.7180	1.0189	1.0486
	.7890	1.0203	1.0509
	.8590	1.0500	1.1157
	.9300	1.0487	1.1111
	1.0000	1.0433	1.0995
St'bd rake	.0177	.6034	.3681
	.0443	.7282	.5370
	.0797	.8022	.6505
	.1507	.9259	.8681
	.2920	1.0270	1.0671
	.4340	1.0270	1.0671
	.5050	1.0407	1.0949
	.5750	1.0393	1.0926
	.6460	1.0367	1.0856
	.7180	1.0407	1.0949
	.7890	1.0378	1.0903
	.8590	1.0433	1.0995
	.9300	1.0446	1.1042
	1.0000	1.0446	1.1042

Station	x/l	C_p
Port hull	.0144	.606
	.0625	.000
	.127	.127
	.107	.107
	.1587	.169
	.2068	.199
	.2545	.200
	.3025	.199
	.3510	.189
	.3985	.182
	.4470	.185
	.4950	.159
	.5430	.150
	.5910	.113
St'bd hull	.6390	.101
	.6870	.077
	.7350	.053
	.7845	.030
	.8310	.050
	.8795	.006
	.9275	.125
	.7600	-.032
	.8075	-.055
	.8550	-.018
	.9045	.064
	.9520	.206

Station	z/h	U_1/U_{∞}	q_1/q_{∞}
Wake rake	.0000	.5951	.3532
	.0833	.7219	.5200
	.1667	.8915	.7930
	.2081	.9865	.9710
	.2500	1.1007	1.2086
	.2919	1.0495	1.0991
	.3338	.9368	.8757
	.3750	.9677	.9343
	.4170	.9376	.8771
	.4580	.9554	.9106
	.5000	.9611	.9215
	.5420	.9631	.9253
	.5830	.9664	.9319
	.6250	.9980	.9937
	.6670	.9988	.9951
	.7080	.9959	.9895
	.7500	.9975	.9929
	.7900	.9980	.9937
	.8333	1.0213	1.0405
	.9170	1.0238	1.0458
	1.0000	1.0223	1.0429

TABLE 6 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(k) $n = 88.53$ rps $\frac{U}{nD} = .765$ $\alpha = -5^\circ$

Station	x/l	C_p	Station	y/h	U/U_∞	q_1/q_∞	Station	z/h	U/U_∞	q_1/q_∞
Port hull	.0144	.609	Port rake	.0177	.4482	.2031	Wake rake	.0000	.5706	.3250
	.0625	-.026		.0443	.5614	.3229		.0833	.8529	.7258
	.1107	-.151		.0797	.6397	.4167		.1667	1.0117	1.0213
	.1587	-.187		.1507	.7661	.5938		.2081	1.0755	1.1541
	.2068	-.239		.2920	.9458	.9115		.2500	.9868	.9716
	.2545	-.235		.4340	1.0070	1.0313		.2919	.8791	.7712
	.3025	-.239		.5050	1.0406	1.1042		.3338	.9140	.8334
	.3510	-.213		.5750	1.0380	1.0990		.3750	.9402	.8819
	.3985	-.218		.6460	1.0350	1.0938		.4170	.9701	.9389
	.4470	-.218		.7180	1.0319	1.0833		.4580	.9760	.9505
	.4950	-.192		.7890	1.0289	1.0781		.5000	.9782	.9547
	.5430	-.187		.8590	1.0556	1.1354		.5420	.9772	.9527
	.5910	-.156		.9300	1.0556	1.1354		.5830	.9792	.9569
	.6390	-.130		1.0000	1.0556	1.1042		.6250	1.0033	1.0043
St'bd hull	.6870	-.114	St'bd rake	.0177	.6100	.3802	St'bd rake	.6670	1.0044	1.0064
	.7350	-.093		.0443	.7278	.5365		.7080	.9980	.9937
	.7845	-.072		.0797	.8057	.6615		.7500	1.0022	1.0022
	.8310	-.093		.1507	.9329	.8854		.7900	1.0027	1.0033
	.8795	-.026		.2920	1.0526	1.1302		.8333	1.0340	1.0665
	.9275	.093		.4340	1.0556	1.1354		.8910	1.0364	1.0719
	.7600	-.057		.5050	1.0592	1.1406		1.0000		
	.8075	-.114		.5750	1.0592	1.1406				
	.8550	-.046		.6460	1.0556	1.1354				
	.9045	.041		.7180	1.0526	1.1302				
	.9520	.177		.7890	1.0556	1.1354				
				.8590	1.0622	1.1458				
				.9300	1.0622	1.1458				
				1.0000	1.0622	1.1510				

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(1) $n = 133.25$ rps $\frac{U_\infty}{nD} = .763$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.618	Port rake	.0177	.4545	.2055	Wake rake	.0000	.6355	.4029
	.0625	.022		.0443	.5679	.3196		.0833	.7675	.5877
	.1107	-.107		.0797	.6473	.4155		.1667	.9521	.9044
	.1587	-.141		.1507	.7691	.5850		.2081	1.0496	1.0992
	.2068	-.160		.2920	.9503	.8973		.2500	1.1340	1.2831
	.2545	-.178		.4340	.9938	.9817		.2919	1.0127	1.0233
	.3025	-.180		.5050	1.0276	1.0502		.3338	.9188	.8423
	.3510	-.180		.5750	1.0246	1.0434		.3750	.9493	.8991
	.3985	-.175		.6460	1.0246	1.0434		.4170	.9404	.8826
	.4470	-.180		.7180	1.0261	1.0457		.4580	.9585	.9167
	.4950	-.153		.7890	1.0261	1.0457		.5000	.9622	.9237
	.5430	-.146		.8590	1.0505	1.0959		.5420	.9637	.9267
	.5910	-.109		.9300	1.0518	1.1005		.5830	.9671	.9333
	.6390	-.102		1.0000	1.0451	1.0868		.6250	.9983	.9944
	.6870	-.070	St'bd hull	.0177	.6087	.3676		.6670	.9986	.9949
St'bd hull	.7350	-.045		.0443	.7274	.5251		.7080	.9983	.9944
	.7845	-.020		.0797	.7924	.6233		.7500	.9990	.9959
	.8310	-.047		.1507	.9073	.8174		.7900	.9990	.9959
	.8795	.009		.2920	1.0276	1.0502		.8333	1.0242	1.0465
	.9275	.118		.4340	1.0329	1.0616		.9170	1.0263	1.0508
	.7600	-.018		.5050	1.0451	1.0845		1.0000	1.0242	1.0465
	.8075	-.057		.5750	1.0451	1.0845				
	.8550	-.009		.6460	1.0451	1.0868				
	.9045	.070		.7180	1.0451	1.0845				
	.9520	.196		.7890	1.0464	1.0890				
				.8590	1.0493	1.0936				
				.9300	1.0464	1.0890				
				1.0000	1.0505	1.0959				

8191-1

L-1618

TABLE 6 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25$

(m) $n = 95.71$ rps $\frac{U}{nD} = .711$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.605	Port rake	.0177	.4258	.1895	Wake rake	.0000	.6143	.3765
	.0625	-.036		.0443	.5475	.3105		.0833	.8983	.8052
	.1107	-.163		.0797	.6220	.4000		.1667	1.0669	1.1356
	.1587	-.200		.1507	.7537	.5895		.2081	1.1317	1.2779
	.2068	-.231		.2920	.9483	.9368		.2500	.9852	.9684
	.2545	-.227		.4340	1.0057	1.0474		.2919	.8783	.7697
	.3025	-.221		.5050	1.0334	1.1105		.3338	.9083	.8230
	.3510	-.215		.5750	1.0304	1.1000		.3750	.9349	.8721
	.3985	-.205		.6460	1.0304	1.1000		.4170	.9604	.9202
	.4470	-.190		.7180	1.0304	1.1053		.4580	.9641	.9275
	.4950	-.184		.7890	1.0304	1.1053		.5000	.9664	.9317
	.5430	-.178		.8590	1.0575	1.1579		.5420	.9659	.9307
	.5910	-.164		.9300	1.0545	1.1526		.5830	.9691	.9370
	.6390	-.139		1.0000	1.0456	1.1368		.6250	.9952	.9882
	.6870	-.114	St'bd hull	.0177	.6022	.3737		.6670	.9968	.9914
St'bd hull	.7350	-.089		.0443	.7246	.5474		.7080	.9932	.9841
	.7845	-.073		.0797	.8061	.6737		.7500	.9952	.9882
	.8310	-.094		.1507	.9349	.9053		.7900	.9937	.9850
	.8795	-.026		.2920	1.0456	1.1316		.8333	1.0208	1.0394
	.9275	.089		.4340	1.0456	1.1316		.9170	1.0196	1.0374
	.7600	-.063		.5050	1.0456	1.1316		1.0000	1.0222	1.0425
	.8075	-.100		.5750	1.0456	1.1368				
	.8550	-.052		.6460	1.0456	1.1368				
	.9045	.031		.7180	1.0456	1.1368				
	.9520	.173		.7890	1.0456	1.1368				
				.8590	1.0481	1.1421				
				.9300	1.0481	1.1421				
				1.0000	1.0456	1.1368				

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(n) $n = 102.81$ rps $\frac{U_\infty}{nD} = .661$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0144	.597	Port rake	.0177	.4188	.1804	Wake rake	.0000	.6480	.4191
	.0625	-.010		.0443	.5538	.3093		.0833	.9370	.8759
	.1107	-.170		.0797	.6283	.4021		.1667	1.1282	1.2699
	.1587	-.190		.1507	.7709	.6031		.2081	1.1809	1.3914
	.2068	-.205		.2920	.9586	.9330		.2500	.9835	.9650
	.2545	-.225		.4340	1.0190	1.0515		.2919	.8869	.7848
	.3025	-.232		.5050	1.0283	1.0722		.3338	.9097	.8256
	.3510	-.232		.5750	1.0315	1.0773		.3750	.9331	.8666
	.3985	-.221		.6460	1.0217	1.0619		.4170	.9624	.9241
	.4470	-.221		.7180	1.0253	1.0670		.4580	.9705	.9399
	.4950	-.201		.7890	1.0190	1.0567		.5000	.9717	.9419
	.5430	-.190		.8590	1.0555	1.1289		.5420	.9685	.9357
	.5910	-.149		.9300	1.0586	1.1340		.5830	.9717	.9419
	.6390	-.139		1.0000	1.0520	1.1237		.6250	.9977	.9933
St'd hull	.6870	-.118	St'd rake	.0177	.5815	.3454		.6670	.9988	.9953
	.7350	-.097		.0443	.7289	.5412		.7080	.9962	.9902
	.7845	-.067		.0797	.8030	.6546		.7500	.9977	.9933
	.8310	-.092		.1507	.9325	.8814		.7900	.9988	.9953
	.8795	-.036		.2920	1.0345	1.0876		.8333	1.0217	1.0415
	.9275	.077		.4340	1.0406	1.0979		.9170	1.0227	1.0436
				.5050	1.0466	1.1082		1.0000	1.0217	1.0415
				.5750	1.0520	1.1237				
				.6460	1.0436	1.1031				
				.7180	1.0466	1.1082				
				.7890	1.0466	1.1082				
				.8590	1.0520	1.1237				
				.9300	1.0466	1.1134				
				1.0000	1.0466	1.1134				

TABLE 6 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25$

(a) $n = 110.00$ rps $\frac{U}{ND} = .616$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0144	.611	Port rake	.0177	.4270	.1865	Wake rake	.0000	.7031	.4933
	.0625	-.020		.0443	.5491	.3057		.0833	1.0033	1.0045
	.1107	-.145		.0797	.6485	.4249		.1667	1.2372	1.5273
	.1587	-.165		.1507	.7683	.6010		.2081	1.2440	1.5441
	.2068	-.185		.2920	.9511	.9171		.2500	.9806	.9593
	.2545	-.196		.4340	1.0024	1.0207		.2919	.8856	.7826
	.3025	-.207		.5050	1.0303	1.0777		.3338	.9138	.8331
	.3510	-.186		.5750	1.0303	1.0777		.3750	.9382	.8783
	.3985	-.186		.6460	1.0273	1.0725		.4170	.9660	.9308
	.4470	-.178		.7180	1.0237	1.0674		.4580	.9719	.9425
St'd hull	.4950	-.171	St'd rake	.7890	1.0237	1.0674		.5000	.9724	.9435
	.5430	-.155		.8590	1.0541	1.1295		.5420	.9687	.9361
	.5910	-.124		.9300	1.0605	1.1399		.5830	.9719	.9425
	.6390	-.114		1.0000	1.0486	1.1140		.6250	.9960	.9898
	.6870	-.091		.0177	.5925	.3575		.6670	.9975	.9930
	.7350	-.067		.0443	.7128	.5181		.7080	.9960	.9898
	.7845	-.057		.0797	.7926	.6373		.7500	.9949	.9877
	.8310	-.082		.1507	.9144	.8497		.7900	.9966	.9908
	.8795	-.015		.2920	1.0364	1.0933		.8333	1.0263	1.0508
	.9275	.098		.4340	1.0334	1.0829		.9170	1.0293	1.0572
				.5050	1.0456	1.1088		1.0000	1.0247	1.0477
				.5750	1.0456	1.1088				
				.6460	1.0486	1.1140				
				.7180	1.0486	1.1140				
				.7890	1.0486	1.1140				
				.8590	1.0426	1.1036				
				.9300	1.0486	1.1192				
				1.0000	1.0456	1.1088				

TABLE 6 Concluded
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 25^\circ$

(p) $n = 117.22$ rps $\frac{U}{nD} = .578$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0144	.606	Port rake	.0177	.4344	.1917	Wake rake	.0000	.7425	.5501
	.0625	-.015		.0443	.5548	.3109		.0833	1.0571	1.1150
	.1107	-.145		.0797	.6387	.4145		.1667	1.3209	1.7409
	.1587	-.176		.1507	.7649	.5907		.2081	1.2824	1.6409
	.2068	-.222		.2920	.9477	.9119		.2500	.9960	.9898
	.2545	-.223		.4340	1.0086	1.0363		.2919	.8928	.7952
	.3025	-.222		.5050	1.0334	1.0881		.3338	.9149	.8352
	.3510	-.202		.5750	1.0364	1.0933		.3750	.9376	.8772
	.3985	-.196		.6460	1.0237	1.0674		.4170	.9632	.9257
	.4470	-.183		.7180	1.0237	1.0674		.4580	.9680	.9351
	.4950	-.171		.7890	1.0210	1.0622		.5000	.9692	.9372
	.5430	-.165		.8590	1.0605	1.1399		.5420	.9664	.9319
	.5910	-.140		.9300	1.0605	1.1399		.5830	.9703	.9393
	.6390	-.119		1.0000	1.0541	1.1295		.6250	.9912	.9803
	.6870	-.103	St'bd hull	.0177	.6040	.3679		.6670	.9927	.9835
	.7350	-.082		.0443	.7223	.5285		.7080	.9901	.9783
	.7845	-.051		.0797	.7960	.6425		.7500	.9907	.9793
	.8310	-.088		.1507	.9240	.8653		.7900	.9901	.9783
	.8795	-.010		.2920	1.0364	1.0933		.8333	1.0216	1.0414
	.9275	.077		.4340	1.0364	1.0933		.8700	1.0180	1.0339
St'bd hull	.7600	-.046	St'bd rake	.5050	1.0486	1.1192		.9170	1.0237	1.0455
	.8075	-.093		.5750	1.0486	1.1192		1.0000		
	.8550	-.041		.6460	1.0456	1.1088				
	.9045	.041		.7180	1.0486	1.1140				
	.9520	.150		.7890	1.0486	1.1192				
				.8590	1.0426	1.1036				

TABLE 7
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(a) $n = 67.83$ rps $\frac{U}{nD} = 1.502$ $\alpha = -0.5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0144	.587	Port rake	.0177	.4267	.1832	Wake rake	.0000	.4881	.2377
	.0625	-.002		.0443	.5420	.2936		.0833	.6479	.4189
	.1107	-.132		.0797	.6213	.3863		.1667	.7726	.5956
	.1587	-.152		.1507	.7391	.5475		.2081	.8346	.6948
	.2068	-.180		.2920	.9196	.8477		.2500	.8805	.7736
	.2545	-.190		.4340	.9782	.9603		.2919	.8435	.7098
	.3025	-.192		.5050	1.0164	1.0353		.3338	.8795	.7717
	.3510	-.187		.5750	1.0097	1.0221		.3750	.9146	.8346
	.3985	-.178		.6460	1.0124	1.0287		.4170	.9406	.8829
	.4470	-.167		.7180	1.0110	1.0265		.4580	.9570	.9139
	.4950	-.156		.7890	1.0137	1.0309		.5000	.9635	.9261
	.5430	-.145		.8590	1.0388	1.0817		.5420	.9668	.9325
	.5910	-.108		.9300	1.0375	1.0795		.5830	.9661	.9312
	.6390	-.099		1.0000	1.0322	1.0684		.6250	.9949	.9876
	.6870	-.075						.6670	.9940	.9858
	.7350	-.050						.7080	.9946	.9872
St'bd hull	.7845	-.028	St'bd rake	.0177	.5944	.3532		.7500	.9953	.9885
	.8310	-.046		.0443	.7168	.5143		.7900	.9949	.9876
	.8795	.026		.0797	.7819	.6137		.8333	1.0168	1.0318
	.9275	.143		.1507	.9030	.8168		.9170	1.0164	1.0308
				.2920	1.0164	1.0353		1.0000	1.0173	1.0326
				.4340	1.0232	1.0486				
				.5050	1.0338	1.0728				
				.5750	1.0338	1.0728				
				.6460	1.0296	1.0640				
				.7180	1.0309	1.0662				
				.7890	1.0322	1.0684				
				.8590	1.0375	1.0795				
				.9300	1.0388	1.0817				
				1.0000	1.0388	1.0817				

TABLE 7 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(b) $n = 77.15$ rps $\frac{U}{nD} = 1.326$ $\alpha = -0.5^\circ$

Station	x/l	C_p	Station	y/h	U/U_∞	q_1/q_∞	Station	z/h	U/U_∞	q_1/q_∞
Port hull	.0144	.612	Port rake	.0177	.4305	.1838	Wake rake	.0000	.4927	.2422
	.0625	.026		.0443	.5467	.2976		.0833	.6646	.4408
	.1107	-.116		.0797	.6213	.3851		.1667	.7837	.6129
	.1587	-.144		.1507	.7430	.5492		.2081	.8510	.7226
	.2068	-.183		.2920	.9282	.8556		.2500	.8928	.7954
	.2545	-.188		.4340	.9824	.9606		.2919	.8491	.7194
	.3025	-.192		.5050	1.0232	1.0394		.3338	.8835	.7791
	.3510	-.179		.5750	1.0178	1.0306		.3750	.9173	.8396
	.3985	-.175		.6460	1.0178	1.0306		.4170	.9404	.8824
	.4470	-.177		.7180	1.0164	1.0284		.4580	.9578	.9151
	.4950	-.153		.7890	1.0205	1.0350		.5000	.9630	.9253
	.5430	-.144		.8590	1.0467	1.0897		.5420	.9648	.9288
	.5910	-.107		.9300	1.0467	1.0897		.5830	.9655	.9302
	.6390	-.105		1.0000	1.0414	1.0788		.6250	.9940	.9858
	.6870	-.068						.6670	.9958	.9894
St'bd hull	.7350	-.046	St'bd rake	.0177	.6039	.3632		.7080	.9940	.9858
	.7845	-.032		.0443	.7221	.5186		.7500	.9963	.9903
	.8310	-.046		.0797	.7942	.6280		.7900	.9958	.9894
	.8795	.017		.1507	.9135	.8293		.8333	1.0164	1.0308
	.9275	.144		.2920	1.0309	1.0569		.89170	1.0166	1.0312
				.4340	1.0338	1.0813		1.0000	1.0166	1.0312
				.5050	1.0362	1.0678				
	.7600	-.021		.5750	1.0362	1.0678				
	.8075	-.056		.6460	1.0375	1.0700				
	.8550	-.008		.7180	1.0338	1.0613				
	.9045	.081		.7890	1.0362	1.0678				
	.9520	.227		.8590	1.0404	1.0766				
				.9300	1.0404	1.0766				
				1.0000	1.0404	1.0766				

TABLE 7 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(c) $n = 86.50$ rps $\frac{U}{nD} = 1.179$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.638	Port rake	.0177	.4410	.1943	Wake rake	.0000	.5043	.2537
	.0625	.035		.0443	.5588	.3113		.0833	.7054	.4964
	.1107	-.103		.0797	.6368	.4040		.1667	.8222	.6745
	.1587	-.134		.1507	.7566	.5695		.2081	.8883	.7873
	.2068	-.155		.2920	.9392	.8786		.2500	.9224	.8488
	.2545	-.165		.4340	.9876	.9713		.2919	.8543	.7281
	.3025	-.170		.5050	1.0177	1.0309		.3338	.8847	.7809
	.3510	-.170		.5750	1.0177	1.0309		.3750	.9198	.8442
	.3985	-.167		.6460	1.0177	1.0309		.4170	.9408	.8832
	.4470	-.170		.7180	1.0189	1.0331		.4580	.9570	.9140
	.4950	-.145		.7890	1.0204	1.0353		.5000	.9618	.9231
	.5430	-.136		.8590	1.0455	1.0883		.5420	.9633	.9259
	.5910	-.097		.9300	1.0443	1.0861		.5830	.9638	.9268
	.6390	-.088		1.0000	1.0378	1.0706		.6250	.9947	.9874
St'bd hull	.6870	-.070	St'bd rake	.0177	.6012	.3598		.6670	.9943	.9864
	.7350	-.048		.0443	.7157	.5099		.7080	.9947	.9874
	.7845	-.015		.0797	.7817	.6071		.7500	.9966	.9910
	.8310	-.041		.1507	.8927	.7925		.7900	.9943	.9864
	.8795	.024		.2920	1.0055	1.0066		.8333	1.0156	1.0291
	.9275	.143		.4340	1.0281	1.0530		.9170	1.0156	1.0291
				.5050	1.0335	1.0640		1.0000	1.0151	1.0282
				.5750	1.0349	1.0662				
				.6460	1.0335	1.0640				
				.7180	1.0335	1.0640				

TABLE 7 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(d) $n = 63.33$ rps $\frac{U}{nD} = 1.072$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U/U_∞	q_1/q_∞
Port hull	.0144	.605	Port rake	.0177	.4055	.1650	Wake rake	.0000	.4999	.2493
	.0625	-.005		.0443	.5364	.2900		.0833	.7465	.5560
	.1107	-.130		.0797	.6058	.3700		.1667	.8705	.7559
	.1587	-.165		.1507	.7506	.5650		.2081	.9325	.8678
	.2068	-.220		.2920	.9425	.8950		.2500	.9215	.8473
	.2545	-.215		.4340	1.0022	1.0100		.2919	.8609	.7396
	.3025	-.215		.5050	1.0261	1.0600		.3338	.8937	.7970
	.3510	-.205		.5750	1.0235	1.0550		.3750	.9293	.8616
	.3985	-.190		.6460	1.0235	1.0550		.4170	.9544	.9088
	.4470	-.195		.7180	1.0235	1.0550		.4580	.9662	.9314
	.4950	-.175		.7890	1.0235	1.0550		.5000	.9703	.9396
	.5430	-.155		.8590	1.0498	1.1100		.5420	.9682	.9355
	.5910	-.125		.9300	1.0731	1.1550		.5830	.9694	.9375
	.6390	-.115		1.0000	1.0473	1.1000		.6250	.9923	.9827
	.6870	-.093	St'bd rake	.0177	.5964	.3550		.6670	.9930	.9837
	.7350	-.065		.0443	.7177	.5200		.7080	.9914	.9806
	.7845	-.040		.0797	.7860	.6250		.7500	.9923	.9827
	.8310	-.065		.1507	.9260	.8600		.7900	.9930	.9837
	.8795	.005		.2920	1.0295	1.0650		.8333	1.0129	1.0237
	.9275	.130		.4340	1.0380	1.0850		.9170	1.0114	1.0206
				.5050	1.0443	1.0950		1.0000	1.0149	1.0278
				.5750	1.0527	1.1150				
				.6460	1.0473	1.1050				
				.7180	1.0527	1.1150				
				.7890	1.0527	1.1150				
				.8590	1.0527	1.1150				
				.9300	1.0527	1.1150				
				1.0000	1.0556	1.1200				
St'bd hull	.7600	-.025								
	.8075	-.080								
	.8550	-.025								
	.9045	.065								
	.9520	.215								

TABLE 7 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(e) $n = 95.82$ rps $\frac{U}{nD} = 1.063$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0144	.596	Port rake	.0177	.4324	.1875	Wake	.0000	.5136	.2633
	.0625	.006		.0443	.5470	.3013		.0833	.7412	.5480
	.1107	-.120		.0797	.6263	.3951		.1667	.8624	.7420
	.1587	-.156		.1507	.7443	.5558		.2081	.9232	.8503
	.2068	-.196		.2920	.9250	.8594		.2500	.9220	.8481
	.2545	-.194		.4340	.9855	.9754		.2919	.8532	.7263
	.3025	-.192		.5050	1.0169	1.0402		.3338	.8840	.7796
	.3510	-.180		.5750	1.0142	1.0335		.3750	.9198	.8439
	.3985	-.178		.6460	1.0156	1.0379		.4170	.9402	.8820
	.4470	-.168		.7180	1.0156	1.0379		.4580	.9541	.9083
	.4950	-.151		.7890	1.0156	1.0357		.5000	.9596	.9188
	.5430	-.129		.8590	1.0423	1.0915		.5420	.9592	.9178
	.5910	-.107		.9300	1.0436	1.0938		.5830	.9604	.9202
	.6390	-.098		1.0000	1.0356	1.0781		.6250	.9926	.9831
St'bd hull	.6870	-.072	St'bd rake	.0177	.6066	.3705	St'bd rake	.6670	.9919	.9817
	.7350	-.044		.0443	.7239	.5268		.7080	.9913	.9804
	.7845	-.026		.0797	.7943	.6339		.7500	.9926	.9831
	.8310	-.040		.1507	.9071	.8259		.7900	.9928	.9836
	.8795	.022		.2920	1.0156	1.0379		.8333	1.0145	1.0267
	.9275	.133		.4340	1.0235	1.0536		.89170	1.0142	1.0263
	.7600	-.020		.5050	1.0331	1.0714		1.0000	1.0163	1.0304
	.8075	-.051		.5750	1.0289	1.0647				
	.8550	-.004		.6460	1.0331	1.0737				
	.9045	.075		.7180	1.0302	1.0670				
	.9520	.214		.7890	1.0331	1.0714				
				.8590	1.0356	1.0781				
				.9300	1.0331	1.0714				
				1.0000	1.0356	1.0781				

TABLE 7 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS

OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(f) $n = 105.21$ rps $\frac{U_\infty}{nD} = .967$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.607	Port rake	.0177	.4356	.1885	Wake rake	.0000	.5329	.2834
	.0625	.015		.0443	.5525	.3038		.0833	.7861	.6165
	.1107	-.119		.0797	.6273	.3925		.1667	.9138	.8331
	.1587	-.148		.1507	.7509	.5610		.2081	.9723	.9432
	.2068	-.188		.2920	.9310	.8625		.2500	.9322	.8672
	.2545	-.187		.4340	.9869	.9690		.2919	.8563	.7487
	.3025	-.186		.5050	1.0171	1.0310		.3338	.8957	.8003
	.3510	-.175		.5750	1.0157	1.0266		.3750	.9279	.8589
	.3985	-.172		.6460	1.0171	1.0310		.4170	.9473	.8953
	.4470	-.172		.7180	1.0171	1.0288		.4580	.9589	.9174
	.4950	-.150		.7890	1.0185	1.0333		.5000	.9632	.9257
	.5430	-.141		.8590	1.0452	1.0887		.5420	.9632	.9257
	.5910	-.104		.9300	1.0437	1.0843		.5830	.9632	.9257
	.6390	-.095		1.0000	1.0401	1.0754		.6250	.9930	.9837
	.6870	-.073						.6670	.9941	.9861
	.7350	-.051						.7080	.9934	.9847
St'bd hull	.7845	-.031	St'bd rake	.0177	.6075	.3659		.7500	.9937	.9851
	.8310	-.048		.0443	.7249	.5233		.7900	.9946	.9870
	.8795	.017		.0797	.7902	.6208		.8333	1.0183	1.0345
	.9275	.133		.1507	.9072	.8182		.9170	1.0178	1.0335
				.2920	1.0225	1.0399		1.0000	1.0189	1.0359
				.4340	1.0279	1.0510				
				.5050	1.0304	1.0576				
				.5750	1.0304	1.0576				
				.6460	1.0304	1.0576				
				.7180	1.0318	1.0599				
				.7890	1.0304	1.0576				
				.8590	1.0401	1.0754				
				.9300	1.0401	1.0754				
				1.0000	1.0401	1.0776				

TABLE 7 Continued

CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(g) $n = 73.33$ rps $\frac{U}{nD} = .923$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.600	Port rake	.0177	.4156	.1750	Wake rake	.0000	.5419	.2930
	.0625	-.005		.0443	.5380	.2900		.0833	.8064	.6489
	.1107	-.130		.0797	.6177	.3800		.1667	.9507	.9017
	.1587	-.160		.1507	.7529	.5650		.2081	1.0021	1.0018
	.2068	-.180		.2920	.9386	.8800		.2500	.9408	.8831
	.2545	-.182		.4340	1.0082	1.0150		.2919	.8812	.7748
	.3025	-.200		.5050	1.0385	1.0800		.3338	.9090	.8243
	.3510	-.180		.5750	1.0325	1.0650		.3750	.9424	.8862
	.3985	-.180		.6460	1.0325	1.0650		.4170	.9632	.9254
	.4470	-.172		.7180	1.0265	1.0550		.4580	.9717	.9419
	.4950	-.165		.7890	1.0325	1.0650		.5000	.9737	.9460
	.5430	-.140		.8590	1.0587	1.1200		.5420	.9737	.9502
	.5910	-.120		.9300	1.0622	1.1300		.5830	.9759	.9915
	.6390	-.105		1.0000	1.0474	1.0950		.6250	.9968	.9945
	.6870	-.079	St'bd rake	.0177	.6075	.3700		.6670	.9983	.9915
St'bd hull	.7350	-.060		.0443	.7276	.5300		.7080	.9958	.9893
	.7845	-.040		.0797	.8078	.6500		.7500	.9979	.9935
	.8310	-.050		.1507	.9420	.8850		.7900	1.0220	1.0420
	.8795	.010		.2920	1.0385	1.0800		.8333	1.0194	1.0368
	.9275	.135		.4340	1.0385	1.0800		1.0000	1.0235	1.0451
St'bd hull	.7600	-.030	St'bd rake	.5050	1.0505	1.1000				
	.8075	-.070		.5750	1.0505	1.1050				
	.8550	-.030		.6460	1.0505	1.1000				
	.9045	.060		.7180	1.0528	1.1100				
	.9520	.210		.7890	1.0505	1.1000				

TABLE 7 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30$

(h) $n = 114.47$ rps $\frac{U}{ND} = .885$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.604	Port rake	.0177	.4437	.1964	Wake rake	.0000	.5631	.3164
	.0625	.000		.0443	.5548	.3058		.0833	.8321	.6908
	.1107	-.127		.0797	.6276	.3906		.1667	.9744	.9473
	.1587	-.154		.1507	.7524	.5625		.2081	1.0160	1.0300
	.2068	-.194		.2920	.9421	.8817		.2500	.9348	.8719
	.2545	-.196		.4340	.9949	.9844		.2919	.8666	.7494
	.3025	-.198		.5050	1.0280	1.0513		.3338	.8915	.7930
	.3510	-.185		.5750	1.0185	1.0313		.3750	.9259	.8553
	.3985	-.180		.6460	1.0212	1.0379		.4170	.9421	.8855
	.4470	-.169		.7180	1.0185	1.0313		.4580	.9548	.9097
	.4950	-.154		.7890	1.0212	1.0357		.5000	.9587	.9171
	.5430	-.145		.8590	1.0494	1.0960		.5420	.9589	.9175
	.5910	-.109		.9300	1.0480	1.0915		.5830	.9614	.9221
	.6390	-.100		1.0000	1.0442	1.0826		.6250	.9918	.9816
St'bd hull	.6870	-.080	St'bd rake	.0177	.6099	.3705		.6670	.9927	.9835
	.7350	-.055		.0443	.7295	.5290		.7080	.9916	.9812
	.7845	-.029		.0797	.7972	.6317		.7500	.9925	.9830
	.8310	-.051		.1507	.9213	.8438		.7900	.9925	.9830
	.8795	.008		.2920	1.0322	1.0580		.8333	1.0171	1.0322
	.9275	.122		.4340	1.0334	1.0603		.9170	1.0169	1.0318
				.5050	1.0413	1.0781		1.0000	1.0171	1.0322
				.5750	1.0413	1.0781				
				.6460	1.0400	1.0759				
				.7180	1.0388	1.0737				
				.7890	1.0400	1.0759				
				.8590	1.0442	1.0826				
				.9300	1.0467	1.0893				
				1.0000	1.0467	1.0893				

8191-T

TABLE 7 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(1) $n = 123.90$ rps $\frac{U}{nD} = .816$ $\alpha = -5.5^\circ$

Sta- tion	x/l	C_p
Port hull	.0144	.618
	.0625	.011
	.1107	-.118
	.1567	-.150
	.2068	-.196
	.2545	-.196
	.3025	-.196
	.3510	-.180
	.3985	-.175
	.4470	-.165
	.4950	-.153
	.5430	-.146
	.5910	-.111
	.6390	-.100
St'bd hull	.6870	-.089
	.7350	-.054
	.7845	-.029
	.8310	-.050
	.8795	.011
	.9275	.121
	.7600	-.029
	.8075	-.068
	.8550	-.016
	.9045	.068
	.9520	.198

Sta- tion	y/h	u_1/u_∞	q_1/q_∞
Port rake	.0177	.4450	.2009
	.0443	.5587	.3151
	.0797	.6399	.4132
	.1507	.7544	.5753
	.2920	.9432	.8995
	.4340	.9892	.9909
	.5050	1.0212	1.0548
	.5750	1.0144	1.0411
	.6460	1.0212	1.0548
	.7180	1.0184	1.0479
	.7890	1.0200	1.0525
	.8590	1.0403	1.0936
	.9300	1.0416	1.0959
	1.0000	1.0373	1.0890
St'bd rake	.0177	.6000	.3630
	.0443	.7221	.5274
	.0797	.7937	.6370
	.1507	.9099	.8379
	.2920	1.0212	1.0548
	.4340	1.0280	1.0685
	.5050	1.0361	1.0845
	.5750	1.0349	1.0822
	.6460	1.0334	1.0799
	.7180	1.0334	1.0799
	.7890	1.0334	1.0799
	.8590	1.0373	1.0890
	.9300	1.0403	1.0936
	1.0000	1.0403	1.0936

Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Wake rake	.0000	.5897	.3470
	.0833	.8796	.7720
	.1667	1.0443	1.0881
	.2081	1.0601	1.1212
	.2500	.9506	.9017
	.2919	.8753	.7644
	.3338	.8949	.7990
	.3750	.9283	.8597
	.4170	.9434	.8882
	.4580	.9545	.9092
	.5000	.9595	.9186
	.5420	.9583	.9162
	.5830	.9595	.9186
	.6250	.9909	.9798
	.6670	.9919	.9816
	.7080	.9912	.9802
	.7500	.9914	.9807
	.7900	.9921	.9821
	.8333	1.0147	1.0274
	.9170	1.0152	1.0283
	1.0000	1.0159	1.0297

TABLE 7 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

$n = 83.32 \text{ rps}$ $\frac{U}{nD} = .813$ $a = -.5$							
Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port rake	.0177	.4577	.2111	Wake rake	.0000	.5129	.3274
	.0443	.5601	.3166		.0833	.8584	.7352
	.0797	.6417	.4121		.1667	1.0275	1.0534
	.1507	.7804	.6131		.2081	1.0592	1.1193
	.2920	.9540	.9146		.2500	.9545	.9092
	.4340	1.0042	1.0151		.2919	.8845	.7806
	.5050	1.0376	1.0804		.3338	.9052	.8175
	.5750	1.0254	1.0603		.3750	.9382	.8783
	.6460	1.0346	1.0754		.4170	.9584	.9164
	.7180	1.0224	1.0553		.4580	.9675	.9340
	.7890	1.0254	1.0603		.5000	.9680	.9349
	.8590	1.0494	1.1106		.5420	.9680	.9349
	.9300	1.0577	1.1256		.5830	.9701	.9391
	1.0000	1.0494	1.1055		.6250	.9843	.9864
St'bd rake	.0177	.5976	.3568	.6670	.9933	.9844	
	.0443	.7191	.5176	.7080	.9922	.9823	
	.0797	.7875	.6281	.7500	.9933	.9844	
	.1507	.9080	.8291	.7900	.9933	.9844	
	.2920	1.0429	1.0955	.8333	1.0164	1.0307	
	.4340	1.0429	1.0955	.9170	1.0154	1.0287	
	.5050	1.0494	1.1106	1.0000	1.0179	1.0338	
	.5750	1.0464	1.1005				
	.6460	1.0400	1.0905				
	.7180	1.0400	1.0905				
	.7890	1.0464	1.1005				
	.8590	1.0376	1.0854				
	.9300	1.0429	1.0955				
	1.0000	1.0464	1.1005				

TABLE 7 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30$
 (K) $n = 133.33$ rps $\frac{U}{ND} = .758$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/u_∞	q_1/q_∞	Sta- tion	z/h	u_1/u_∞	q_1/q_∞
Port hull	.0144	-.599	Port rake	.0177	.4514	.2027	Wake rake	.0000	.6152	.3776
	.0625	.011		.0443	.5619	.3153		.0833	.9203	.8451
	.1107	-.121		.0797	.6402	.4077		.1667	1.1042	1.2166
	.1587	-.150		.1507	.7563	.5698		.2081	1.0933	1.1928
	.2068	-.180		.2920	.9404	.8806		.2500	.9618	.9231
	.2545	-.170		.4340	.9927	.9820		.2919	.8773	.7679
	.3025	-.182		.5050	1.0243	1.0473		.3338	.8974	.8035
	.3510	-.180		.5750	1.0174	1.0315		.3750	.9307	.8642
	.3985	-.175		.6460	1.0243	1.0450		.4170	.9414	.8843
	.4470	-.180		.7180	1.0243	1.0450		.4580	.9501	.9006
	.4950	-.150		.7890	1.0258	1.0495		.5000	.9550	.9100
	.5430	-.144		.8590	1.0488	1.0968		.5420	.9540	.9082
	.5910	-.103		.9300	1.0474	1.0946		.5830	.9553	.9105
	.6390	-.101		1.0000	1.0420	1.0811		.6250	.9890	.9759
	.6870	-.080						.6670	.9883	.9745
	.7350	-.047						.7080	.9885	.9750
St'd hull	.7845	-.020	St'd rake	.0177	.6118	.3716		.7500	.9885	.9750
	.8310	-.049		.0443	.7282	.5293		.7900	.9873	.9727
	.8795	.006		.0797	.8011	.6396		.8333	1.0118	1.0217
	.9275	.121		.1507	.9149	.8333		.9170	1.0133	1.0245
				.2920	1.0258	1.0495		1.0000	1.0136	1.0250
				.4340	1.0271	1.0518				
St'd hull	.7600	-.024	St'd rake	.5050	1.0353	1.0676	St'd rake			
	.8075	-.063		.5750	1.0353	1.0676				
	.8550	-.013		.6460	1.0340	1.0653				
	.9045	.065		.7180	1.0340	1.0653				
	.9520	.184		.7890	1.0311	1.0608				
				.8590	1.0391	1.0766				
				.9300	1.0431	1.0856				
				1.0000	1.0420	1.0811				

TABLE 7 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(1) $n = 93.41$ rps $\frac{U}{nD} = .725$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U_1/U_∞	q_1/q_∞	Sta- tion	z/h	U_1/U_∞	q_1/q_∞
Port hull	.0144	.608	Port rake	.0177	.4428	.1960	Wake rake	.0000	.6400	.4088
	.0625	-.015		.0443	.5546	.3116		.0833	.9476	.8958
	.1107	-.145		.0797	.6417	.4171		.1667	1.1614	1.3458
	.1587	-.170		.1507	.7716	.5930		.2081	1.1412	1.2995
	.2068	-.191		.2920	.9411	.8894		.2500	.9891	.9761
	.2545	-.198		.4340	.9979	1.0050		.2919	.9002	.8083
	.3025	-.206		.5050	1.0316	1.0704		.3338	.9138	.8330
	.3510	-.185		.5750	1.0280	1.0653		.3750	.9459	.8928
	.3985	-.185		.6460	1.0280	1.0653		.4170	.9675	.9340
	.4470	-.175		.7180	1.0280	1.0653		.4580	.9744	.9473
	.4950	-.165		.7890	1.0280	1.0653		.5000	.9728	.9443
	.5430	-.140		.8590	1.0577	1.1256		.5420	.9723	.9432
	.5910	-.125		.9300	1.0548	1.1206		.5830	.9749	.9484
	.6390	-.110		1.0000	1.0494	1.1055		.6250	.9943	.9864
	.6870	-.090						.6670	.9948	.9875
St'bd hull	.7350	-.055	St'bd rake	.0177	.6171	.3819		.7080	.9922	.9823
	.7845	-.025		.0443	.7396	.5528		.7500	.9979	.9936
	.8310	-.065		.0797	.8069	.6583		.7900	.9948	.9875
	.8795	.005		.1507	.9377	.8844		.8333	1.0168	1.0318
	.9275	.115		.2920	1.0376	1.0804		.9170	1.0168	1.0318
				.4340	1.0400	1.0905		1.0000	1.0224	1.0431
	.7600	-.040		.5050	1.0429	1.0955				
	.8075	-.085		.5750	1.0429	1.0955				
	.8550	-.025		.6460	1.0429	1.0955				
	.9045	.065		.7180	1.0429	1.0955				
	.9520	.185		.7890	1.0429	1.0955				
				.8590	1.0429	1.0955				
				.9300	1.0464	1.1005				
				1.0000	1.0494	1.1055				

OTOT-7

TABLE 7 Continued
 CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(M) $n = 103.33$ rps $\frac{U}{ND} = .653$ $\alpha = -0.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0144	.611	Port rake	.0177	.4315	.1869	Wake rake	.0000	.7226	.5209
	.0625	.005		.0443	.5568	.3131		.0833	.9551	.9100
	.1107	-.116		.0797	.6254	.3939		.1667	1.2119	1.4651
	.1587	-.151		.1507	.7632	.5859		.2081	1.2398	1.5336
	.2068	-.165		.2920	.9414	.8889		.2500	1.1298	1.2732
	.2545	-.176		.4340	.9924	.9899		.2919	.9930	.9837
	.3025	-.176		.5050	1.0234	1.0505		.3338	.9497	.8997
	.3510	-.176		.5750	1.0204	1.0455		.3750	.9718	.9421
	.3985	-.181		.6460	1.0234	1.0505		.4170	.9544	.9090
	.4470	-.181		.7180	1.0168	1.0404		.4580	.9610	.9214
	.4950	-.156		.7890	1.0168	1.0404		.5000	.9626	.9245
	.5430	-.136		.8590	1.0416	1.0909		.5420	.9648	.9287
	.5910	-.106		.9300	1.0355	1.0758		.5830	.9675	.9339
	.6390	-.101		1.0000	1.0355	1.0758		.6250	.9924	.9827
	.6870	-.075	St'bd rake	.0177	.5938	.3535		.6670	.9924	.9827
	.7350	-.045		.0443	.7219	.5202		.7080	.9893	.9764
	.7845	-.015		.0797	.7793	.6111		.7500	.9924	.9827
	.8310	-.060		.1507	.8972	.8081		.7900	.9898	.9775
	.8795	.005		.2920	1.0204	1.0455		.8333	1.0178	1.0335
	.9275	.116		.4340	1.0295	1.0657		.9170	1.0188	1.0355
	.7600	-.015		.5050	1.0385	1.0808		1.0000	1.0193	1.0366
	.8075	-.065		.5750	1.0295	1.0657				
	.8550	-.015		.6460	1.0321	1.0707				
	.9045	.050		.7180	1.0295	1.0657				
St'bd hull	.9520	.166		.7890	1.0355	1.0758				
				.8590	1.0321	1.0707				
				.9300	1.0355	1.0758				
				1.0000	1.0416	1.0859				

TABLE 7 Continued
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(n) $n = 113.29$ rps $\frac{U}{nD} = .597$ $\alpha = -5^\circ$

Sta- tion	x/l	C_p	Sta- tion	y/h	U/U_∞	q_1/q_∞
Port hull	.0144	.616	Port wake	.0177	.4368	.1919
	.0625	.010		.0443	.5615	.3182
	.1107	-.141		.0797	.6489	.4242
	.1587	-.171		.1507	.7782	.6111
	.2068	-.180		.2920	.9627	.9343
	.2545	-.200		.4340	1.0040	1.0152
	.3025	-.207		.5050	1.0370	1.0808
	.3510	-.181		.5750	1.0370	1.0808
	.3985	-.181		.6460	1.0305	1.0707
	.4470	-.186		.7180	1.0340	1.0758
	.4950	-.166		.7890	1.0305	1.0707
	.5430	-.156		.8590	1.0489	1.1061
	.5910	-.130		.9300	1.0519	1.1111
	.6390	-.111		1.0000	1.0425	1.0960
	.6870	-.088	St'bd wake	.0177	.6041	.3687
	.7350	-.060		.0443	.7378	.5505
	.7845	-.035		.0797	.8089	.6566
	.8310	-.060		.1507	.9399	.8889
	.8795	.000		.2920	1.0400	1.0909
	.9275	.101		.4340	1.0400	1.0859
				.5050	1.0454	1.1010
				.5750	1.0489	1.1061
				.6460	1.0400	1.0909
				.7180	1.0454	1.1010
				.7890	1.0454	1.1010
				.8590	1.0454	1.1010
				.9300	1.0519	1.1111
				1.0000	1.0519	1.1111
St'bd hull	.7600	-.040	Wake	.0000	.7828	.6115
	.8075	-.090		.0833	1.0848	1.1743
	.8550	-.030		.1667	1.3506	1.8200
	.9045	.040		.2081	1.2638	1.5934
	.9520	.156		.2500	1.0680	1.1381
				.2919	.9559	.9115
				.3338	.9388	.8795
				.3750	.9627	.9249
				.4170	.9548	.9095
				.4580	.9607	.9208
				.5000	.9622	.9240
				.5420	.9607	.9208
				.5830	.9622	.9240
				.6250	.9909	.9799
				.6670	.9909	.9799
				.7080	.9893	.9767
				.7500	.9893	.9767
				.7900	.9915	.9808
				.8333	1.0209	1.0398
				.9170	1.0203	1.0388
				1.0000	1.0203	1.0388

8161-1

TABLE 7 Continued
 CHROMISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
 OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30$

(o) $n = 123.33$ rps $\frac{U}{ND} = .546$ $\alpha = -.5$

Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0144	.611	Port rake	.0177	.4541	.2124	Wake rake	.0000	.8402	.7041
	.0625	-.015		.0443	.5238	.2798		.0833	1.1836	1.3978
	.1107	-.145		.0797	.6464	.4301		.1667	1.4554	2.1135
	.1587	-.171		.1507	.7773	.6166		.2081	1.3025	1.6924
	.2068	-.217		.2920	.9479	.9223		.2500	1.0401	1.0792
	.2545	-.215		.4340	1.0114	1.0466		.2919	.9357	.8733
	.3025	-.212		.5050	1.0269	1.0777		.3338	.9322	.8671
	.3510	-.196		.5750	1.0238	1.0725		.3750	.9577	.9151
	.3985	-.196		.6460	1.0269	1.0777		.4170	.9538	.9078
	.4470	-.196		.7180	1.0203	1.0674		.4580	.9583	.9162
	.4950	-.171		.7890	1.0203	1.0674		.5000	.9605	.9204
	.5430	-.150		.8590	1.0451	1.1192		.5420	.9594	.9183
	.5910	-.124		.9300	1.0451	1.1192		.5830	.9633	.9256
	.6390	-.114		1.0000	1.0451	1.1192		.6250	.9889	.9758
	.6870	-.089						.6670	.9926	.9831
	.7350	-.062	St'd rake	.0177	.5958	.3627		.7080	.9885	.9747
St'd hull	.7845	-.046		.0443	.7243	.5389		.7500	.9905	.9789
	.8310	-.062		.0797	.7972	.6528		.7900	.9905	.9789
	.8795	-.010		.1507	.9311	.8860		.8333	1.0160	1.0301
	.9275	.082		.2920	1.0420	1.1088		.9170	1.0182	1.0343
				.4340	1.0355	1.0984		1.0000	1.0160	1.0301
				.5050	1.0420	1.1088				
				.5750	1.0451	1.1140				
				.6460	1.0420	1.1088				
				.7180	1.0451	1.1140				
				.7890	1.0451	1.1140				
				.8590	1.0451	1.1140				
				.9300	1.0451	1.1140				
				1.0000	1.0475	1.1244				

TABLE 7 Concluded
CHORDWISE PRESSURE-DISTRIBUTION, BOUNDARY-LAYER, AND WAKE CHARACTERISTICS
OF THE MODEL WITH PROPELLER 2 INSTALLED WITH $\beta = 30^\circ$

(p)		n = 133.33		rps		$\frac{U}{ND}$ = .503		$\alpha = -0.5^\circ$		
Sta- tion	x/l	C_p	Sta- tion	y/h	u_1/U_∞	q_1/q_∞	Sta- tion	z/h	u_1/U_∞	q_1/q_∞
Port hull	.0144	.596	Port rake	.0177	.4555	.2092	Wake rake			
	.0625	-.010		.0443	.5769	.3316				
	.1107	-.127		.0797	.6579	.4337				
	.1587	-.163		.1507	.7843	.6173				
	.2068	-.204		.2920	.9638	.9286				
	.2545	-.205		.4340	1.0206	1.0408				
	.3025	-.204		.5050	1.0420	1.0867				
	.3510	-.188		.5750	1.0385	1.0816				
	.3985	-.183		.6460	1.0385	1.0816				
	.4470	-.188		.7180	1.0329	1.0714				
	.4950	-.163		.7890	1.0299	1.0612				
	.5430	-.148		.8590	1.0571	1.1173				
	.5910	-.117		.9300	1.0601	1.1224				
.6390	-.112	1.0000	1.0420	1.0867						
.6870	-.084									
.7350	-.051									
.7845	-.051									
.8310	-.071									
.8795	-.010									
.9275	.086									
St'bd hull	.7600	-.040	St'bd rake	.0177	.5923	.3520				
	.8075	-.081		.0443	.7344	.5408				
	.8550	-.040		.0797	.8081	.6531				
	.9045	.040		.1507	.9237	.8520				
	.9520	.117		.2920	1.0359	1.0765				
			.4340	1.0452	1.0918					
				.5050	1.0536	1.1122				
				.5750	1.0507	1.1071				
				.6460	1.0507	1.1071				
				.7180	1.0507	1.1071				
				.7890	1.0507	1.1071				
				.8590	1.0482	1.1020				
				.9300	1.0482	1.1020				
				1.0000	1.0482	1.1020				

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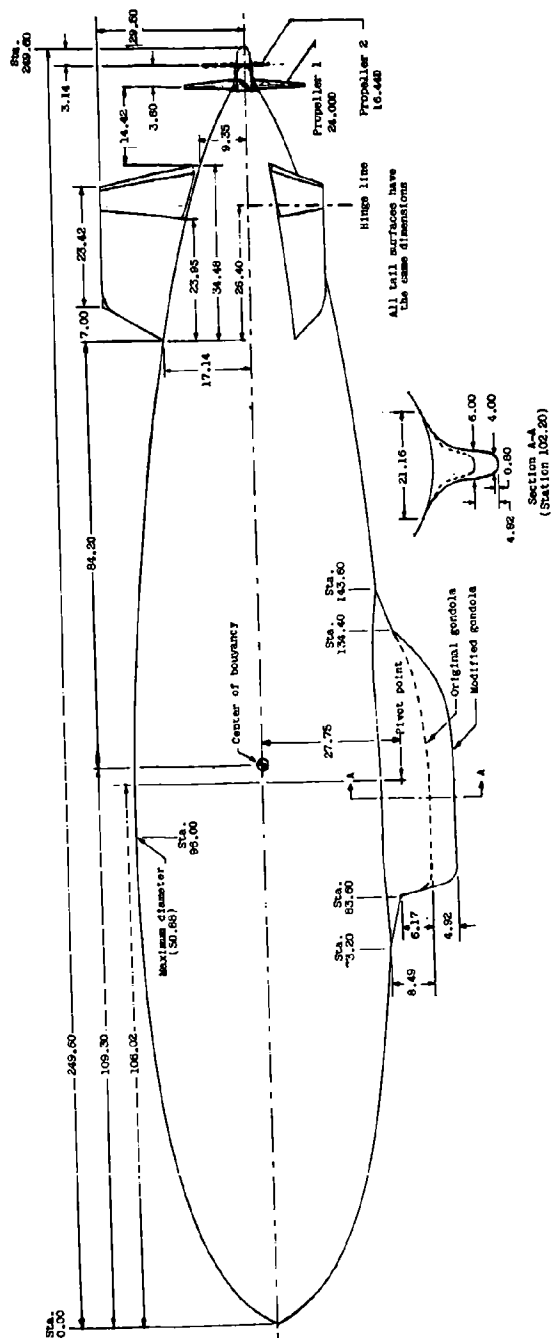


Figure 1.- General dimensions of the hull, gondola, and tail surfaces. All dimensions are in inches.



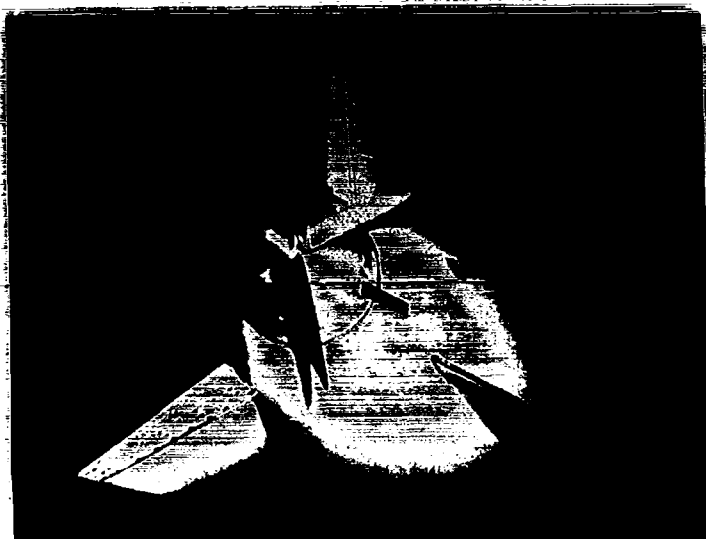
(a) Three-quarter rear view of the airship model mounted for tests in the Langley full-scale tunnel. Propeller 1 configuration.

L-60-418

Figure 2.- Photographs of the model.

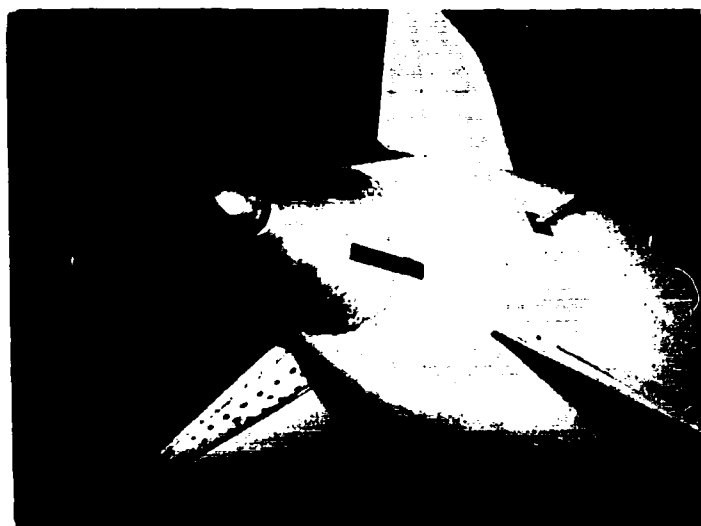
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L-1618



(b) Propeller 1 installation.

L-60-419



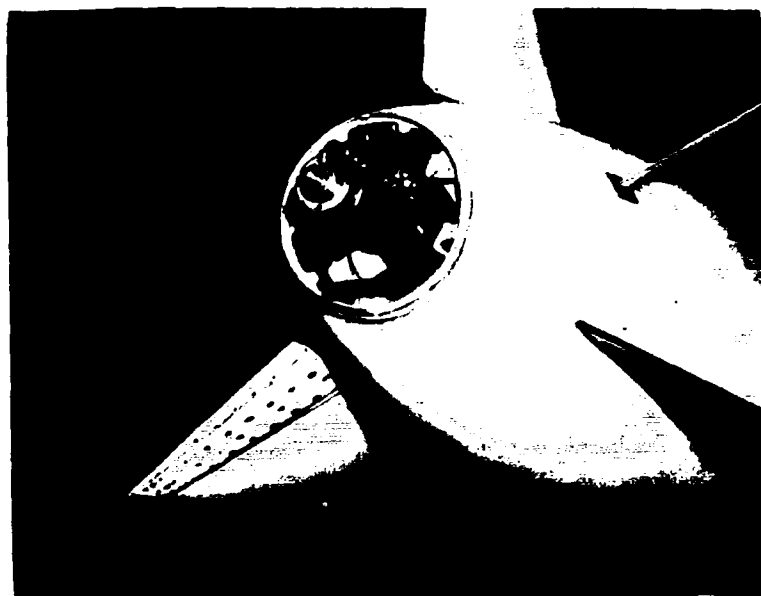
(c) Propeller 2 installation.

L-60-422

Figure 2.- Continued.



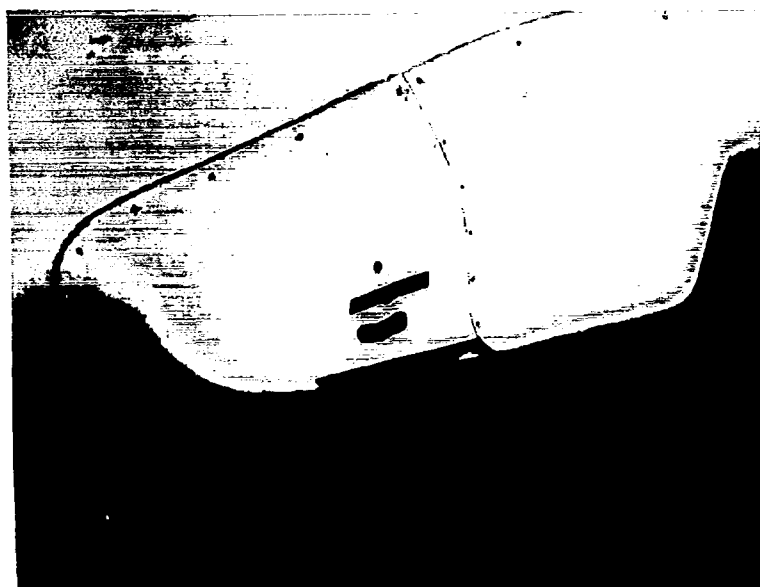
(d) Tandem-motor arrangement and strain-gage balance for propeller 1. L-60-423



(e) Single model motor and support. L-60-421

Figure 2.- Continued.

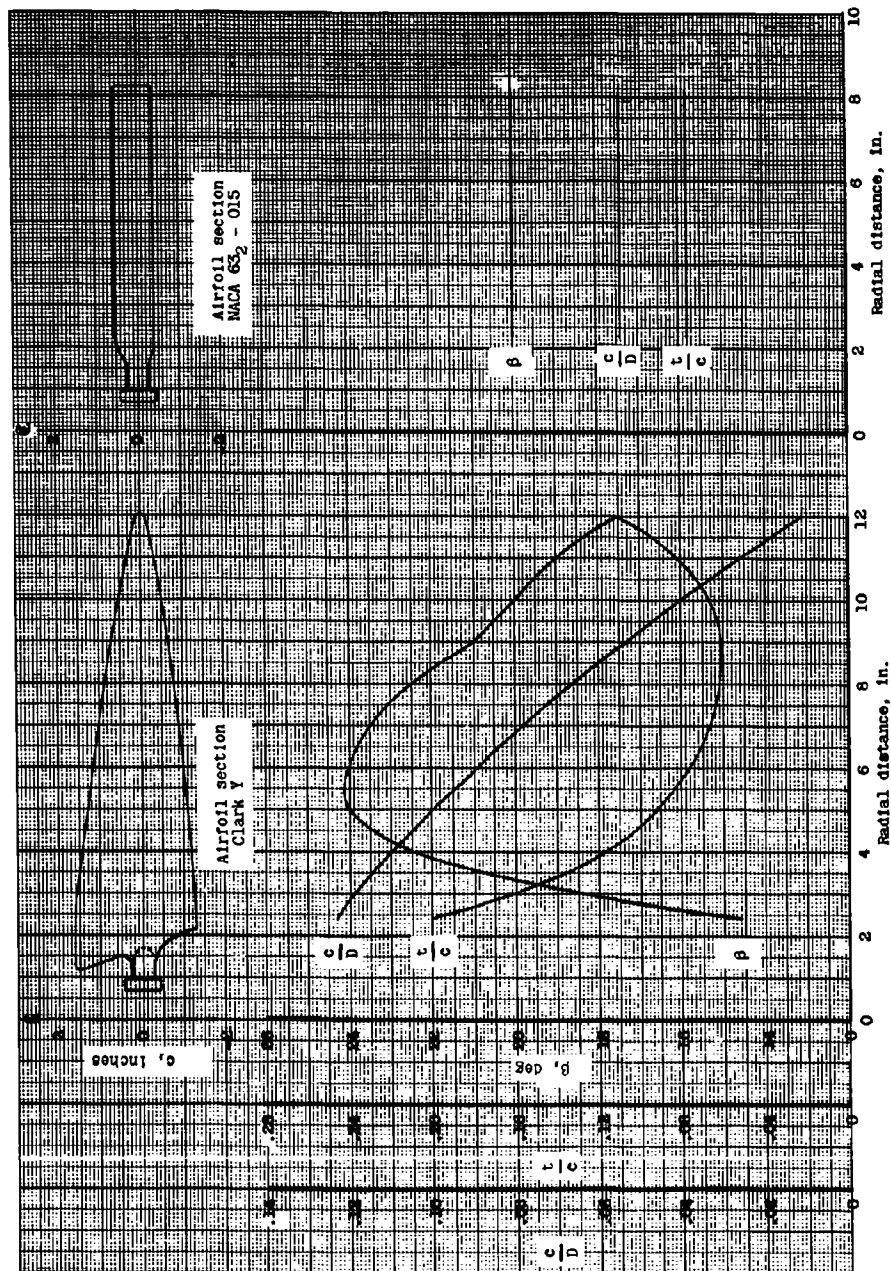
L-1618



(f) Gondola—support-strut relationship.

L-60-420

Figure 2.- Concluded.

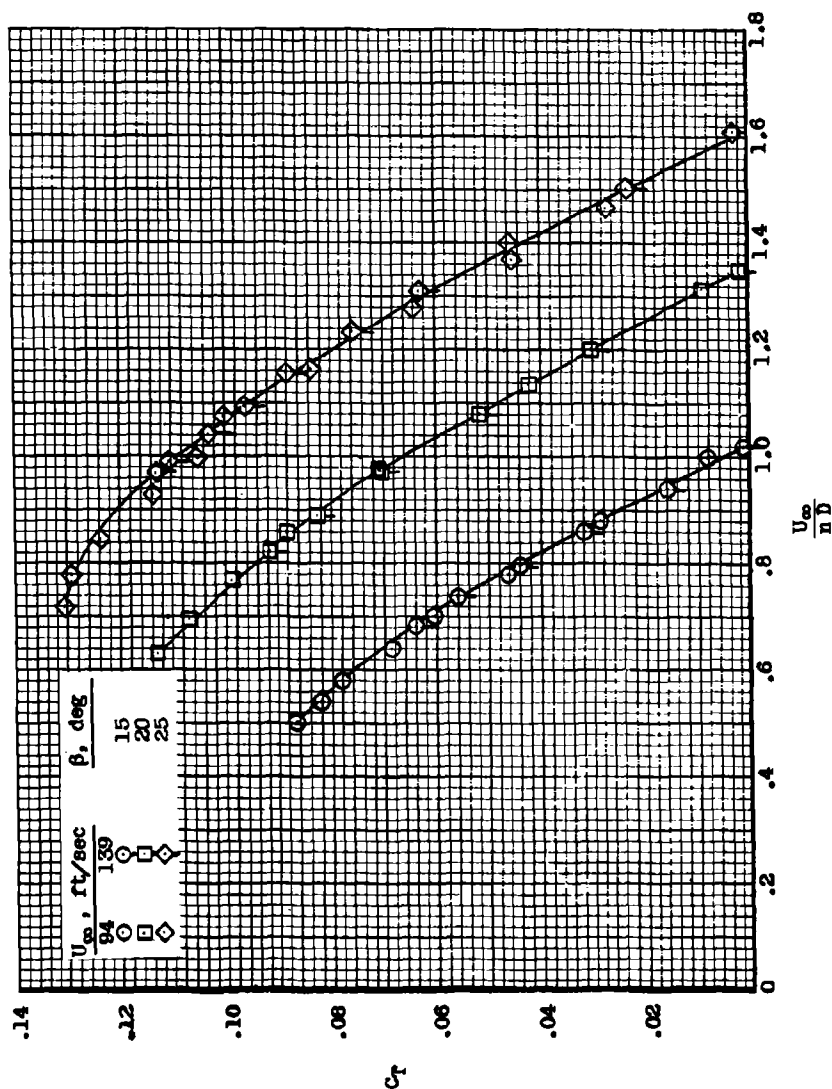


(a) Propeller 1.

(b) Propeller 2.

Figure 3.- Propeller blade-form curves.

L-1618



(a) C_T against U_∞/nD .

Figure 4.- Variation of the propeller characteristics and model drag with propeller 1 operating.
 $\alpha = -0.5^\circ$.

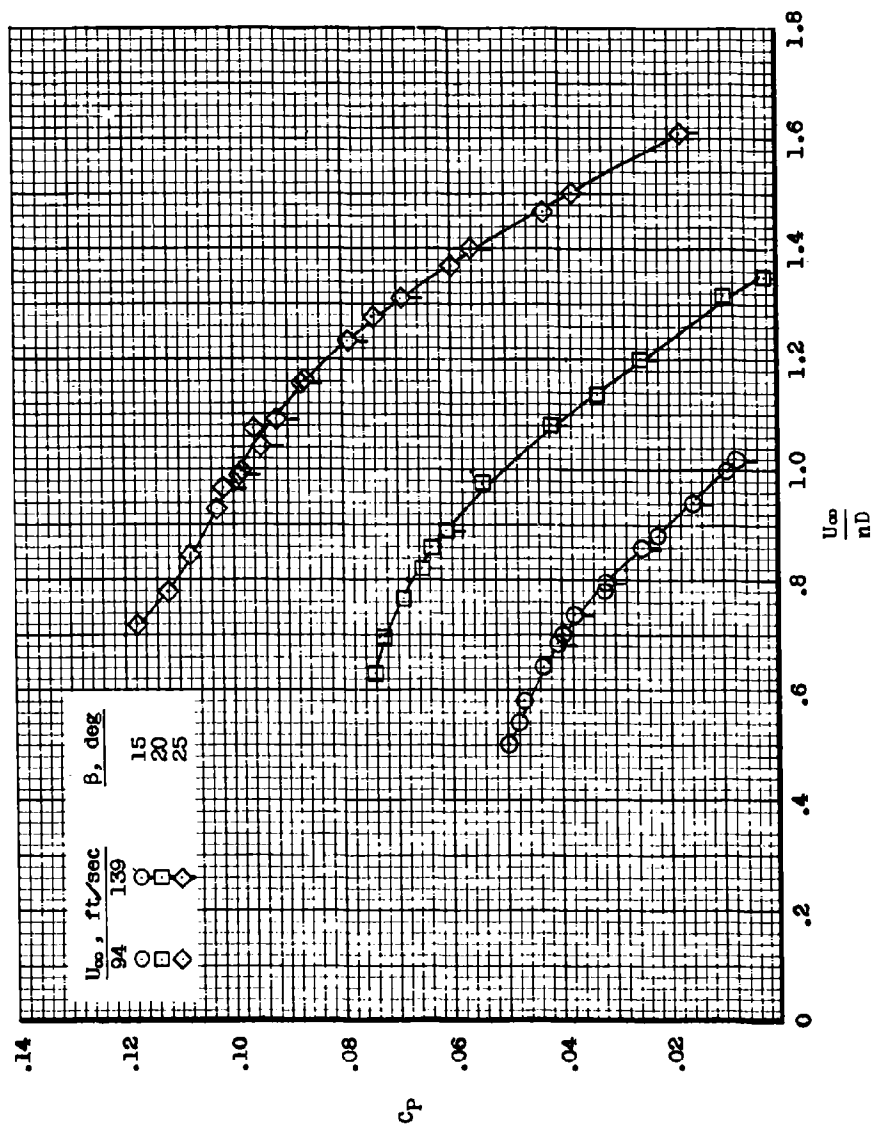
(b) C_p against U_∞ / nD .

Figure 4.- Continued.

L-1618

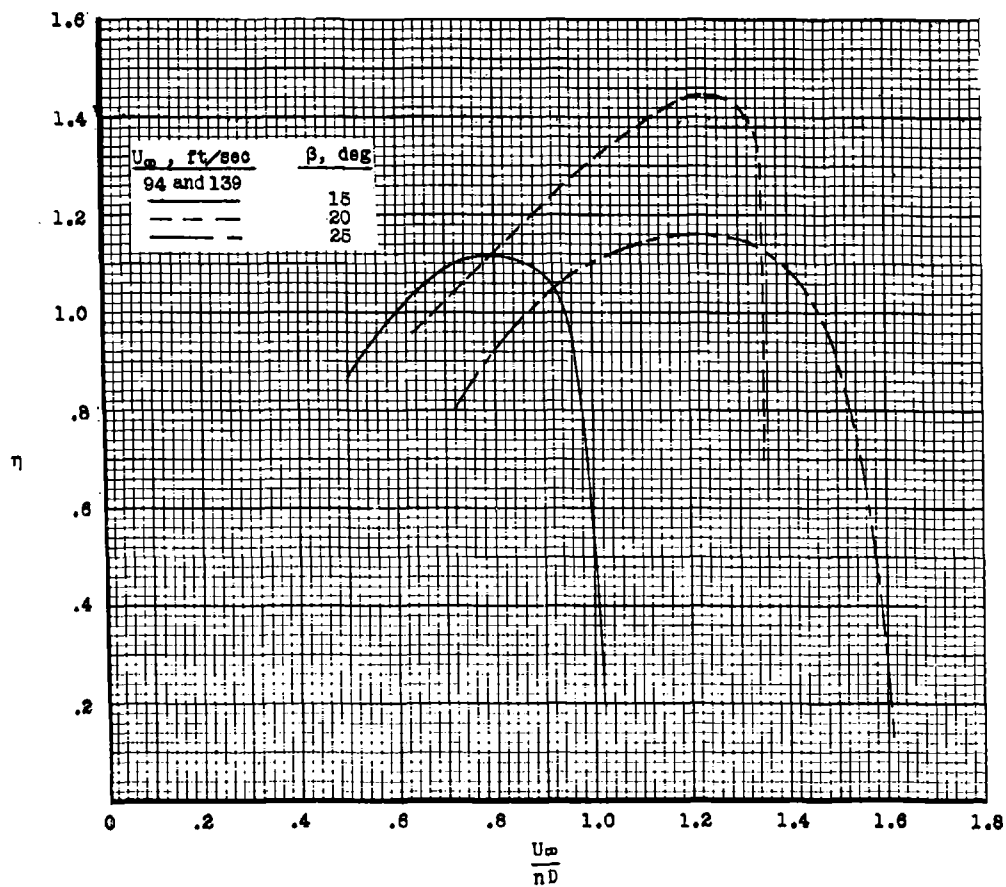
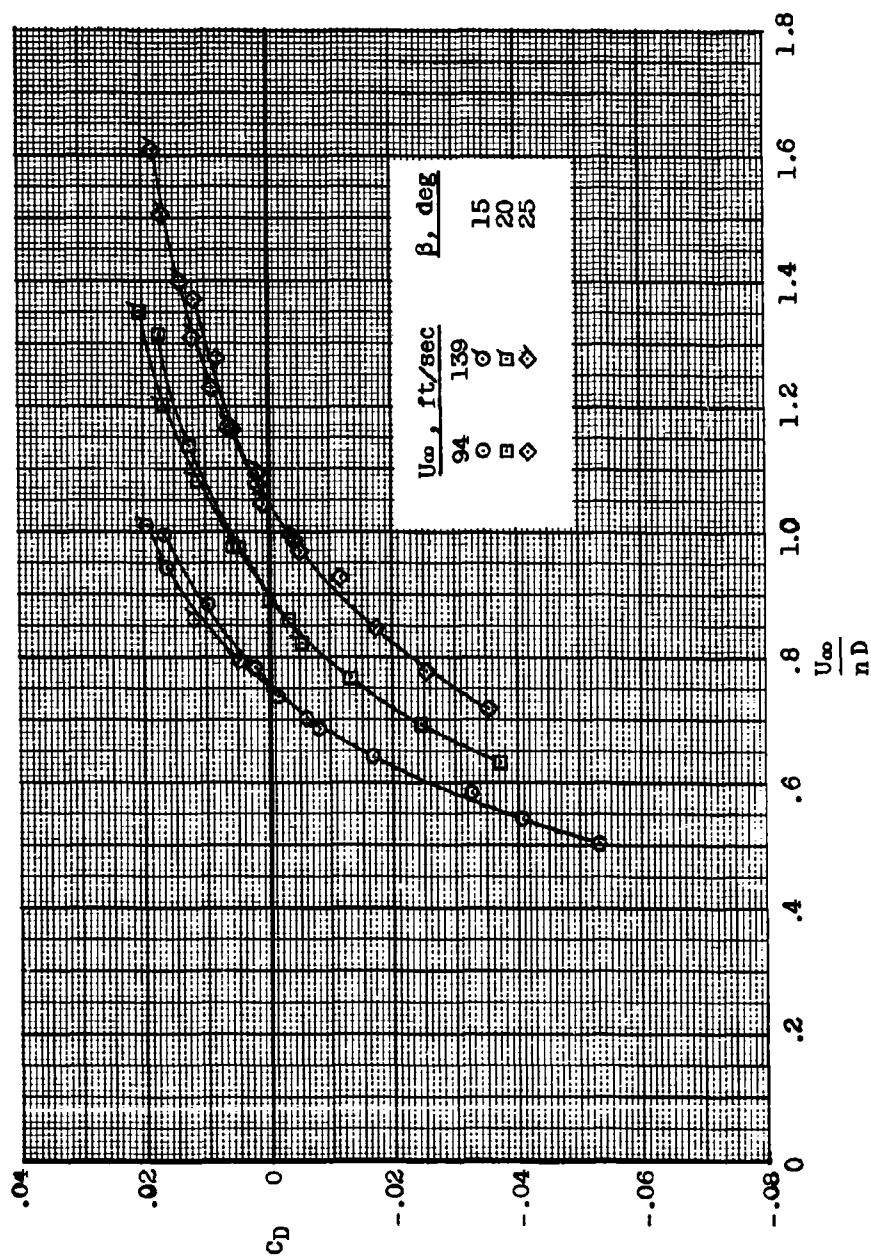
(c) η against U_∞/nD .

Figure 4.- Continued.

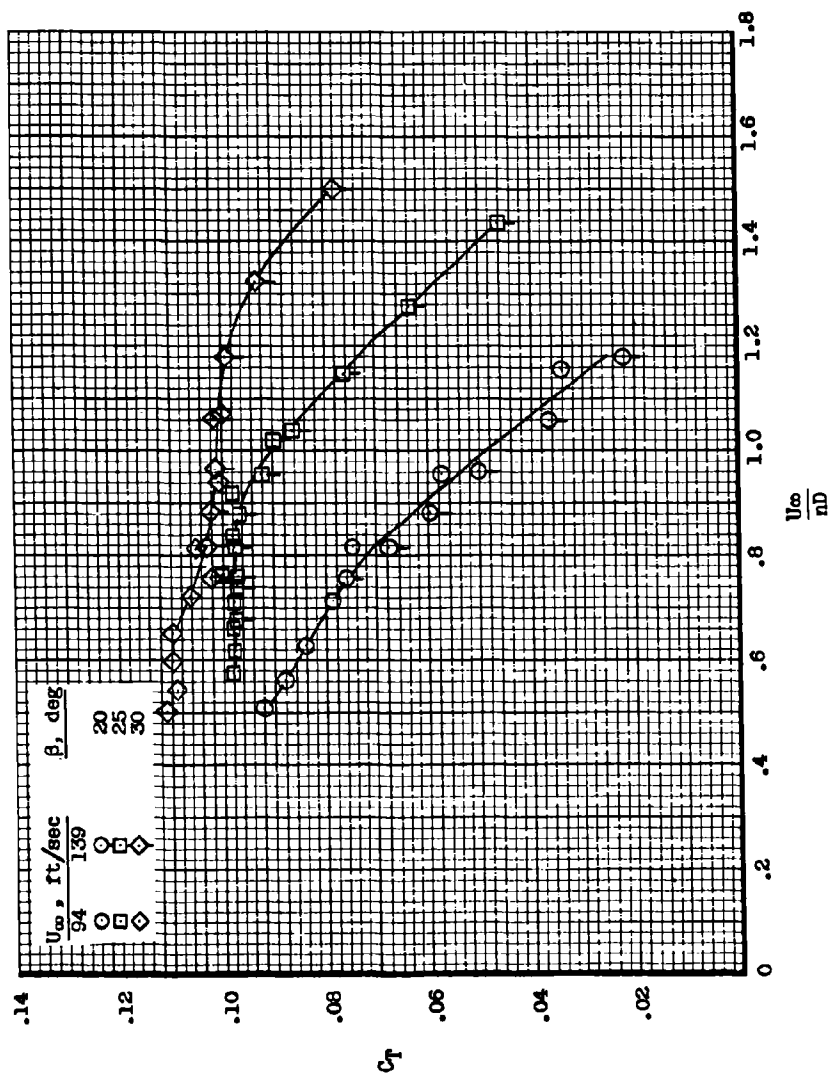


(d) C_D against U_∞/nD .

Figure 4.- Concluded.

8191-7

L-1618



(a) C_T against U_∞/nD .

Figure 5.- Variation of the propeller characteristics and model drag with propeller 2 operating.
 $\alpha = -0.5^\circ$.

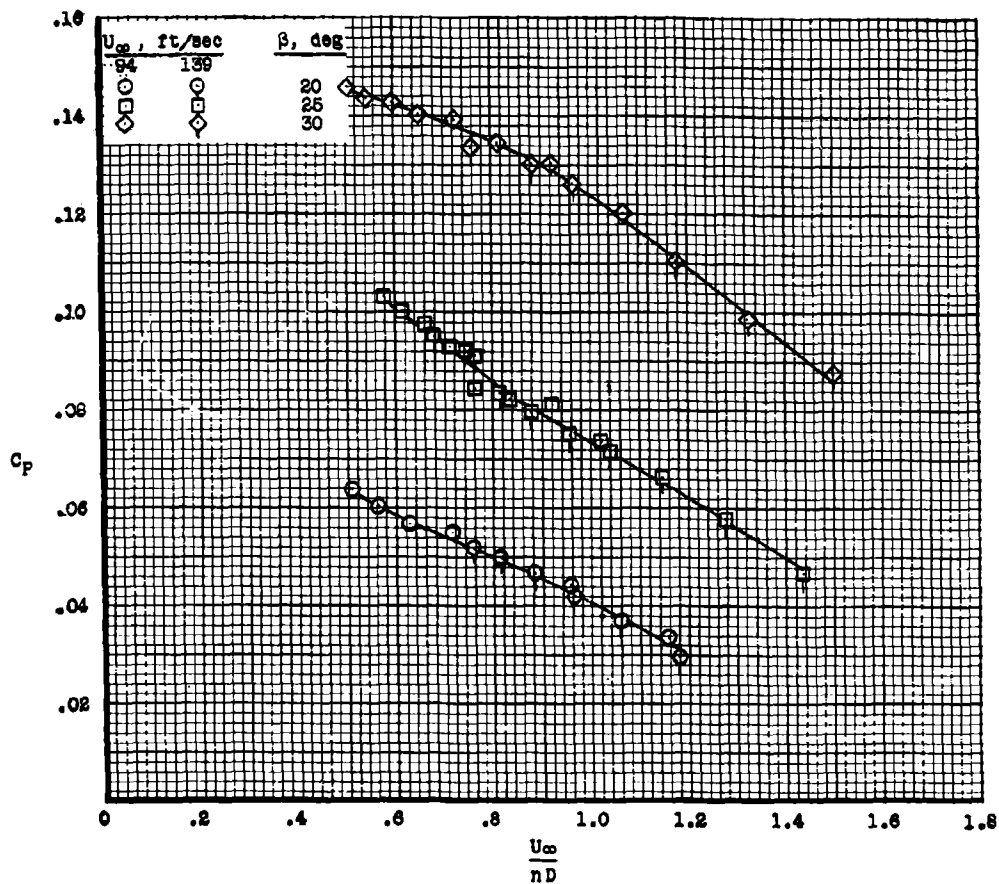
(b) C_p against U_∞/nD .

Figure 5.- Continued.

L-1618

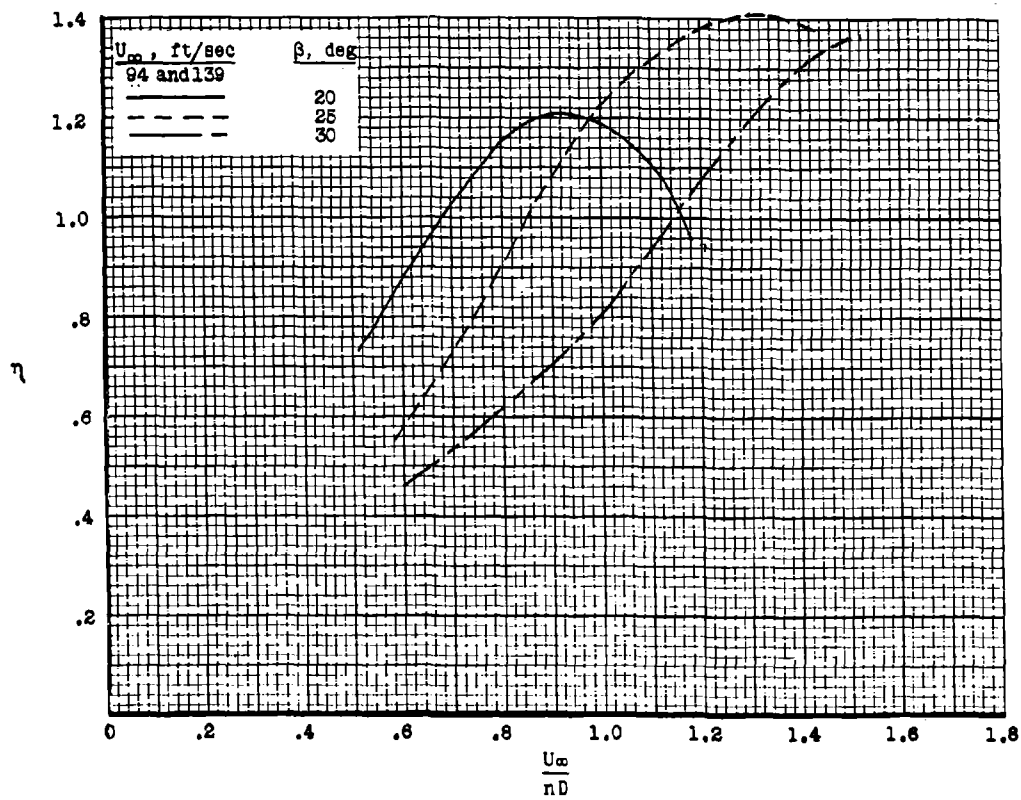
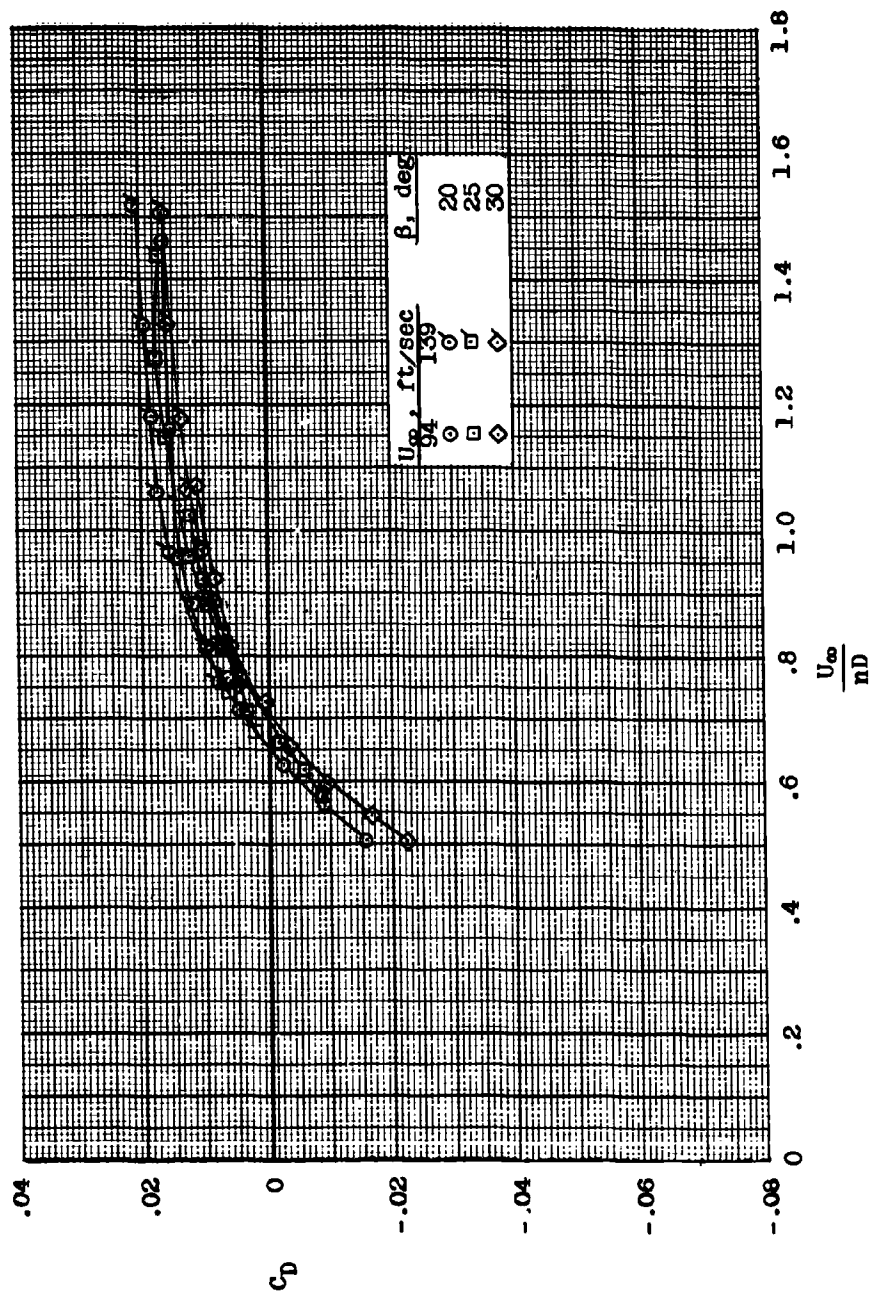
(c) η against U_{∞}/nD .

Figure 5.- Continued.



(d) C_D against U_∞/nD .

Figure 5.- Concluded.

8191-71

L-1618

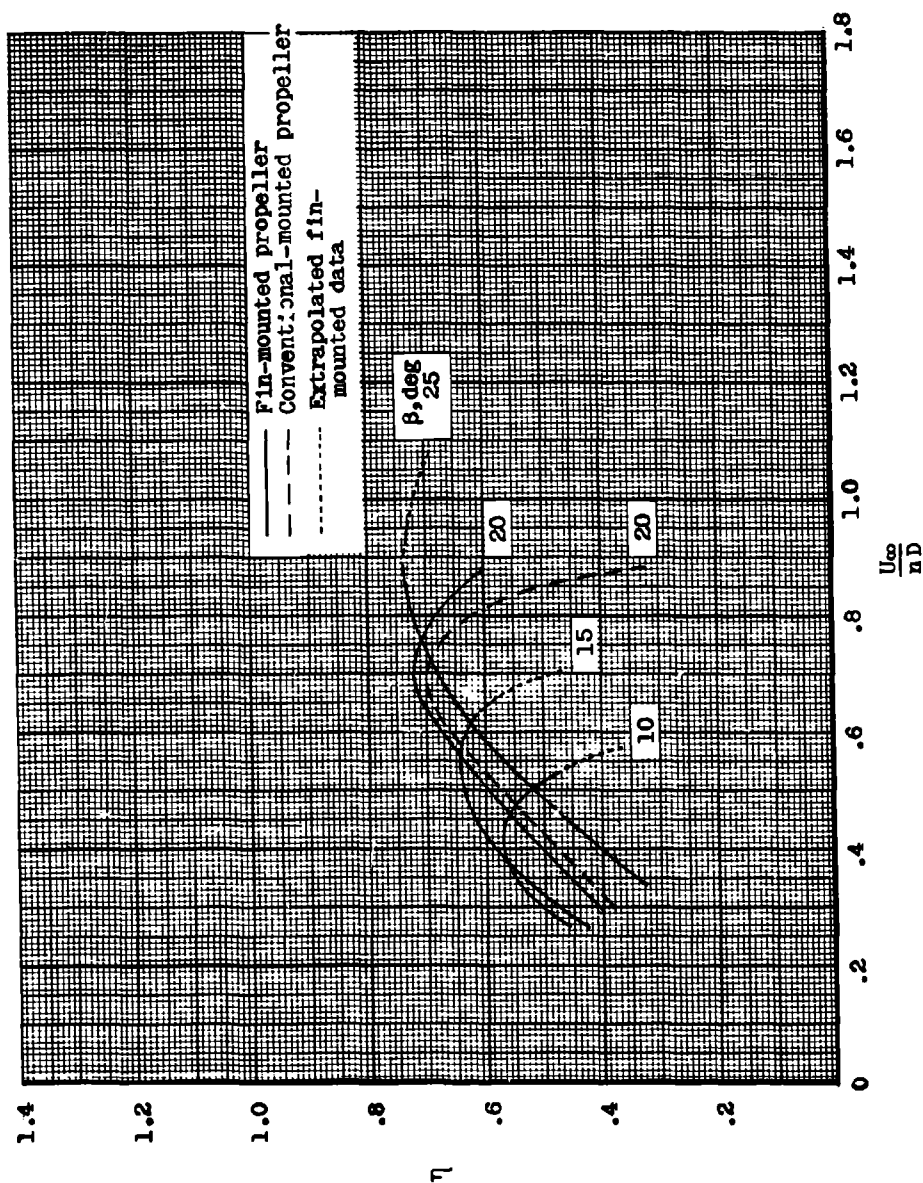
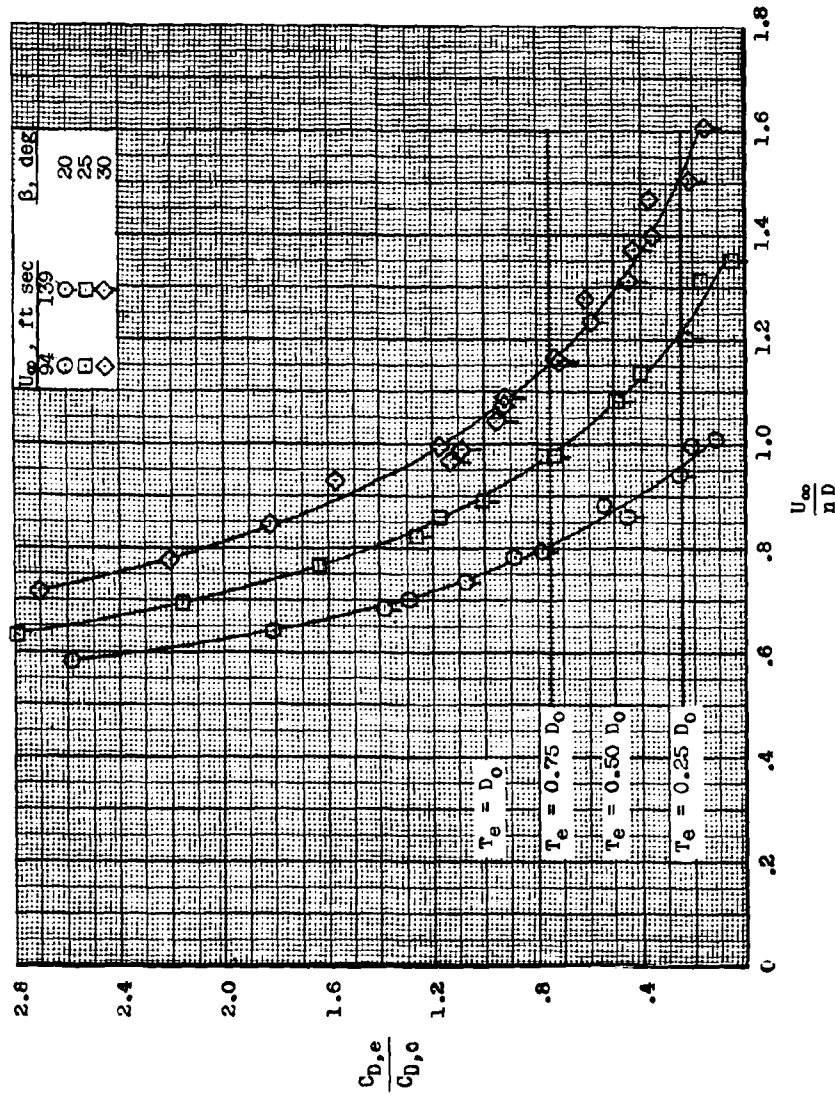


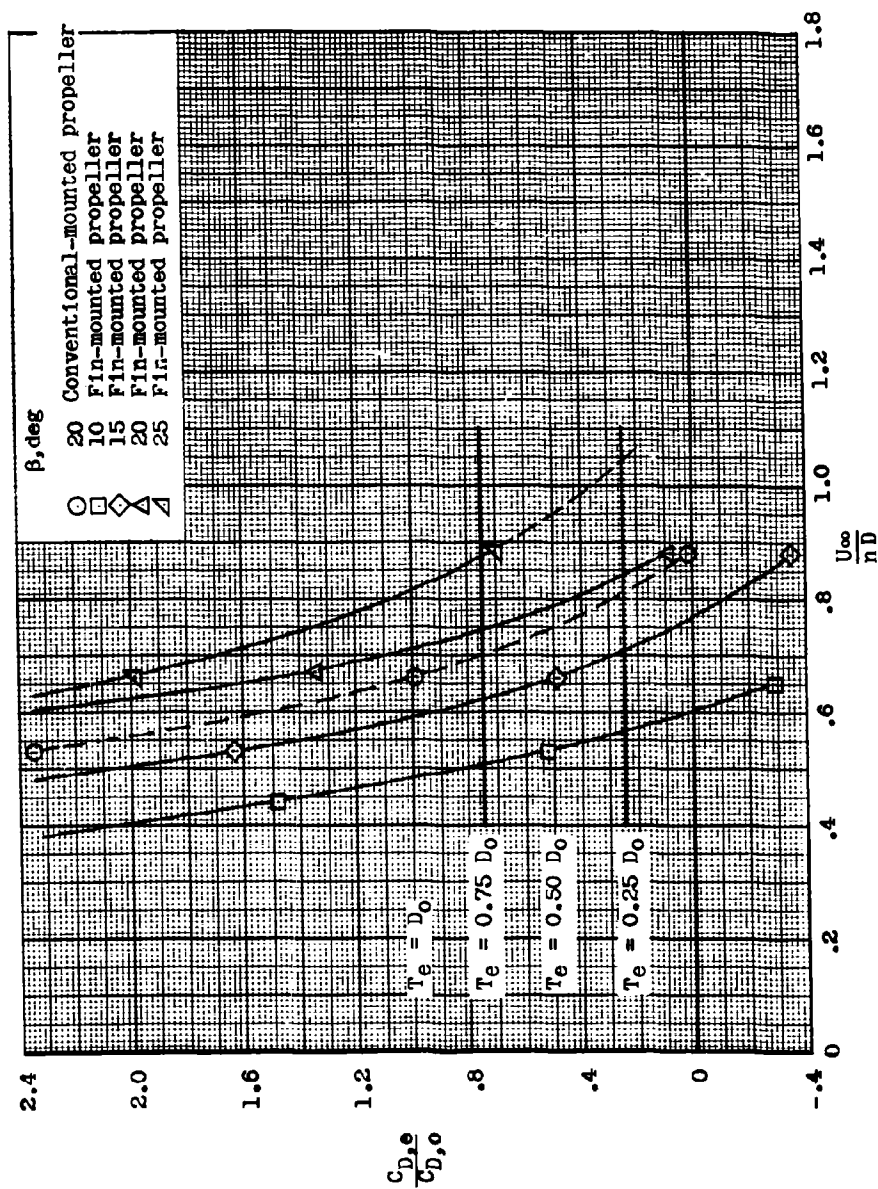
Figure 6.- Variation of the propeller efficiency with U_∞/nD for the conventional-mounted- and fin-mounted-propeller configurations. $\alpha = -0.5^\circ$.



(a) Propeller 1.

Figure 7.- Ratio of the effective drag, propeller operating, to the drag of the basic model with propeller removed. $\alpha = -0.5^\circ$.

L-1618



(b) Conventional-mounted and fin-mounted propellers.

Figure 7.- Concluded.

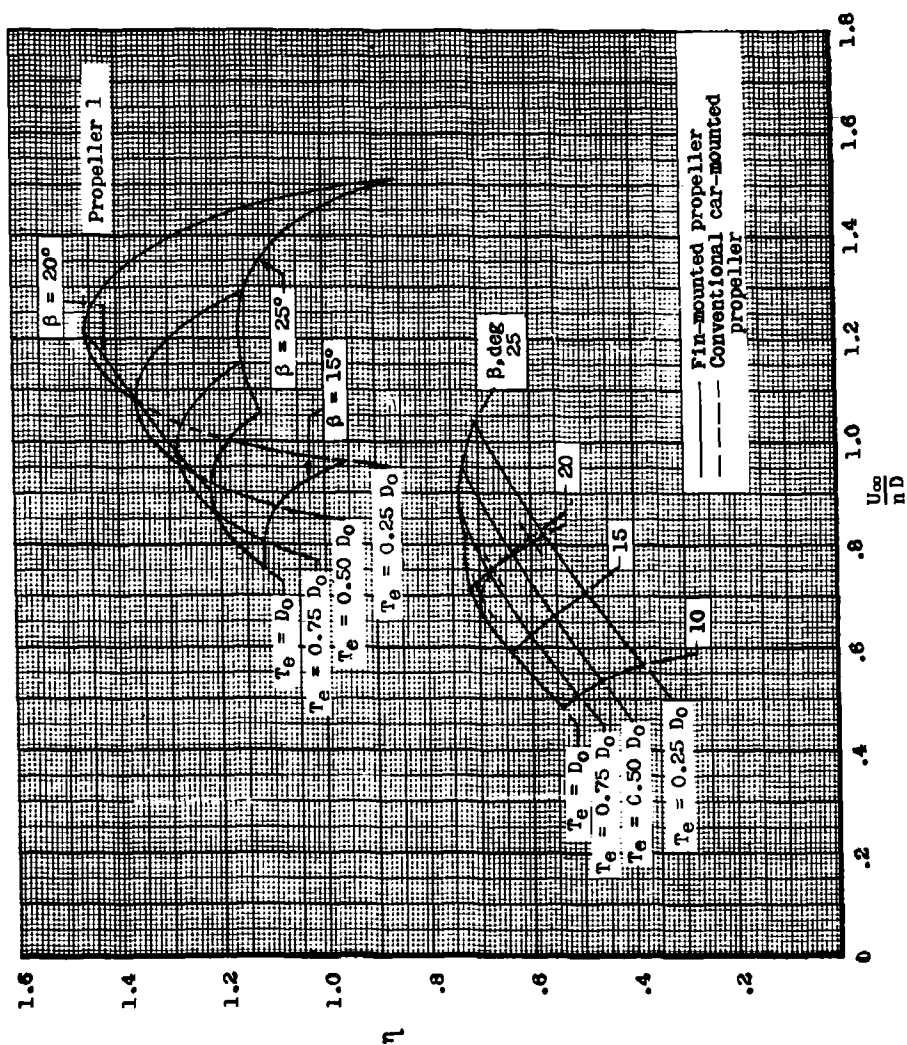


Figure 8.- Variation of the propeller efficiency with advance ratio for propeller 1 and conventional-mounted and fin-mounted propellers. $\alpha = -0.5^\circ$.

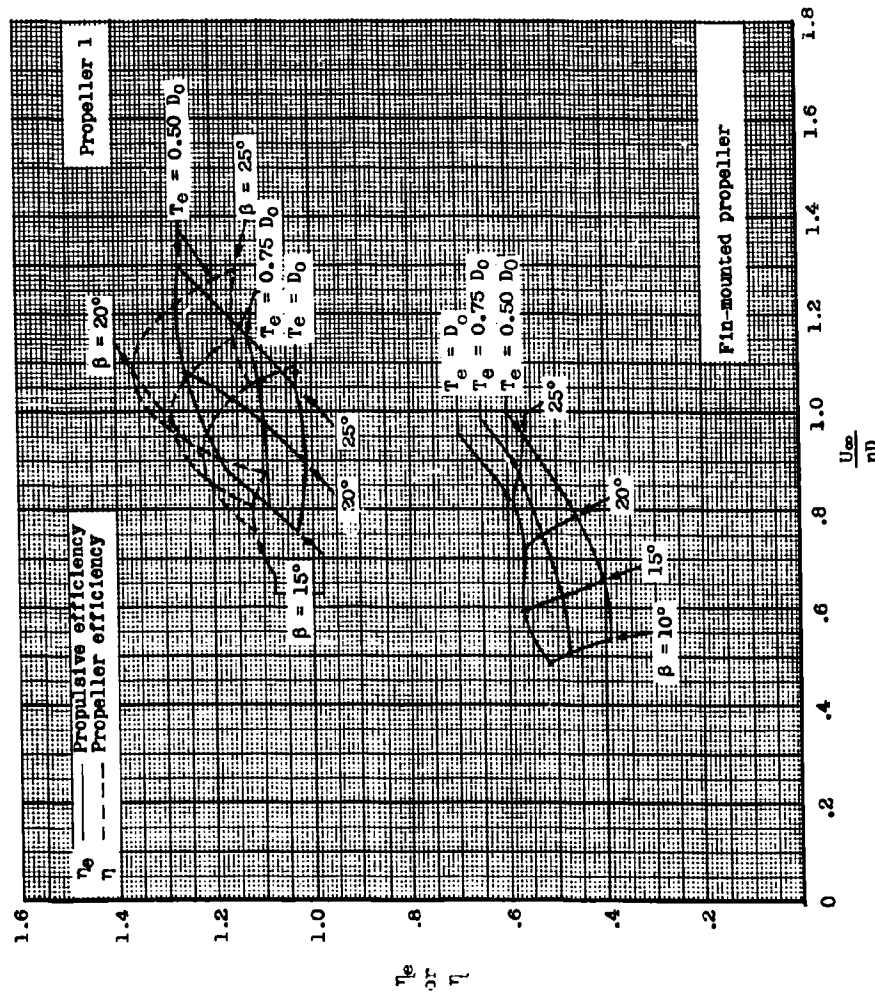
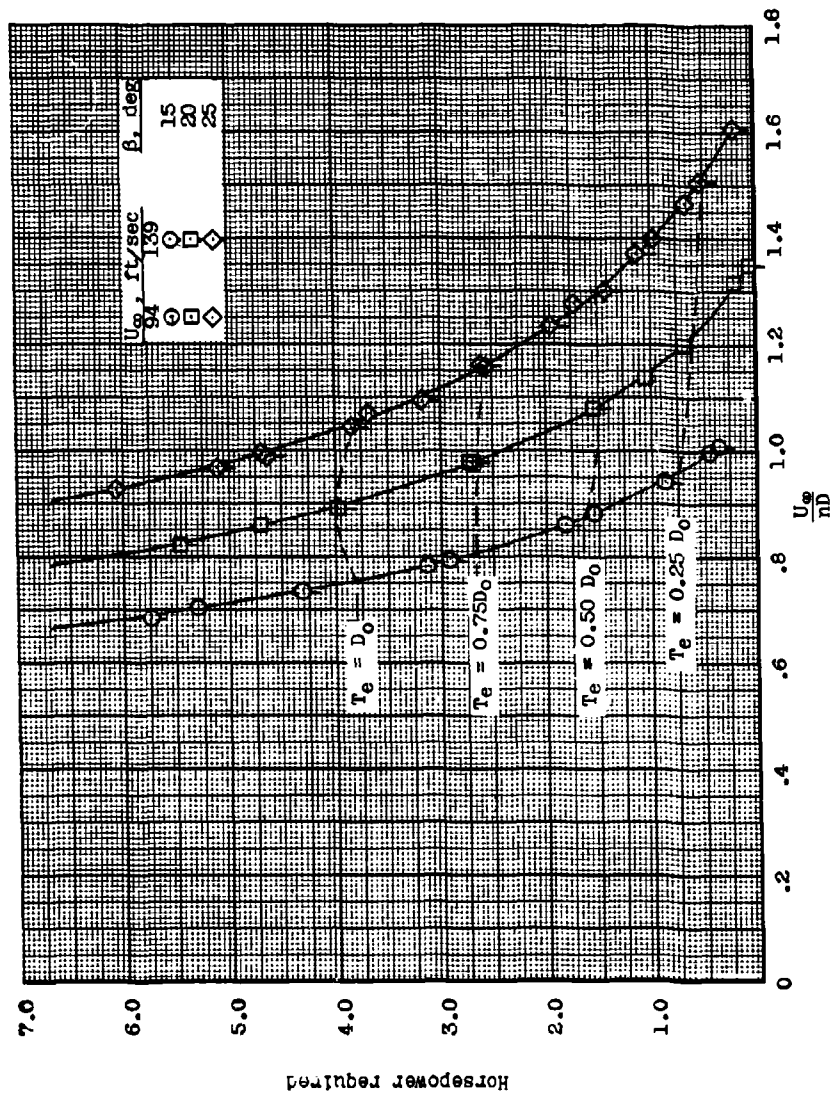
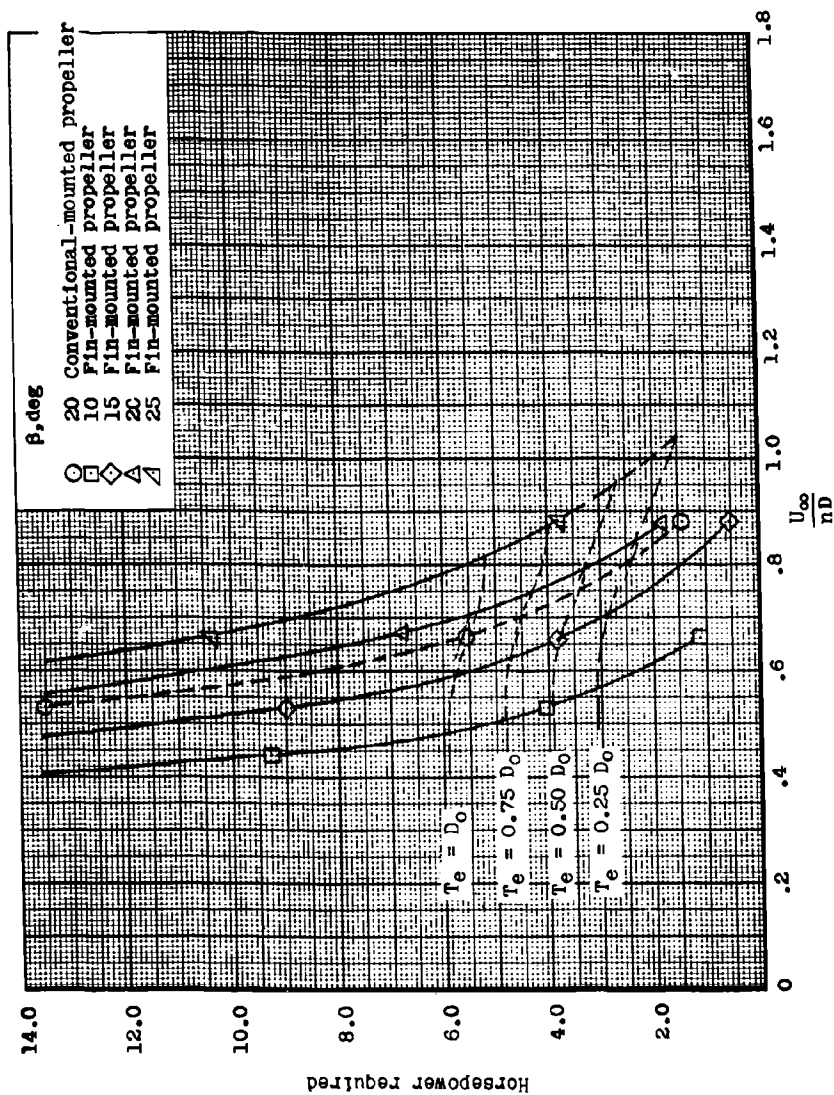


Figure 9.- Variation of the propeller propulsive efficiency with advance ratio for propeller 1 and a fin-mounted propeller. Propeller efficiency of propeller 1 is included for comparison purposes.



(a) Propeller 1.

Figure 10.- Variation of the horsepower required for varied flight conditions for the model with propeller 1 and conventional-mounted or fin-mounted propellers operating.



(b) Conventional-mounted or fin-mounted propeller.

Figure 10.- Concluded.

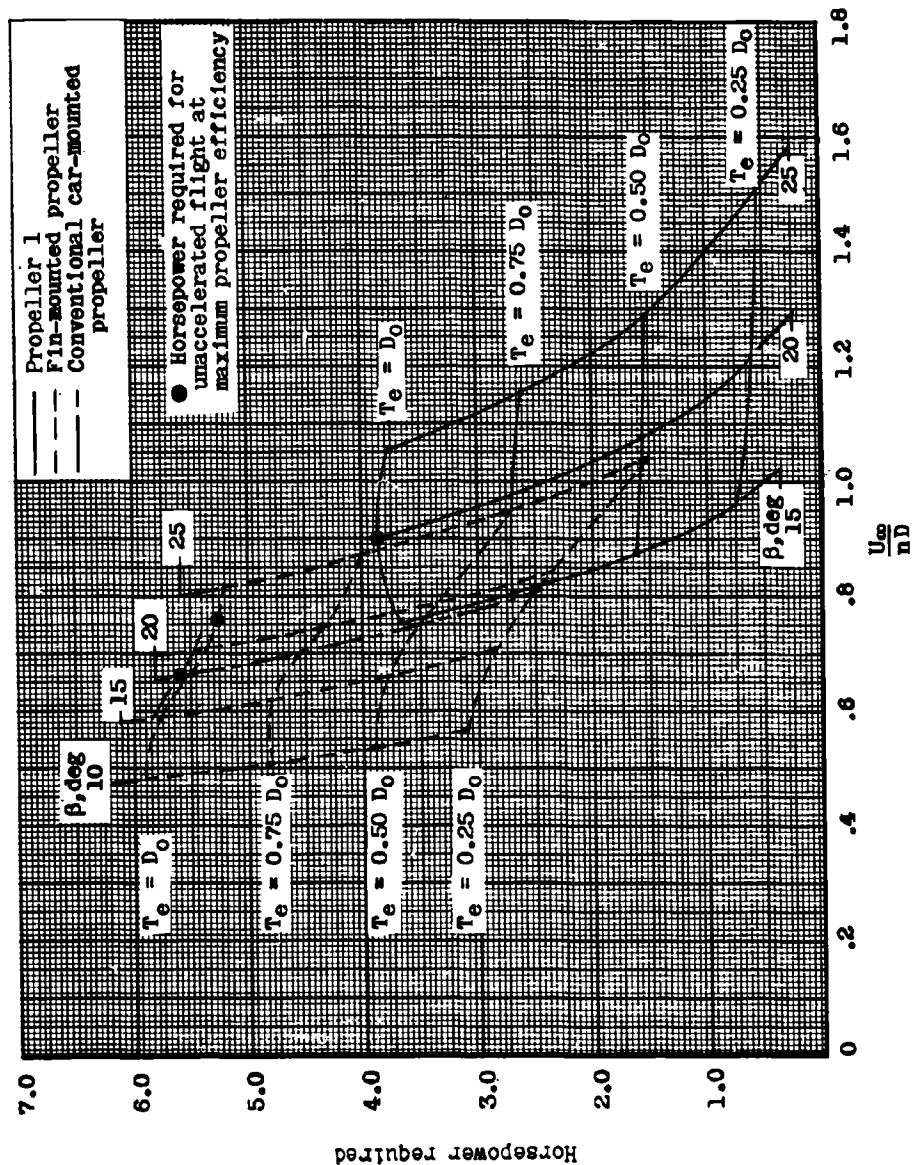


Figure 11.1.- Comparison of the horsepower required for several flight conditions of the model with propeller 1 and conventional-mounted and fin-mounted propellers operating. $\alpha = -0.5^\circ$.

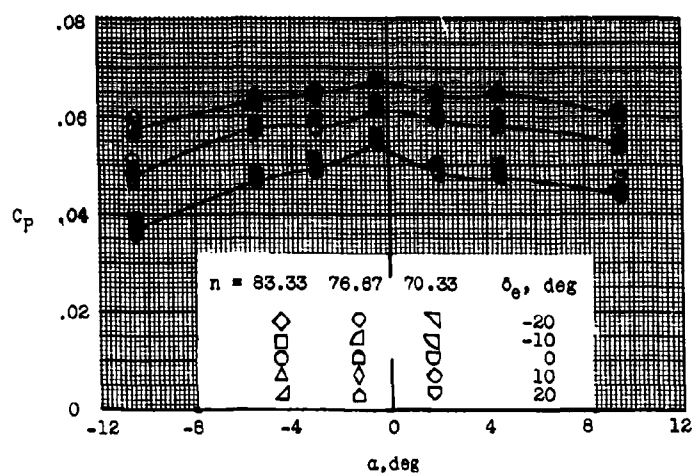
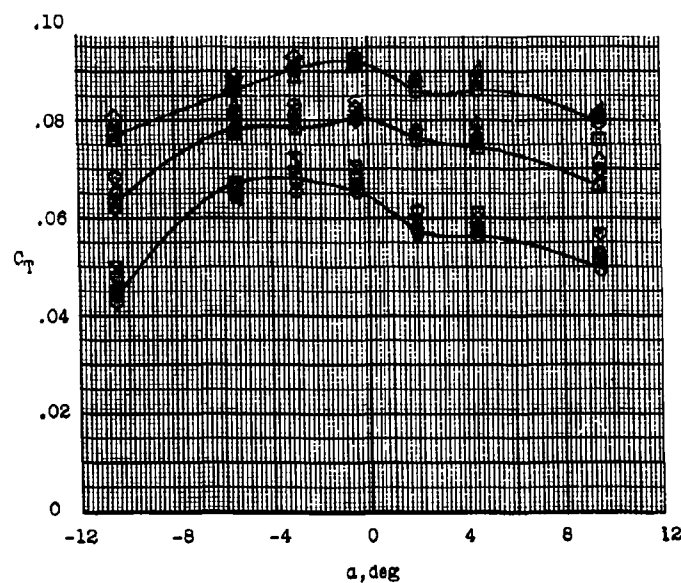
(a) C_p against α .(b) C_T against α .

Figure 12.- Variation of thrust and power coefficients with angle of attack for three revolution speeds with and without elevator deflection. Propeller 1 operating at $\beta = 20^\circ$. $U_\infty \approx 140$ ft/sec.

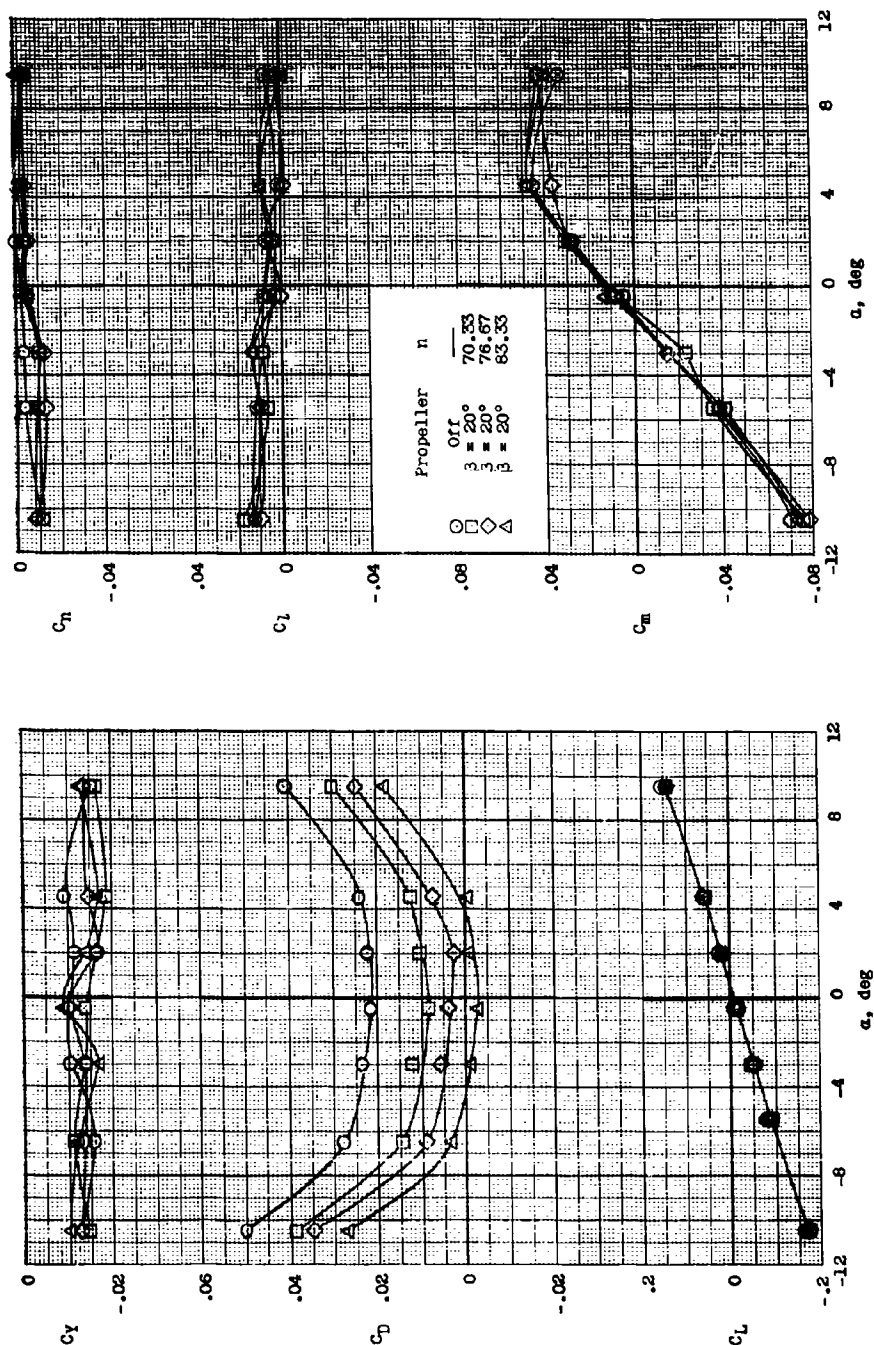
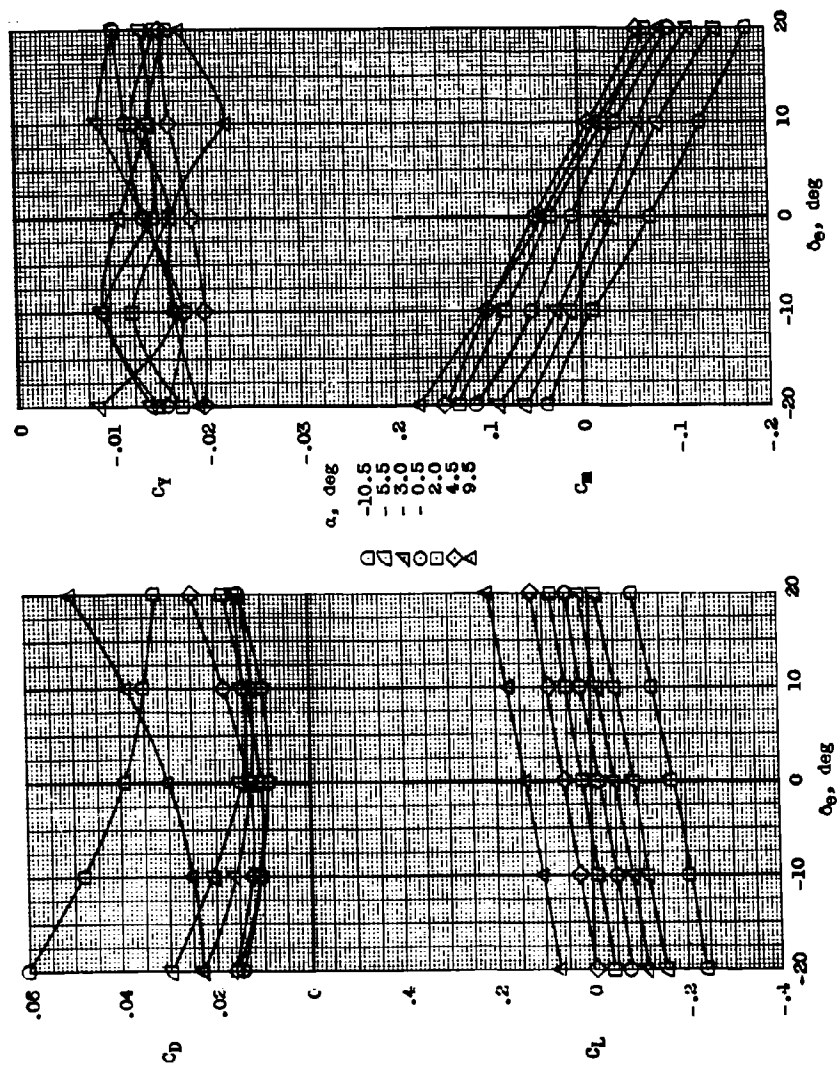


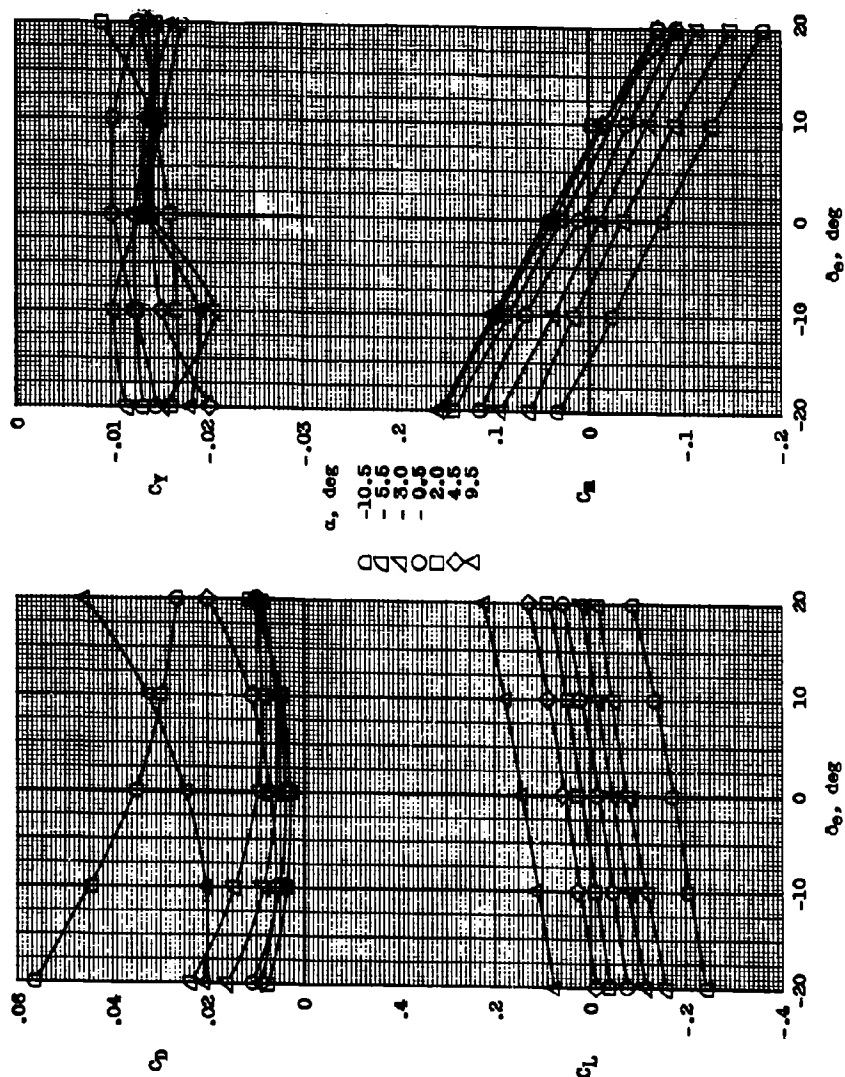
Figure 13.- Variation of the aerodynamic characteristics of the model with angle of attack with and without propeller 1 operating. $U_\infty \approx 140$ ft/sec.

L-1618



(a) $\frac{U_\infty}{nD} = 1.019$, $n = 70.33$.

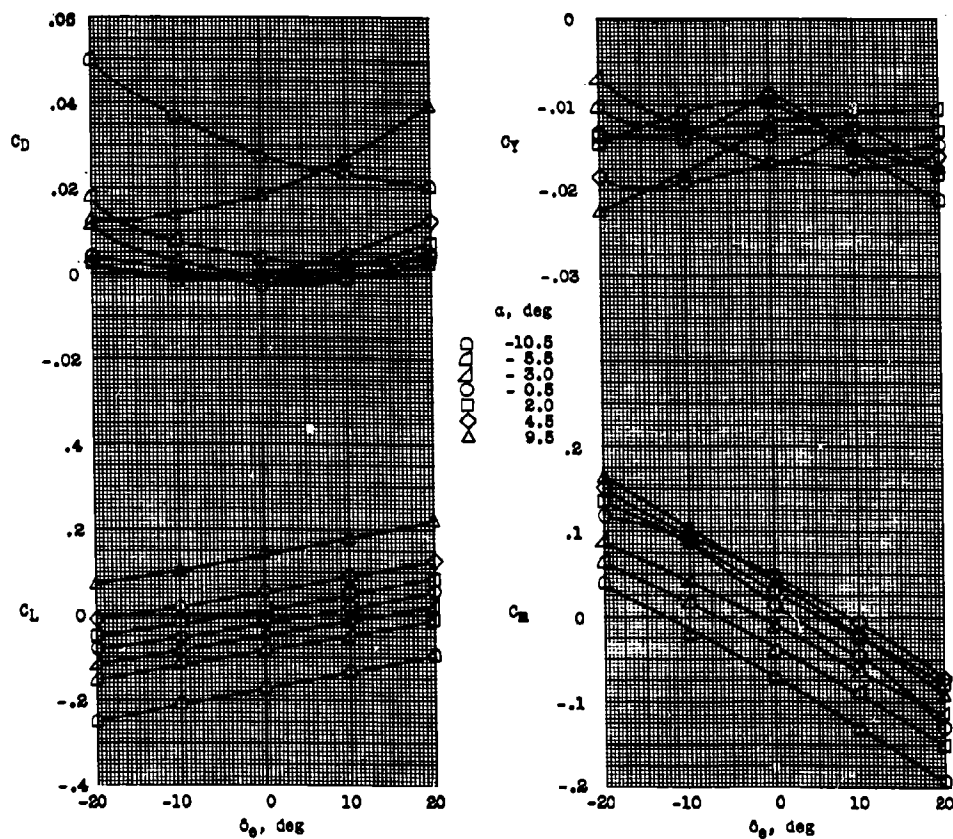
Figure 14.- The effect of elevator deflection on the aerodynamic characteristics of the model with propeller 1 installed. $\beta = 20^\circ$.



(b) $\frac{U_\infty}{nD} = 0.938, n = 76.67.$

Figure 14.- Continued.

L-1618



(c) $\frac{U}{nD} = 0.867, \quad n = 83.33.$

Figure 14.- Concluded.

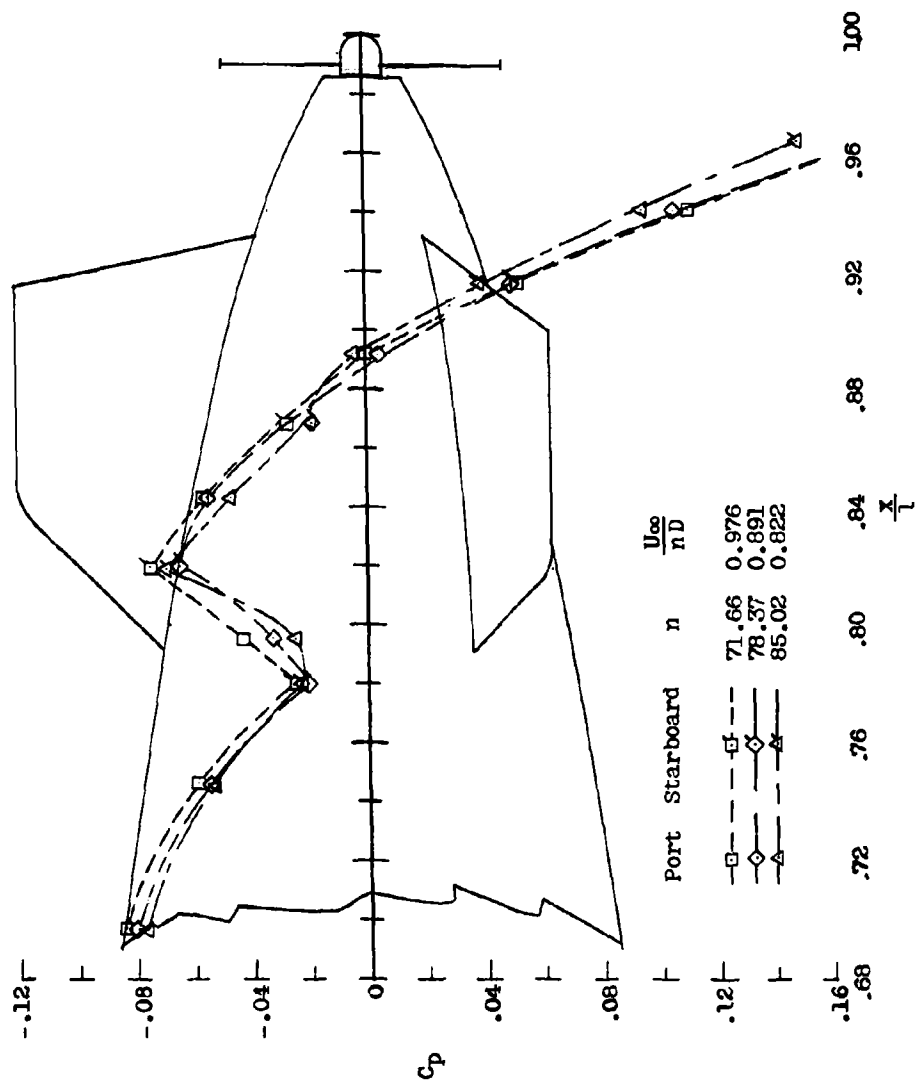


Figure 15.- Aft-hull surface-pressure coefficients with propeller 1 installed and operating.
 $\beta = 20^\circ$; $\alpha = -0.5^\circ$.

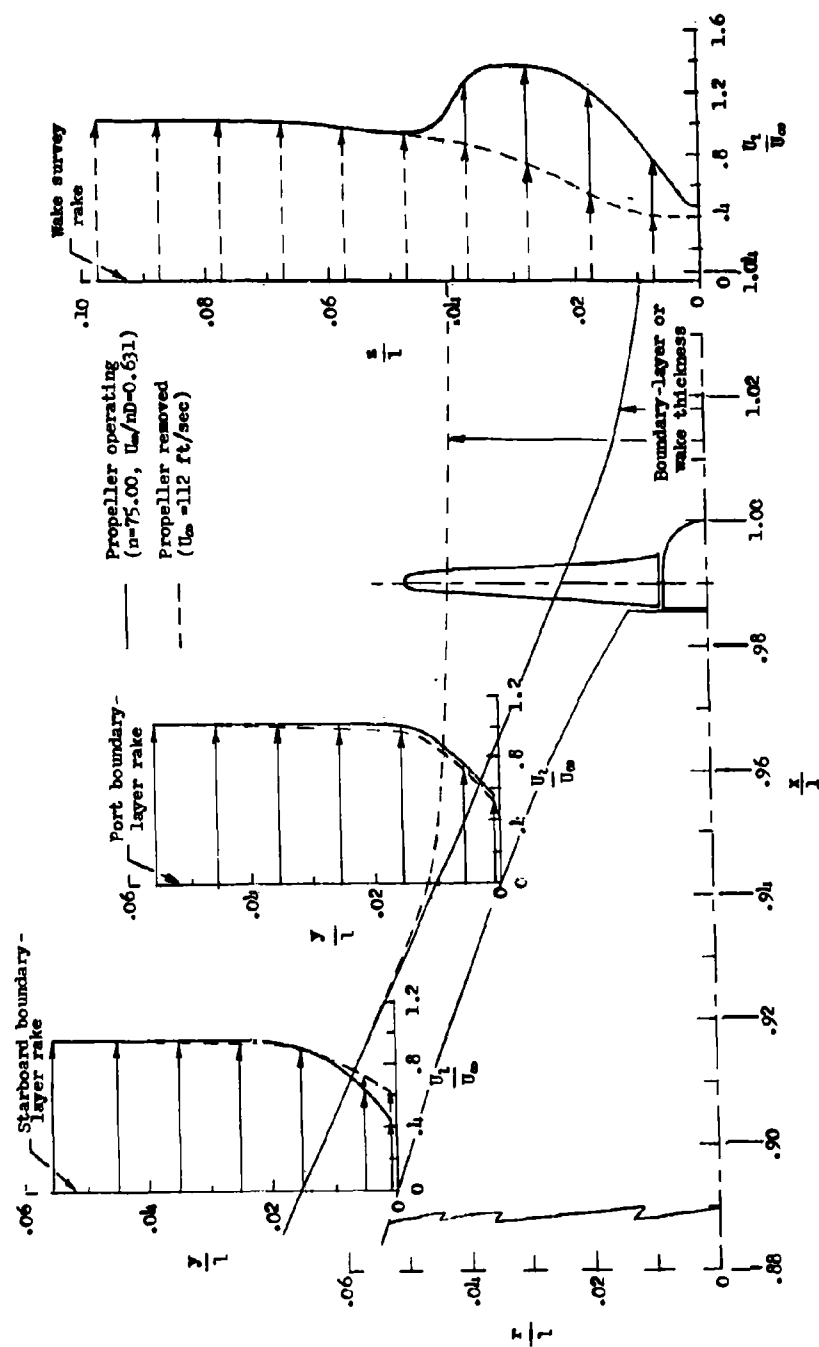


Figure 16.- Variation of the boundary-layer and wake-flow characteristics at $\alpha = -0.5^\circ$ with and without propeller 1 operating. Data taken from tables 1 and 3(h). The boundary-layer thickness is assumed to extend from the body to a point where $\frac{U_t}{U_\infty} = 0.9$. $\alpha = -0.5^\circ$.

<p>NASA TN D-1026 National Aeronautics and Space Administration. WIND-TUNNEL TESTS OF A 1/20-SCALE AIRSHIP MODEL WITH STERN PROPELLERS. H. Clyde McLemore. January 1962. 137p. OTS price, \$2.75. (NASA TECHNICAL NOTE D-1026)</p> <p>The investigation conducted in the Langley full-scale tunnel included tests of two different propellers and included measurements of propeller thrust and power characteristics, airship force and moment charac- teristics, hull pressure distributions, and hull boundary-layer and wake characteristics. The tests showed that a stern-mounted propeller can give a much higher propulsive efficiency than that of a conventional-mounted- or a fin-mounted-propeller installation. In general, stern-propeller operation was found to have only very small effects on the model aerodynamic characteristics.</p>	<p>I. McLemore, Huel Clyde II. NASA TN D-1026 (Initial NASA distribution: 1, Aerodynamics, aircraft; 50, Stability and control.)</p>	<p>NASA TN D-1026 National Aeronautics and Space Administration. WIND-TUNNEL TESTS OF A 1/20-SCALE AIRSHIP MODEL WITH STERN PROPELLERS. H. Clyde McLemore. January 1962. 137p. OTS price, \$2.75. (NASA TECHNICAL NOTE D-1026)</p> <p>The investigation conducted in the Langley full-scale tunnel included tests of two different propellers and included measurements of propeller thrust and power characteristics, airship force and moment charac- teristics, hull pressure distributions, and hull boundary-layer and wake characteristics. The tests showed that a stern-mounted propeller can give a much higher propulsive efficiency than that of a conventional-mounted- or a fin-mounted-propeller installation. In general, stern-propeller operation was found to have only very small effects on the model aerodynamic characteristics.</p>	<p>I. McLemore, Huel Clyde II. NASA TN D-1026 (Initial NASA distribution: 1, Aerodynamics, aircraft; 50, Stability and control.)</p>	<p>NASA Copies obtainable from NASA, Washington</p>
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